

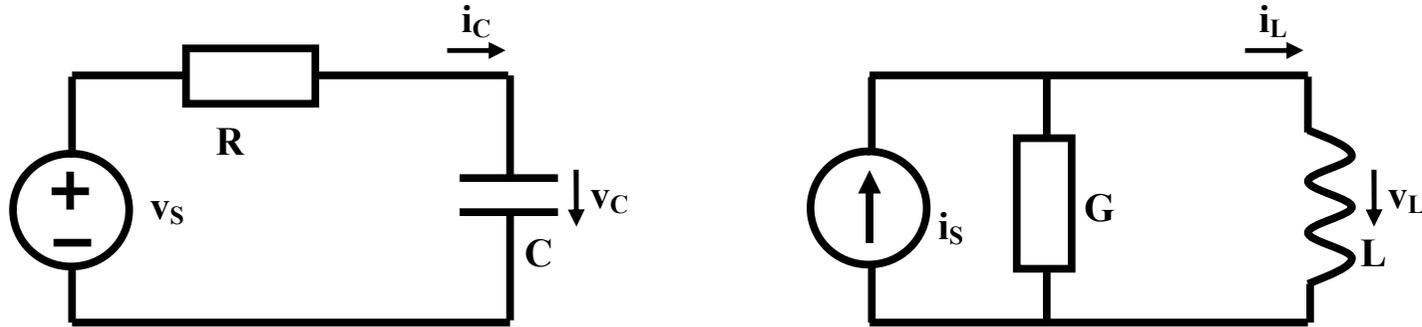
# 电子电路与系统基础II

习题课第六讲 一阶动态电路的时域分析

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# 作业一、RC对偶GL



- 图示的一阶**RC**电路对偶一阶**GL**电路（习惯称之为**RL**电路），对一阶**RC**电路成立的结论对一阶**RL**电路同样成立，只需对偶量互换即可

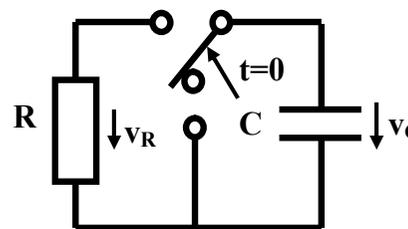
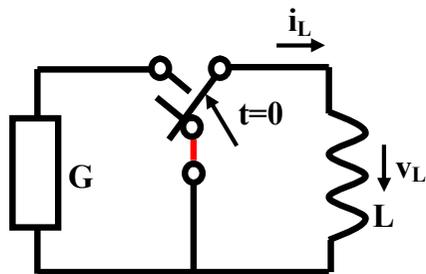
$$v_C(t) = V_0 \cdot e^{-\frac{t}{\tau}} + \int_0^t v_S(\lambda) \cdot e^{-\frac{\lambda-t}{\tau}} d\frac{\lambda}{\tau}$$

$$\tau = RC$$

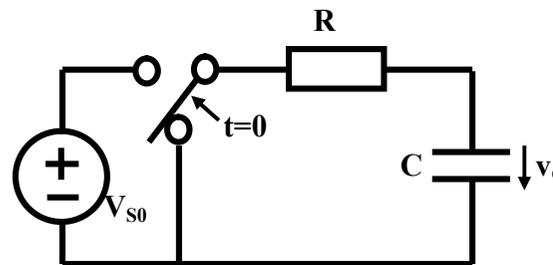
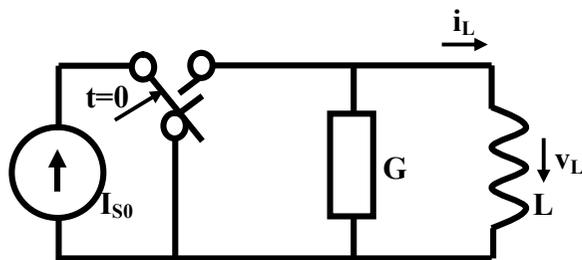
$$i_L(t) = I_0 \cdot e^{-\frac{t}{\tau}} + \int_0^t i_S(\lambda) \cdot e^{-\frac{\lambda-t}{\tau}} d\frac{\lambda}{\tau}$$

$$\tau = GL$$

# 电感放磁、充磁曲线



- **(1) 练习9.2.2** 分析图示一阶RL电路的零输入响应，假设开关在 $t=0$ 时刻拨动，开关拨动前的电感初始电流为 $I_0$ 
  - 给出电感电流放磁曲线，和放磁电压时域波形：表达式和曲线

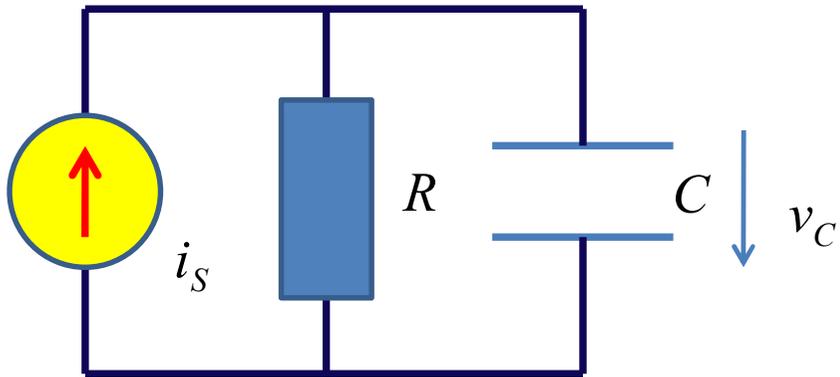


- **(2) 练习9.2.4** 分析图示一阶RL电路的零状态响应，假设开关在 $t=0$ 时刻换路，开关换路前放磁已经结束，电感初始电流为 $0$ 
  - 给出电感电流充磁曲线，和充磁电压时域波形：表达式和曲线

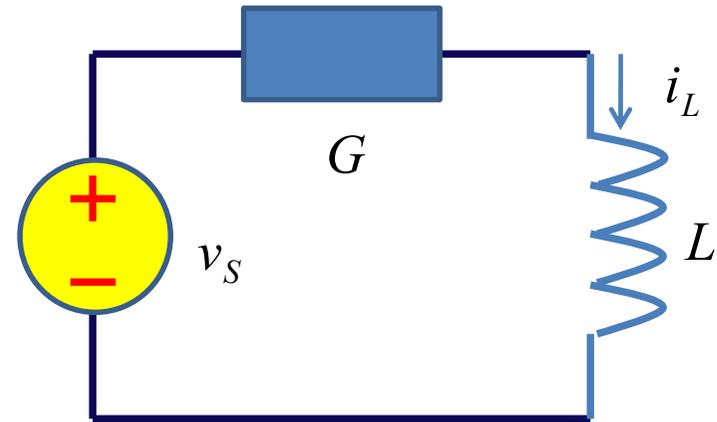
# 电容和电感的对偶关系

	电容	电感
定义	电容是导体保持可移动电荷的能力，在单位电压作用下导体结构（结点）保持的电荷量就是电容量	电感是描述导线结构中流通电流产生与链接磁通的能力，在单位电流作用下导线结构（回路）链接的磁通量就是电感量
存在性	电路中总是有导体（结点）电荷集聚，（结点间）始终存在电容效应	电路中总是有导线（回路）链接磁通，（回路间）始终存在电感效应
线性时不变	$C = \frac{Q}{V} \quad C_d = \frac{dQ}{dV} = C$	$L = \frac{\Phi}{I} \quad L_d = \frac{d\Phi}{dI} = L$
元件约束	$i(t) = \frac{dQ(t)}{dt} = C \frac{dv(t)}{dt}$	$v(t) = \frac{d\Phi(t)}{dt} = L \frac{di(t)}{dt}$
非线性	$Q(V_0 + v(t)) = C_0 \cdot V_0 + C_d(V_0) \cdot v(t) + \dots$	$\Phi(I_0 + i(t)) = L_0 \cdot I_0 + L_d(I_0) \cdot i(t) + \dots$
元件约束	$i(t) = \frac{dQ(t)}{dt} = C_d(V_0 + v(t)) \frac{dv(t)}{dt}$	$v(t) = \frac{d\Phi(t)}{dt} = L_d(I_0 + i(t)) \frac{di(t)}{dt}$
线性时变	$Q(t) = C(t)v(t)$	$\Phi(t) = L(t)i(t)$
元件约束	$i(t) = \frac{dQ(t)}{dt} = C(t) \frac{dv(t)}{dt} + v(t) \frac{dC(t)}{dt}$	$v(t) = \frac{d\Phi(t)}{dt} = L(t) \frac{di(t)}{dt} + i(t) \frac{dL(t)}{dt}$

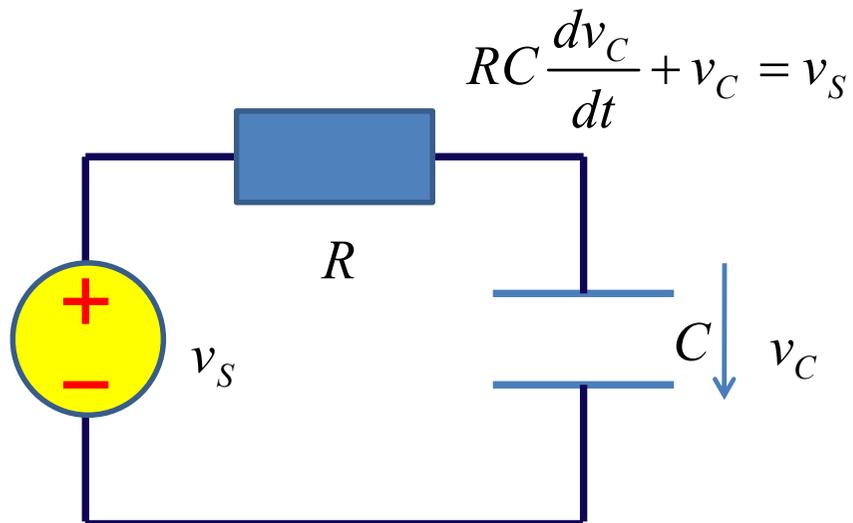
# 阻容电路 对偶 导感电路



$$C \frac{dv_c}{dt} + \frac{v_c}{R} = i_s$$

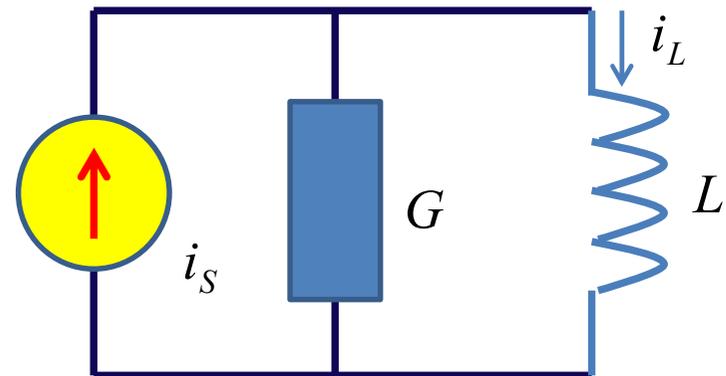


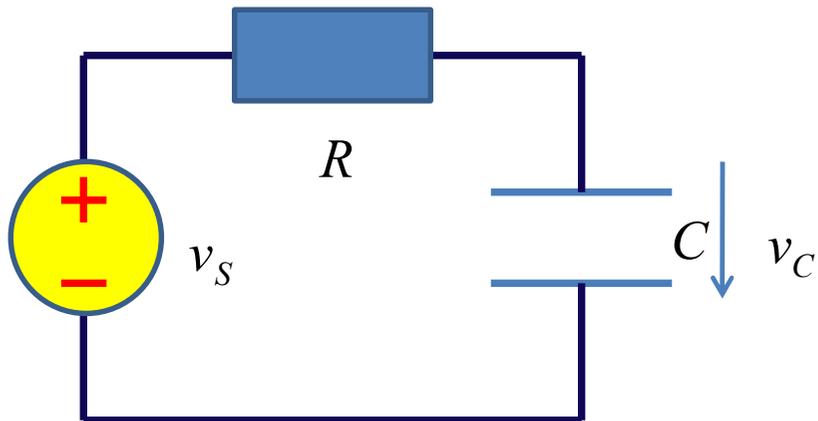
$$L \frac{di_L}{dt} + \frac{i_L}{G} = v_s$$



$$RC \frac{dv_c}{dt} + v_c = v_s$$

$$GL \frac{di_L}{dt} + i_L = i_s$$

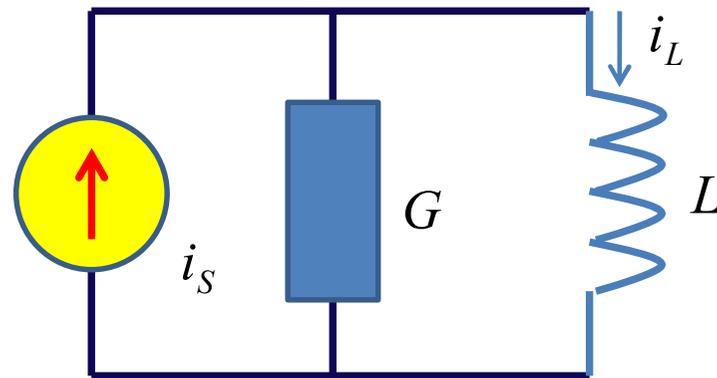




$$RC \frac{dv_C}{dt} + v_C = v_S$$

$$\tau = RC$$

$$\tau \frac{dx}{dt} + x = s$$



$$GL \frac{di_L}{dt} + i_L = i_S$$

$$\tau = GL$$

## 微分方程求解

$$x(t) = \underbrace{X_0 e^{-\frac{t}{\tau}}}_{\text{零输入响应}} + \underbrace{\int_0^t s(\lambda) \cdot e^{-\frac{\lambda-t}{\tau}} d\frac{\lambda}{\tau}}_{\text{零状态响应}}$$

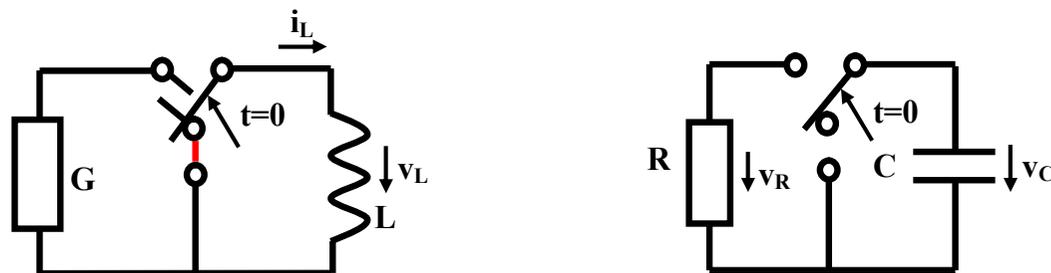
零输入响应

零状态响应

$$v_C(t) = \underbrace{V_0 e^{-\frac{t}{\tau}}}_{\text{零输入响应}} + \underbrace{\int_0^t v_S(\lambda) \cdot e^{-\frac{\lambda-t}{\tau}} d\frac{\lambda}{\tau}}_{\text{零状态响应}}$$

$$i_L(t) = \underbrace{I_0 e^{-\frac{t}{\tau}}}_{\text{零输入响应}} + \underbrace{\int_0^t i_S(\lambda) \cdot e^{-\frac{\lambda-t}{\tau}} d\frac{\lambda}{\tau}}_{\text{零状态响应}}$$

# 零输入响应



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  - 给出电感电流放磁曲线，和放磁电压时域波形：表达式和曲线

$$\underline{i_L(t) = I_0 e^{-\frac{t}{\tau}}} \qquad \underline{v_C(t) = V_0 e^{-\frac{t}{\tau}}}$$

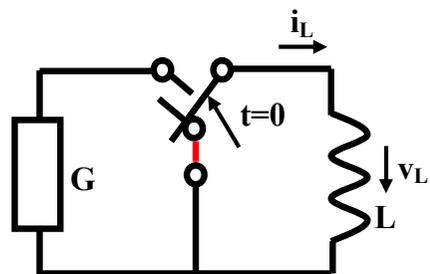
直接根据对偶关系写结果

$$\tau = GL$$

$$\tau = RC$$

无需走求解微分方程的标准流程：直接由三要素给出最终结果

## 三要素法：通用于所有一阶LTI系统



$$\tau = GL$$

时间常数

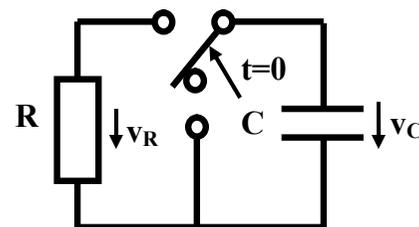
$$i_L(0) = I_0$$

初值

$$i_{L\infty}(t) = 0$$

稳态解

$$\begin{aligned} i_L(t) &= i_{L\infty}(t) + (i_L(0) - i_{L\infty}(0))e^{-\frac{t}{\tau}} \\ &= I_0 e^{-\frac{t}{\tau}} \end{aligned}$$



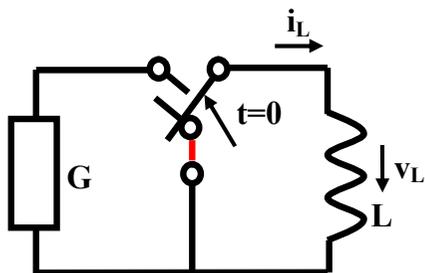
$$\tau = RC$$

$$v_C(0) = V_0$$

$$v_{C\infty}(t) = 0$$

$$\begin{aligned} v_C(t) &= v_{C\infty}(t) + (v_C(0) - v_{C\infty}(0))e^{-\frac{t}{\tau}} \\ &= V_0 e^{-\frac{t}{\tau}} \end{aligned}$$

# 放磁电压、放电电流



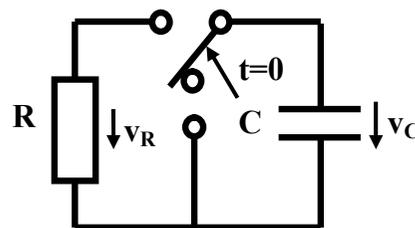
电感磁通因放磁结点的存在以电压形式流失，有电压电感电流则改变

$$i_L(t) = \begin{cases} I_0 & t < 0 \\ I_0 e^{-\frac{t}{\tau}} & t \geq 0 \end{cases}$$

$$v_L(t) = L \frac{d}{dt} i_L(t) = \begin{cases} 0 & t < 0 \\ -\frac{I_0}{G} e^{-\frac{t}{\tau}} & t \geq 0 \end{cases}$$

放磁电压 导致磁通流失，电感电流因而下降

$$i_L(t) = I_0 + \frac{1}{L} \int_0^t v_L(t) dt$$



电容电荷因放电回路的存在以电流形式流失，有电流电容电压则改变

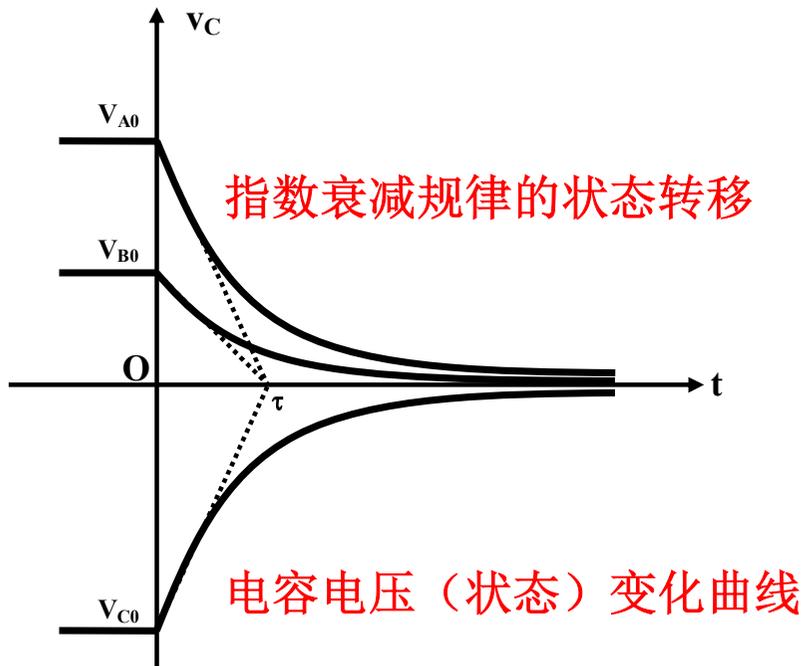
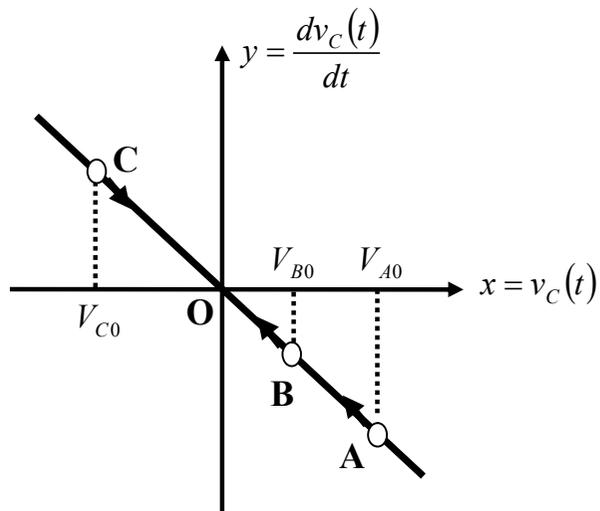
$$v_C(t) = \begin{cases} V_0 & t < 0 \\ V_0 e^{-\frac{t}{\tau}} & t \geq 0 \end{cases}$$

$$i_C(t) = C \frac{d}{dt} v_C(t) = \begin{cases} 0 & t < 0 \\ -\frac{V_0}{R} e^{-\frac{t}{\tau}} & t \geq 0 \end{cases}$$

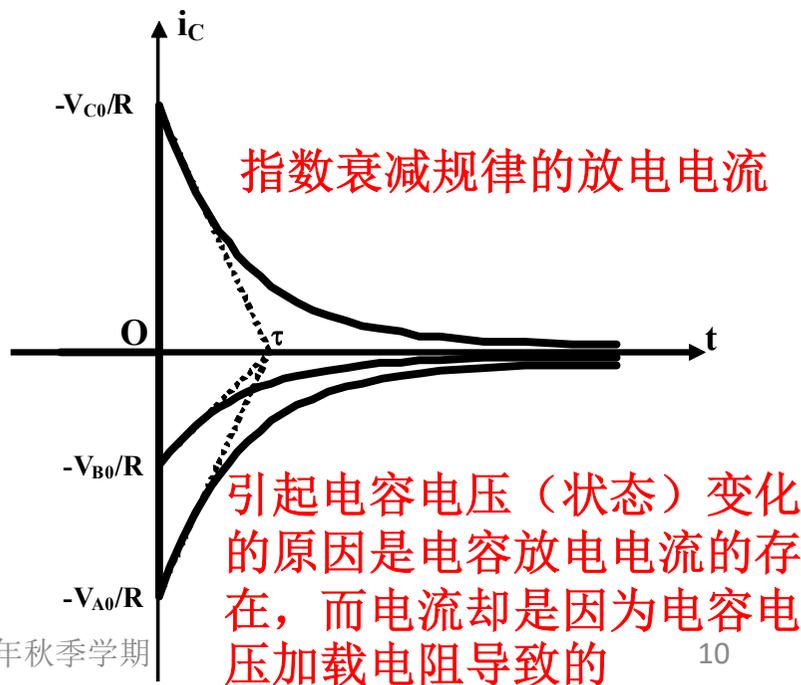
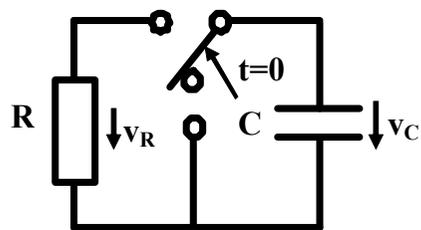
放电电流 导致电荷流失，电容电压因而下降

$$v_C(t) = V_0 + \frac{1}{C} \int_0^t i_C(t) dt$$

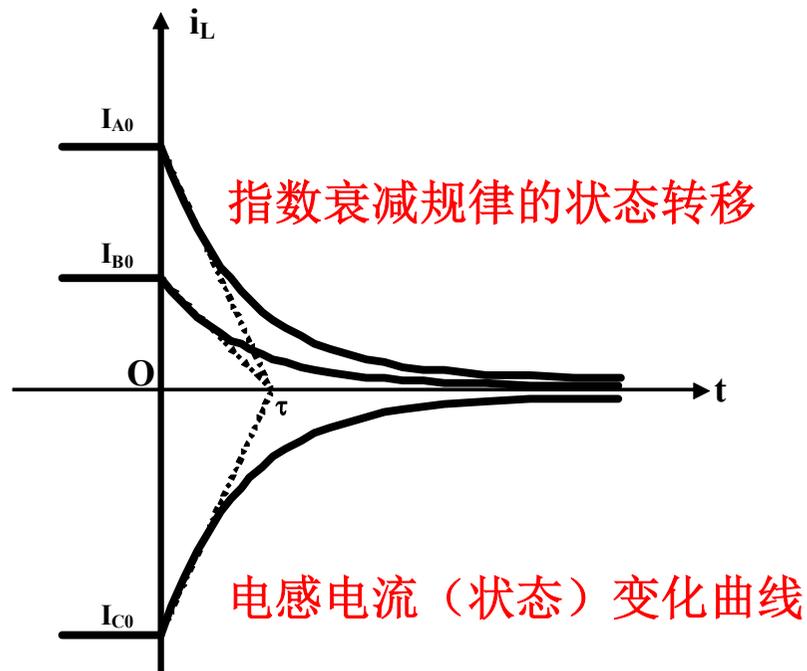
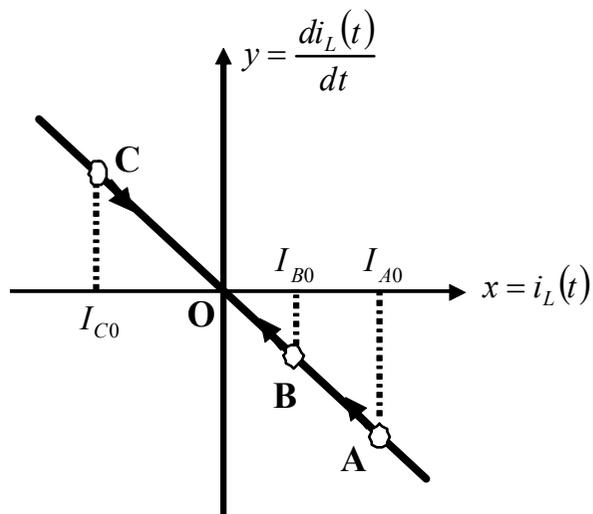
# 放电曲线



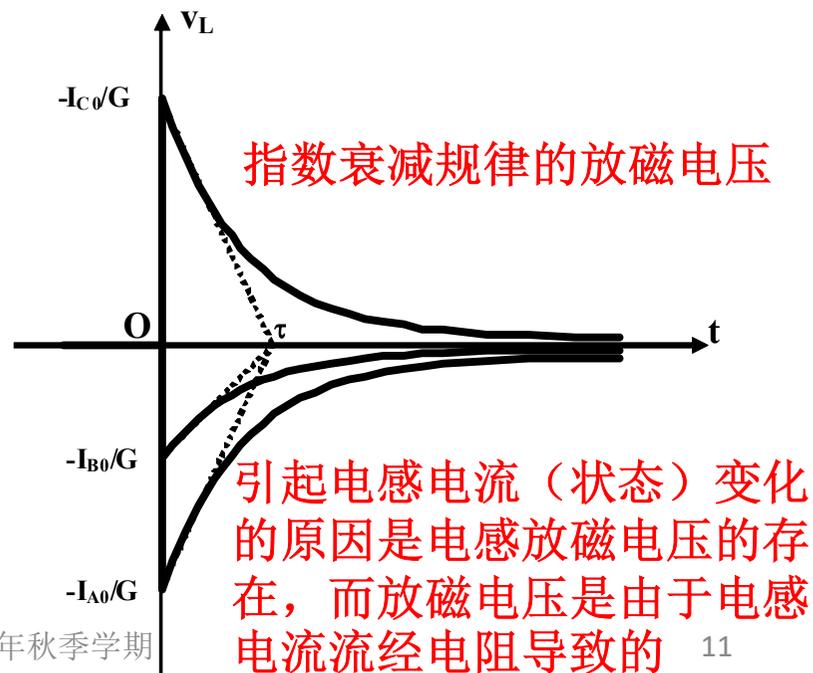
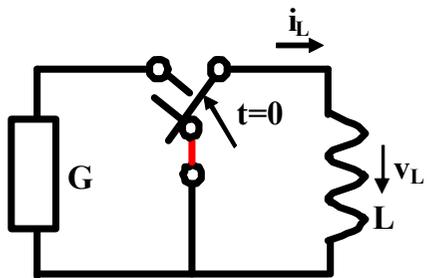
# 放电电流



# 放磁曲线



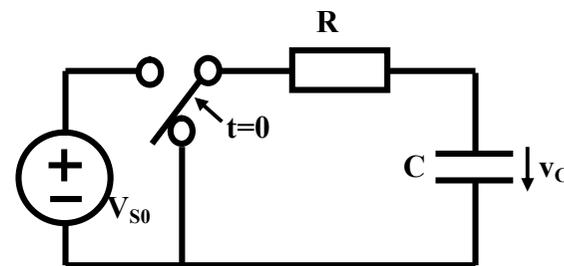
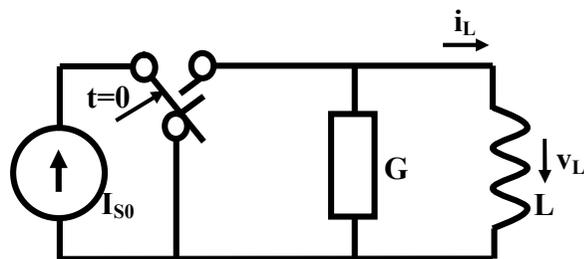
# 放磁电压



# 零状态响应：三要素法

- (2) 练习9.2.4 分析图示一阶RL电路的零状态响应，假设开关在 $t=0$ 时刻换路，开关换路前放磁已经结束，电感初始电流为0

- 给出电感电流充磁曲线，和充磁电压时域波形：表达式和曲线



$$\tau = GL \quad \text{时间常数}$$

$$\tau = RC$$

$$i_L(0) = 0 \quad \text{初值}$$

$$v_C(0) = 0$$

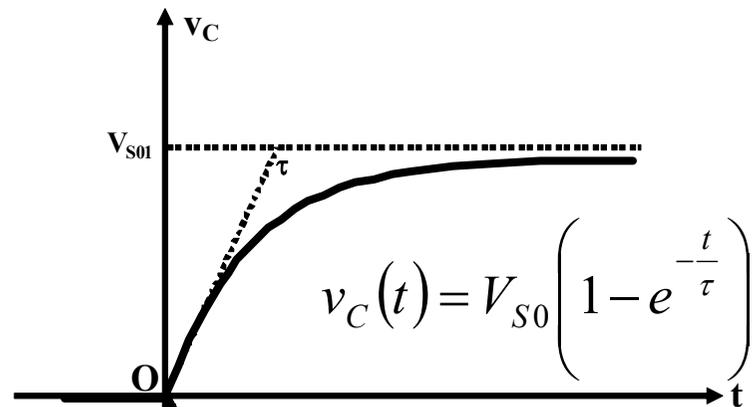
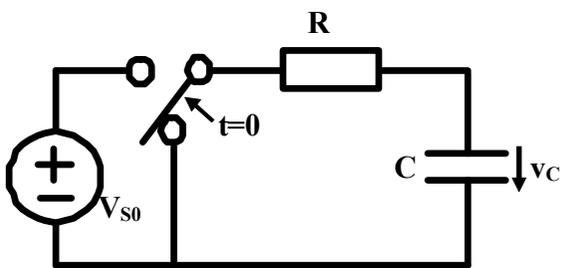
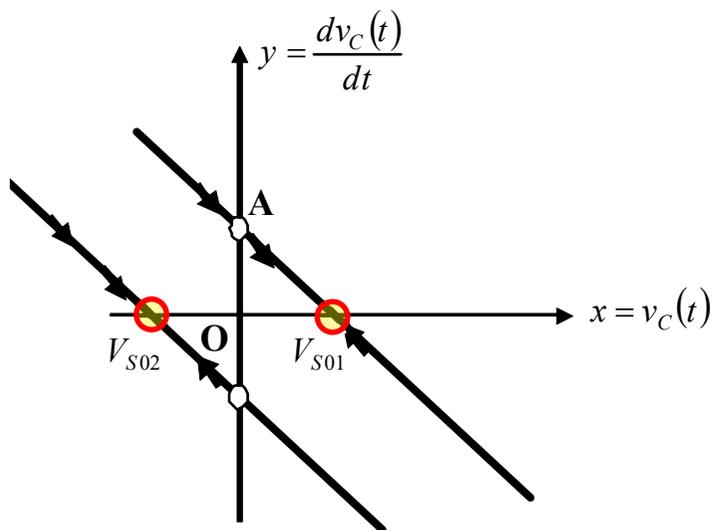
$$i_{L\infty}(t) = I_{S0} \quad \text{稳态解}$$

$$v_{C\infty}(t) = V_{S0}$$

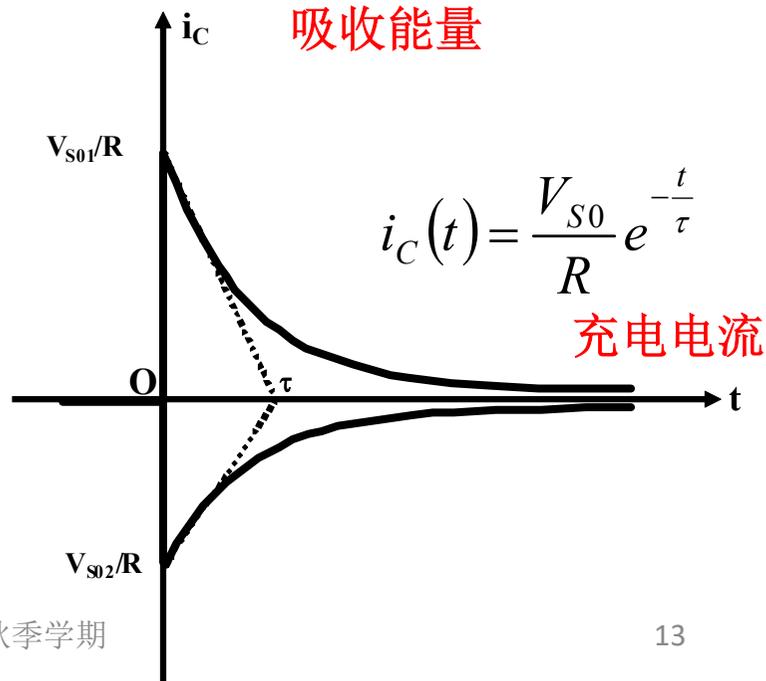
$$\begin{aligned} i_L(t) &= i_{L\infty}(t) + (i_L(0) - i_{L\infty}(0))e^{-\frac{t}{\tau}} \\ &= I_{S0} - I_{S0}e^{-\frac{t}{\tau}} = I_{S0} \left( 1 - e^{-\frac{t}{\tau}} \right) \end{aligned}$$

$$\begin{aligned} v_C(t) &= v_{C\infty}(t) + (v_C(0) - v_{C\infty}(0))e^{-\frac{t}{\tau}} \\ &= V_{S0} - V_{S0}e^{-\frac{t}{\tau}} = V_{S0} \left( 1 - e^{-\frac{t}{\tau}} \right) \end{aligned}$$

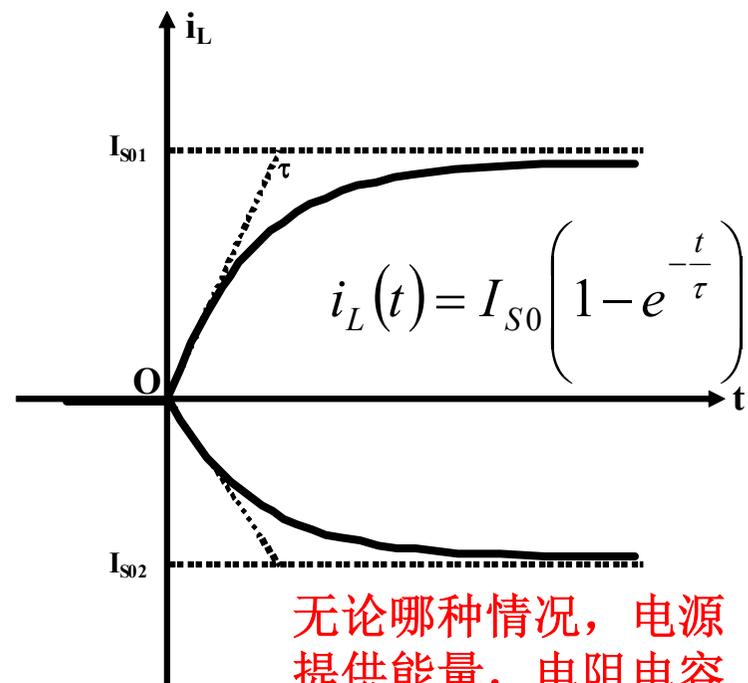
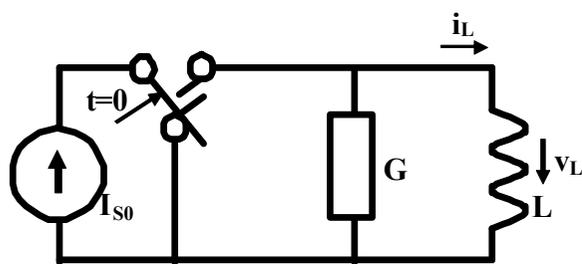
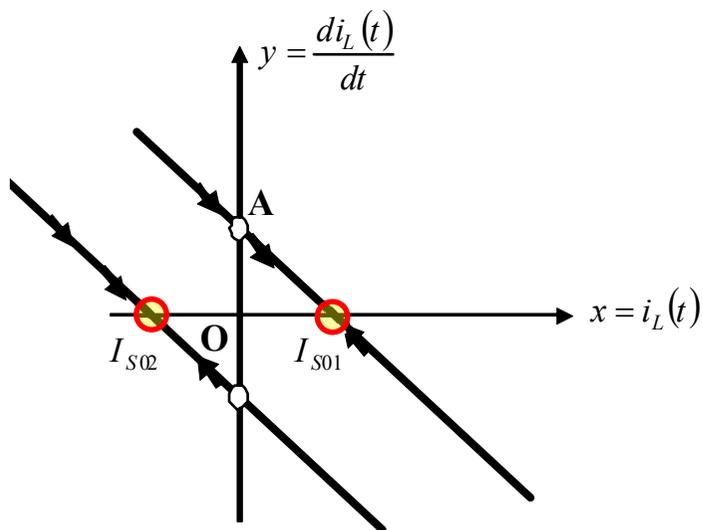
# 充电曲线、充电电流



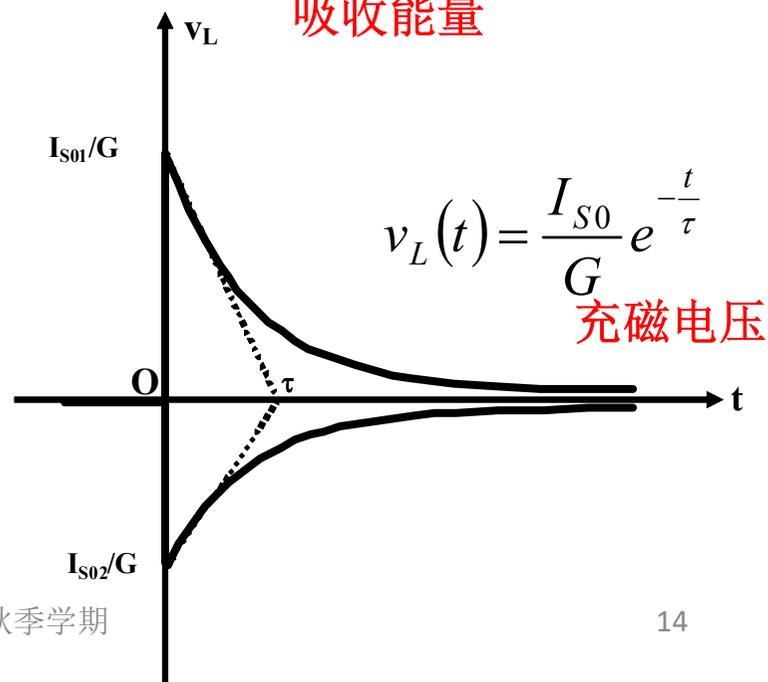
无论哪种情况，电源提供能量，电阻电容吸收能量



# 充磁曲线、充磁电压



无论哪种情况，电源提供能量，电阻电容吸收能量



充磁电压

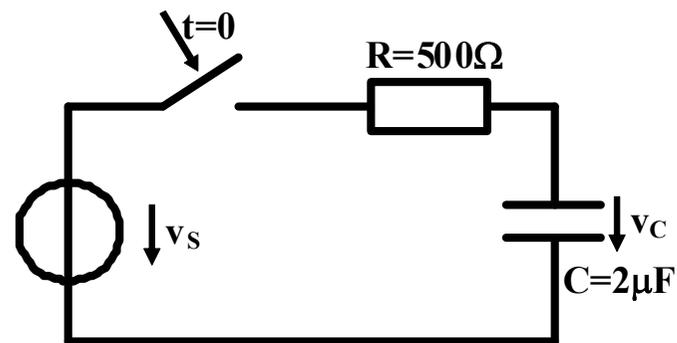
# 作业2 正弦激励

- 如图所示，**t=0**时刻开关闭合，正弦波电压激励源加载到一阶RC串联电路端口

$$v_s(t) = 2 \cos \omega_0 t$$

– 其中， $\omega_0 = 2\pi f_0$   $f_0 = 500\text{Hz}$

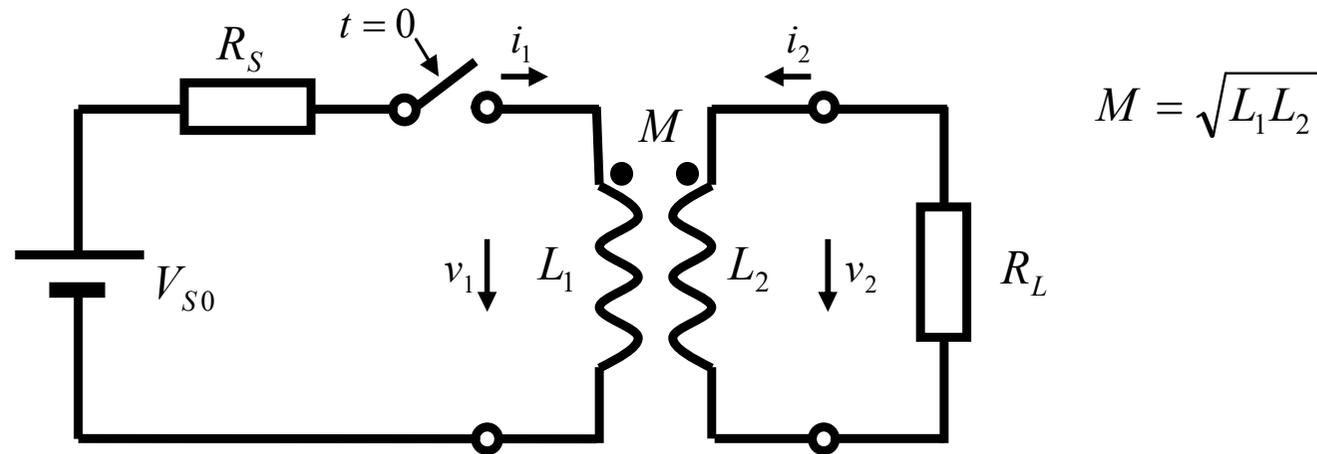
- 假设电容初始电压为0， $v_c(0)=0$ ，请给出电容电压时域表达式



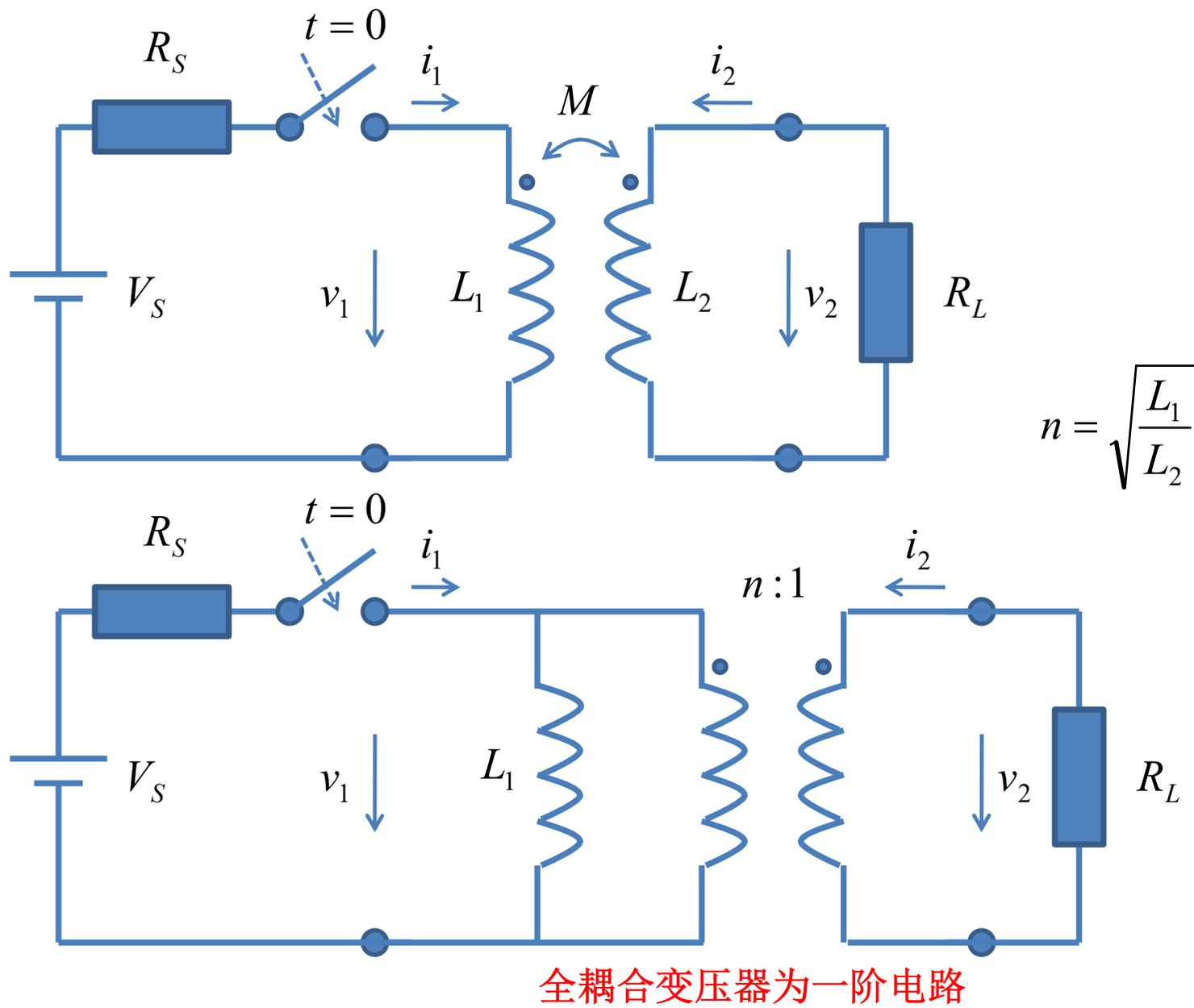
上上次习题课已讲  
后向欧拉法仿真后，用三要素法给出理论结果

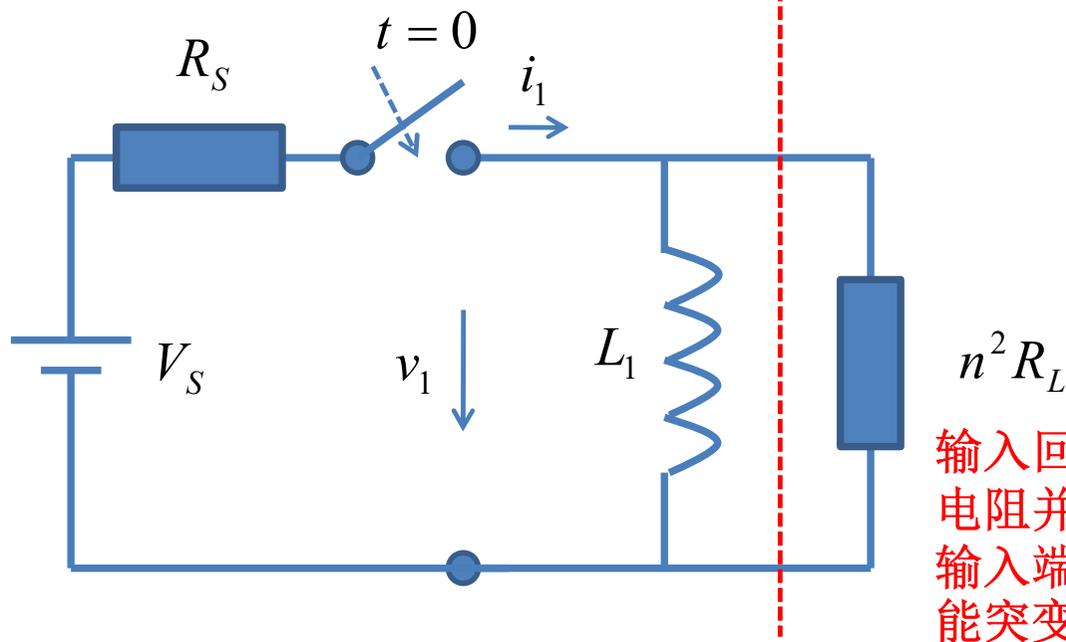
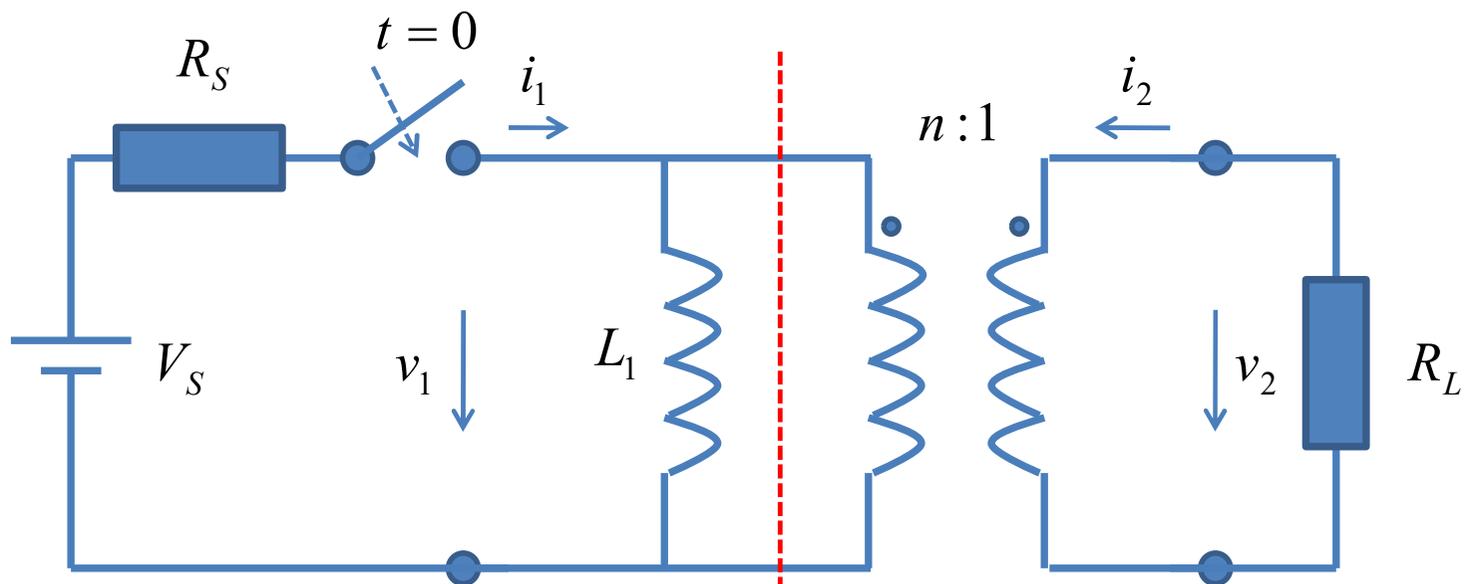
# 作业3 全耦合变压器是一阶元件

- **练习9.2.6** 如图E9.2.9所示，这是一个全耦合变压器电路。开关在 $t=0$ 时刻闭合，求变压器两个端口的电压时域表达式。



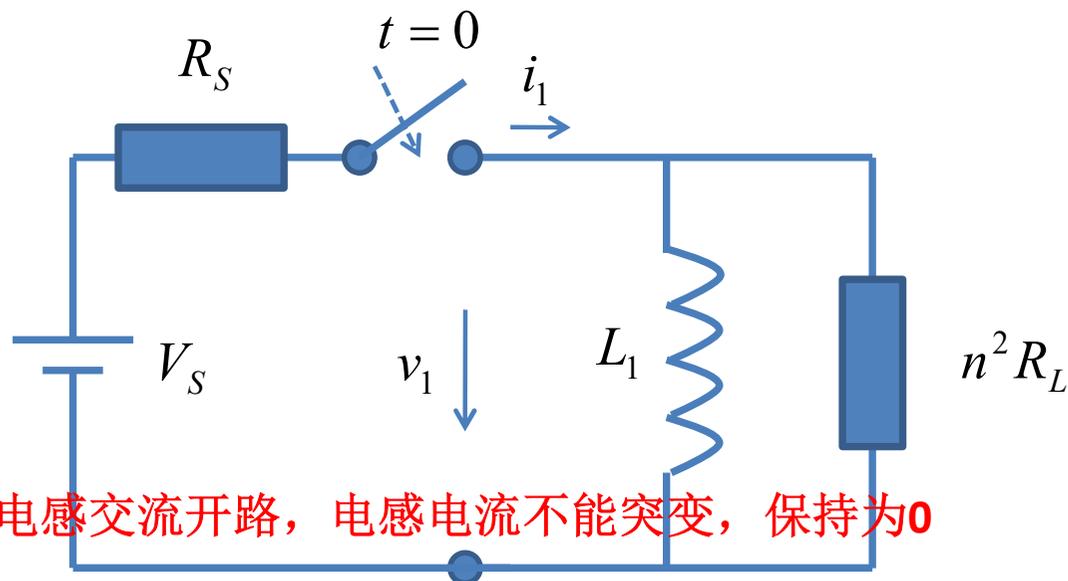
# 输入回路等效电路





输入回路等效电路为电感和电阻并联：由于负载作用，输入端口电流可以突变：不能突变的是什么？

# 三要素法



$$i_1(0^+) = \frac{V_S}{R_S + n^2 R_L}$$

开关闭合瞬间：电感交流开路，电感电流不能突变，保持为0

$$i_{1\infty}(t) = \frac{V_S}{R_S}$$

稳态：电感直流短路

$$\begin{aligned} i_1(t) &= i_{1\infty}(t) + (i_1(0^+) - i_{1\infty}(0^+))e^{-\frac{t}{\tau}} \\ &= \frac{V_S}{R_S} + \left( \frac{V_S}{R_S + n^2 R_L} - \frac{V_S}{R_S} \right) e^{-\frac{t}{\tau}} \quad U(t) \end{aligned}$$

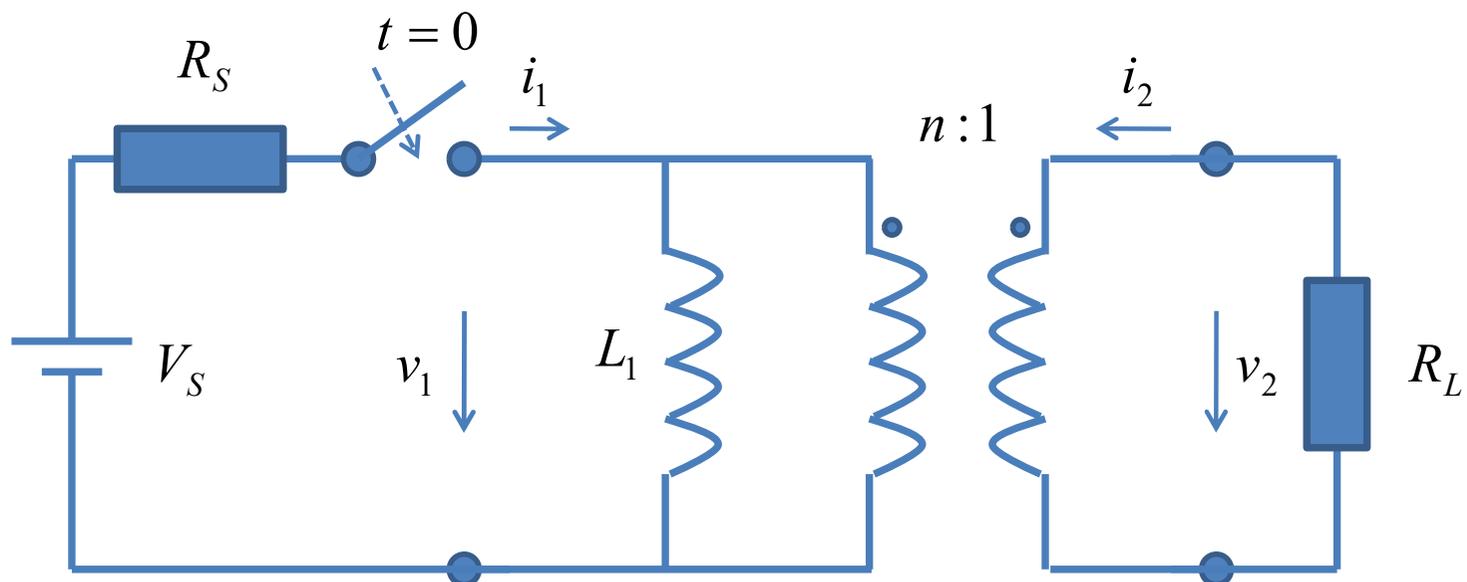
$$\tau = GL_1 = \left( \frac{1}{R_S} + \frac{1}{n^2 R_L} \right) L_1$$

$$= \left( \frac{1}{R_S} + \frac{L_2}{L_1 R_L} \right) L_1$$

$$= G_S L_1 + G_L L_2 = \tau_1 + \tau_2$$

$$\begin{aligned} v_1(t) &= v_{1\infty}(t) + (v_1(0^+) - v_{1\infty}(0^+))e^{-\frac{t}{\tau}} \\ &= \frac{n^2 R_L}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \quad U(t) \end{aligned}$$

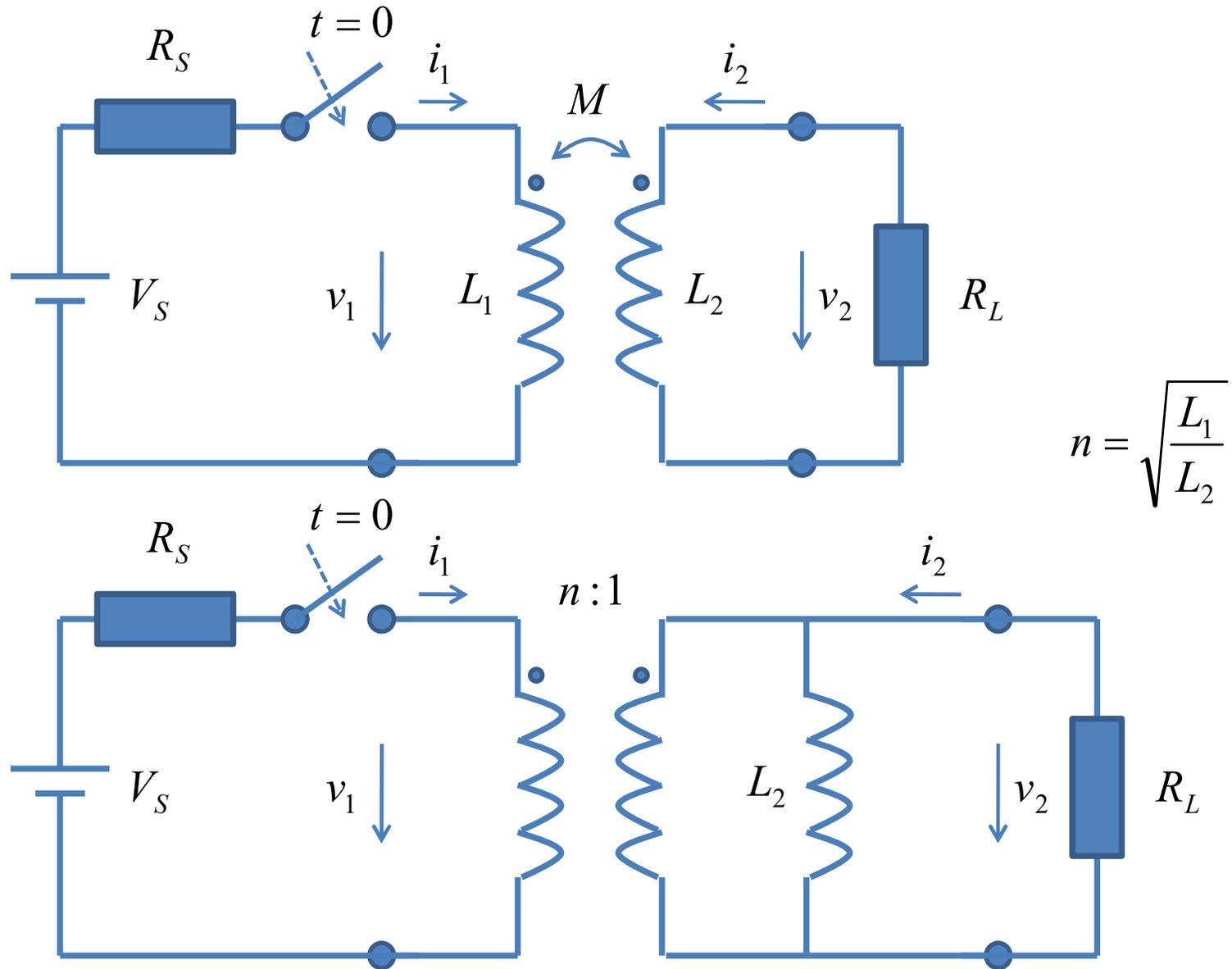
# 由输入回路压流直接获得输出回路压流

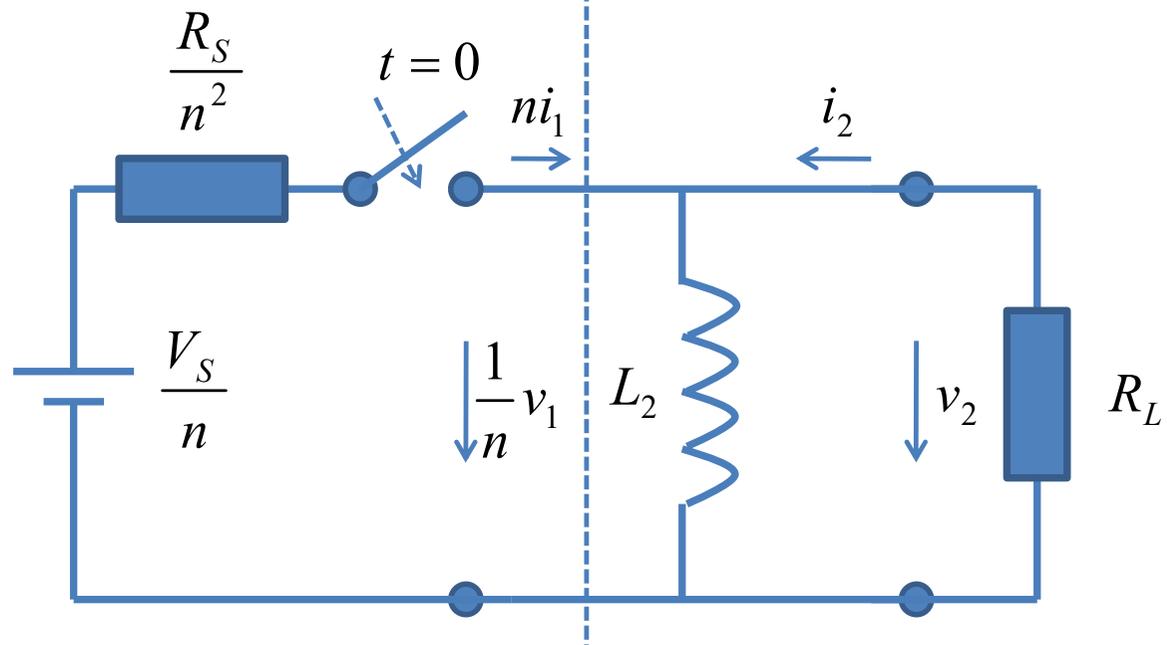
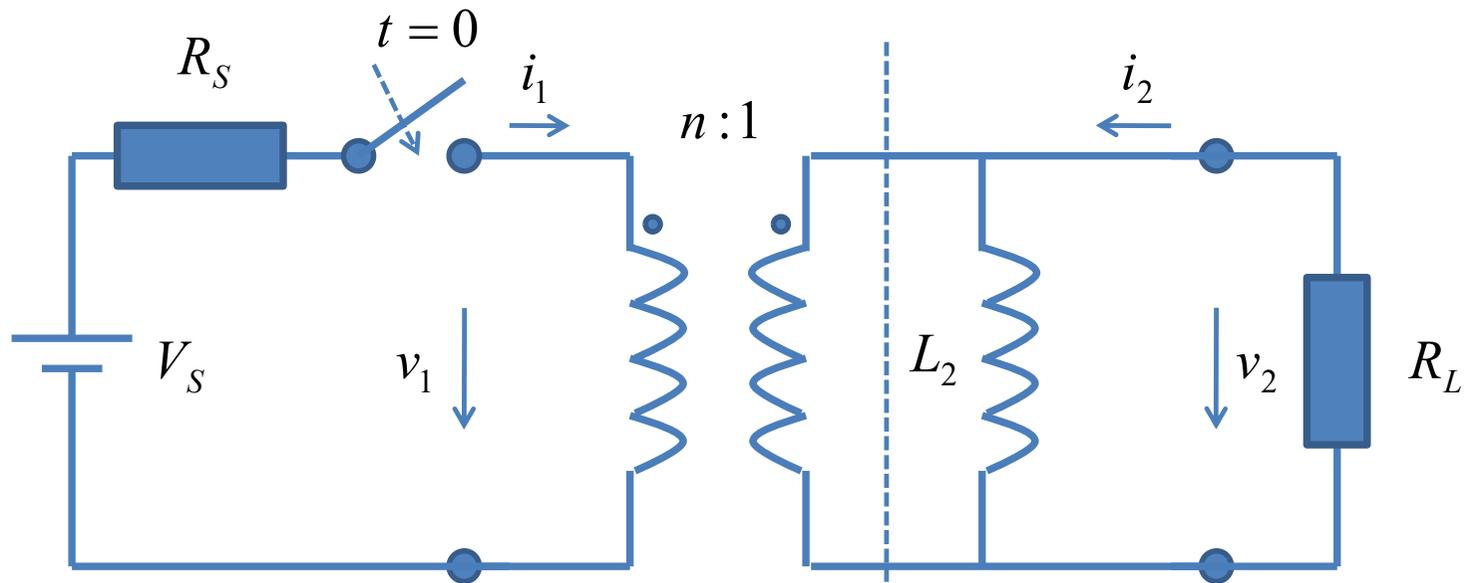


$$v_2(t) = \frac{1}{n} v_1(t) = \frac{nR_L}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \quad U(t)$$

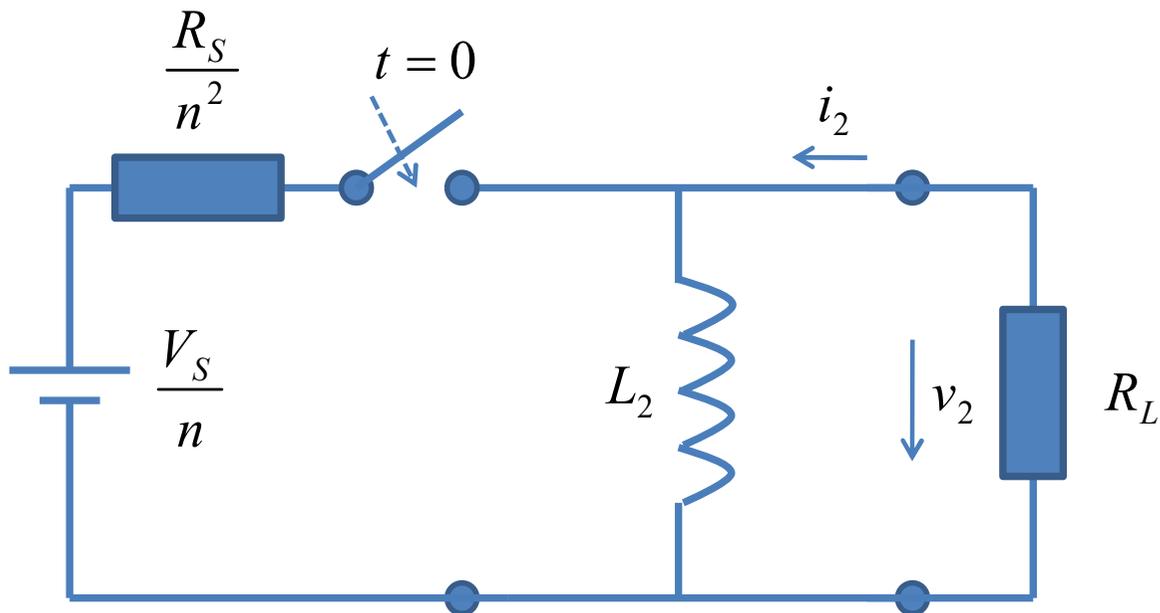
$$i_2(t) = -\frac{v_2(t)}{R_L} = -\frac{n}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \quad U(t)$$

# 也可在输出回路等效分析





# 三要素法



$$i_2(0^+) = -\frac{V_S/n}{R_S/n^2 + R_L}$$

$$i_{2\infty}(t) = 0$$

$$\tau = GL_2 = \left( \frac{n^2}{R_S} + \frac{1}{R_L} \right) L_2$$

$$= \left( \frac{L_1}{L_2 R_S} + \frac{1}{R_L} \right) L_2$$

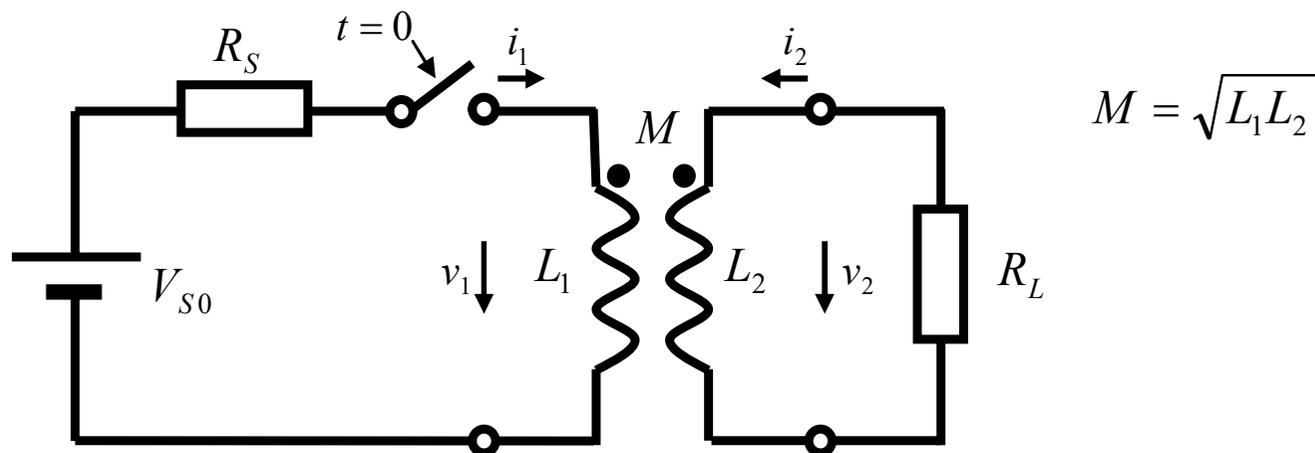
$$= G_S L_1 + G_L L_2 = \tau_1 + \tau_2$$

无论如何等效，时间常数是一阶LTI系统的特征参量，不会发生改变

无论如何等效，同一电量的最终表达式完全一致

$$i_2(t) = i_{2\infty}(t) + (i_2(0^+) - i_{2\infty}(0^+)) e^{-\frac{t}{\tau}} = -\frac{V_S/n}{R_S/n^2 + R_L} e^{-\frac{t}{\tau}} \quad U(t)$$

$$v_2(t) = v_{2\infty}(t) + (v_2(0^+) - v_{2\infty}(0^+)) e^{-\frac{t}{\tau}} = V_S/n \frac{R_L}{R_S/n^2 + R_L} e^{-\frac{t}{\tau}} \quad U(t)$$



$$v_1(t) = \frac{n^2 R_L}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \cdot U(t) \quad i_1(t) = \left( \frac{V_S}{R_S} + \left( \frac{V_S}{R_S + n^2 R_L} - \frac{V_S}{R_S} \right) e^{-\frac{t}{\tau}} \right) \cdot U(t)$$

$$v_2(t) = \frac{n R_L}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \cdot U(t) \quad i_2(t) = -\frac{n}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \cdot U(t)$$

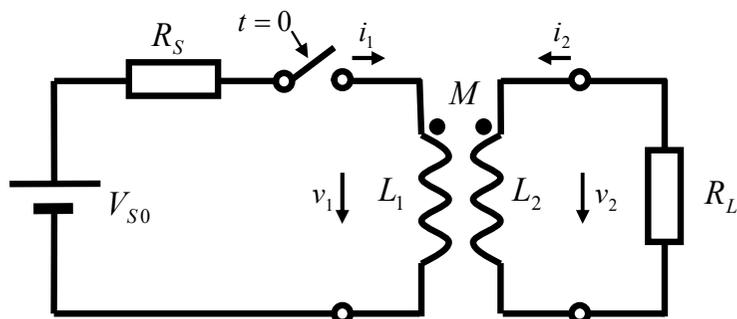
$$i_1(0^-) = 0 \quad i_1(0^+) = \frac{V_S}{R_S + n^2 R_L} \neq 0$$

$$i_2(0^-) = 0 \quad i_2(0^+) = -\frac{n V_S}{R_S + n^2 R_L} \neq 0$$

电感电流不是不能突变吗？

注意：这是二端口电感，具有阻抗变换作用，对于全耦合变压器，端口看入瞬间阻抗并非无穷大

# 非阶跃电流源充磁 电感储能不会突变



$$E_M(0^+) = 0 = E_M(0^-)$$

由于互感变压器吸收能量需要时间，故而存在瞬态过程

除非有冲激电压，无穷大功率，才能完成能量从电源到电感的瞬间转移。

$$M = \sqrt{L_1 L_2}$$

$$\begin{aligned} p_M(t) &= v_1(t)i_1(t) + v_2(t)i_2(t) \\ &= \frac{n^2 R_L}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \cdot \left( \frac{V_S}{R_S} + \left( \frac{V_S}{R_S + n^2 R_L} - \frac{V_S}{R_S} \right) e^{-\frac{t}{\tau}} \right) \cdot U(t) \\ &\quad + \frac{n R_L}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \cdot \left( -\frac{n}{R_S + n^2 R_L} V_S e^{-\frac{t}{\tau}} \right) \cdot U(t) \\ &= \frac{V_S^2}{R_S} \frac{n^2 R_L}{R_S + n^2 R_L} \left( e^{-\frac{t}{\tau}} - e^{-\frac{2t}{\tau}} \right) \cdot U(t) \end{aligned}$$

$$E_M(t) = \int_{-\infty}^t p_M(t) dt = \int_0^t \frac{V_S^2}{R_S} \frac{n^2 R_L}{R_S + n^2 R_L} \left( e^{-\frac{t}{\tau}} - e^{-\frac{2t}{\tau}} \right) dt = \frac{V_S^2}{R_S} \frac{n^2 R_L}{R_S + n^2 R_L} \left( -\tau \cdot \left( e^{-\frac{t}{\tau}} - 1 \right) + \frac{\tau}{2} \left( e^{-\frac{2t}{\tau}} - 1 \right) \right)$$

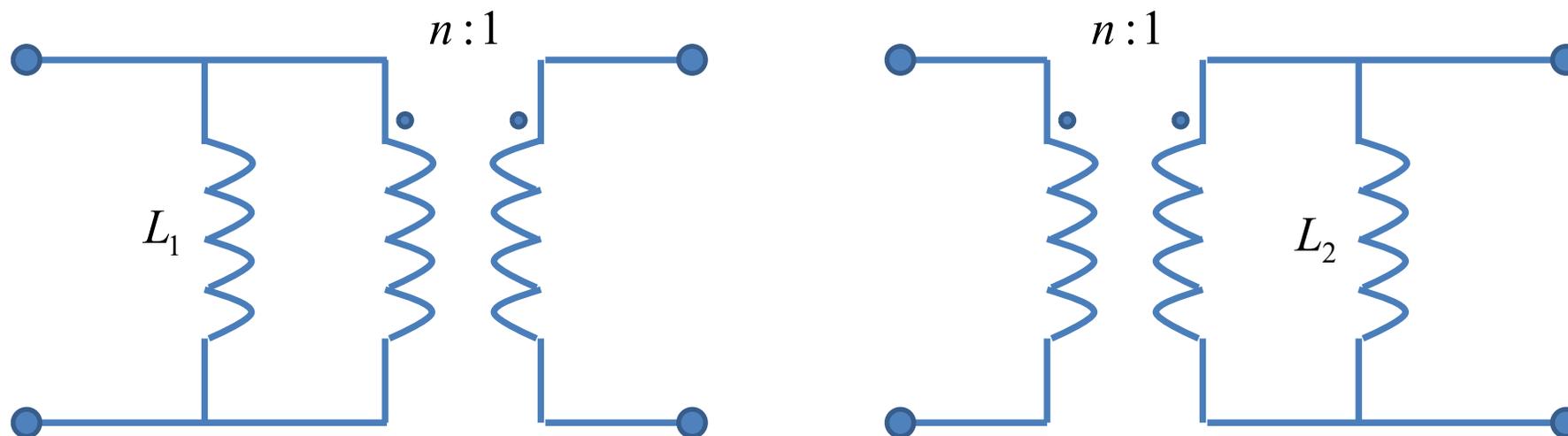
$$E_M(\infty) = \frac{V_S^2}{R_S} \frac{n^2 R_L}{R_S + n^2 R_L} \frac{\tau}{2} = \frac{V_S^2}{R_S} \frac{L_1 R_L}{L_2 R_S + L_1 R_L} \frac{G_S L_1 + G_L L_2}{2} = \frac{1}{2} L_1 \frac{V_S^2}{R_S^2} = \frac{1}{2} L_1 I_{1\infty}^2$$

$$p_M(0^+) = 0 = p_M(0^-)$$

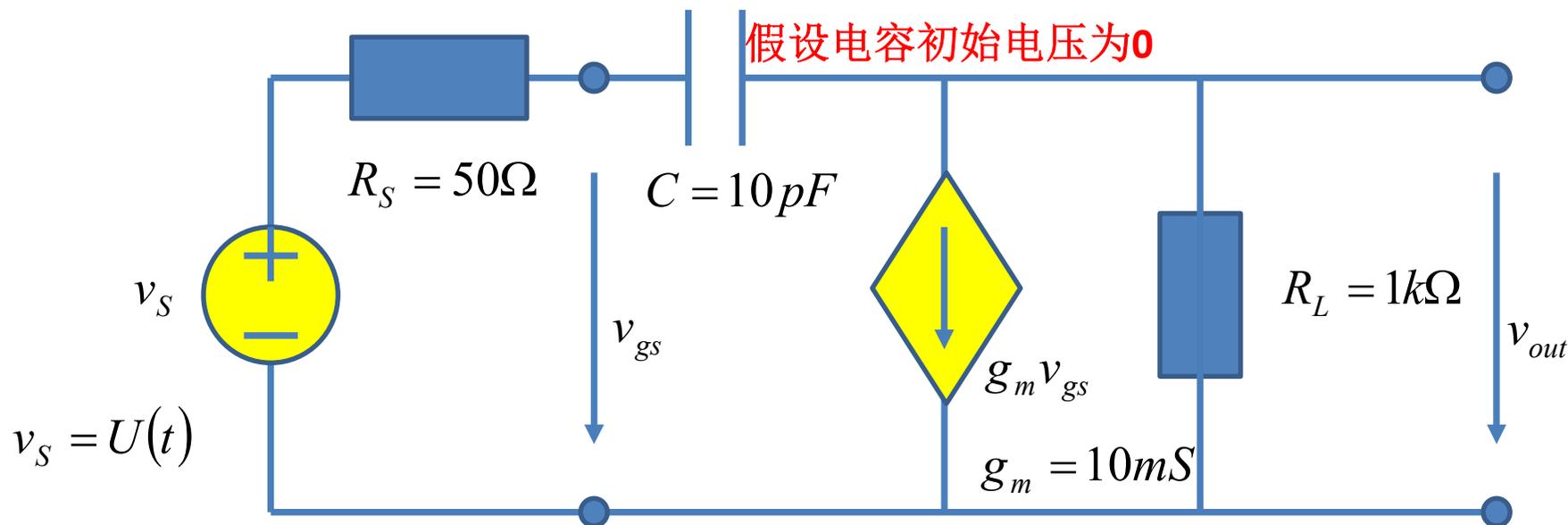
**t=0**瞬间，电感无穷大，视为理想变压器，全耦合变压器在**t=0**瞬间是理想传输系统：端口**1**吸收的功率在端口**2**瞬间全部释放出去，变压器本身没有吸收功率

# 全耦合变压器

- 储能在两个端口随意互换
  - 自行练习：开关闭合稳定后，开关又断开，请分析变压器两端电压变化曲线？

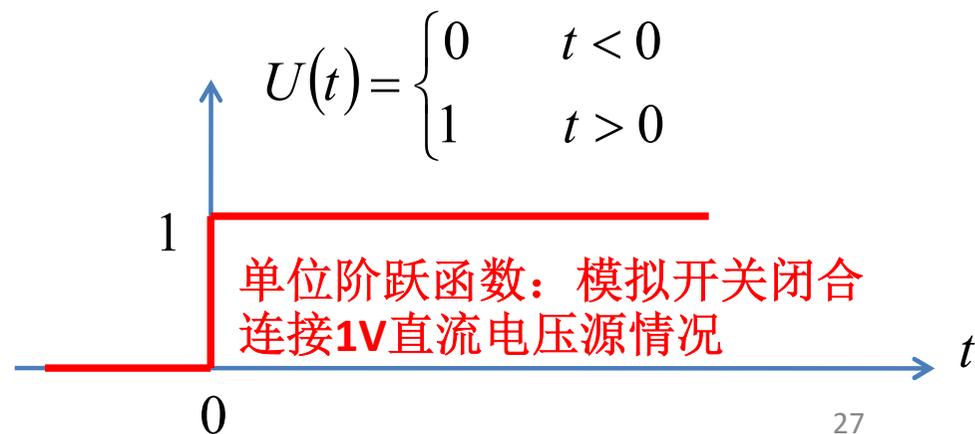


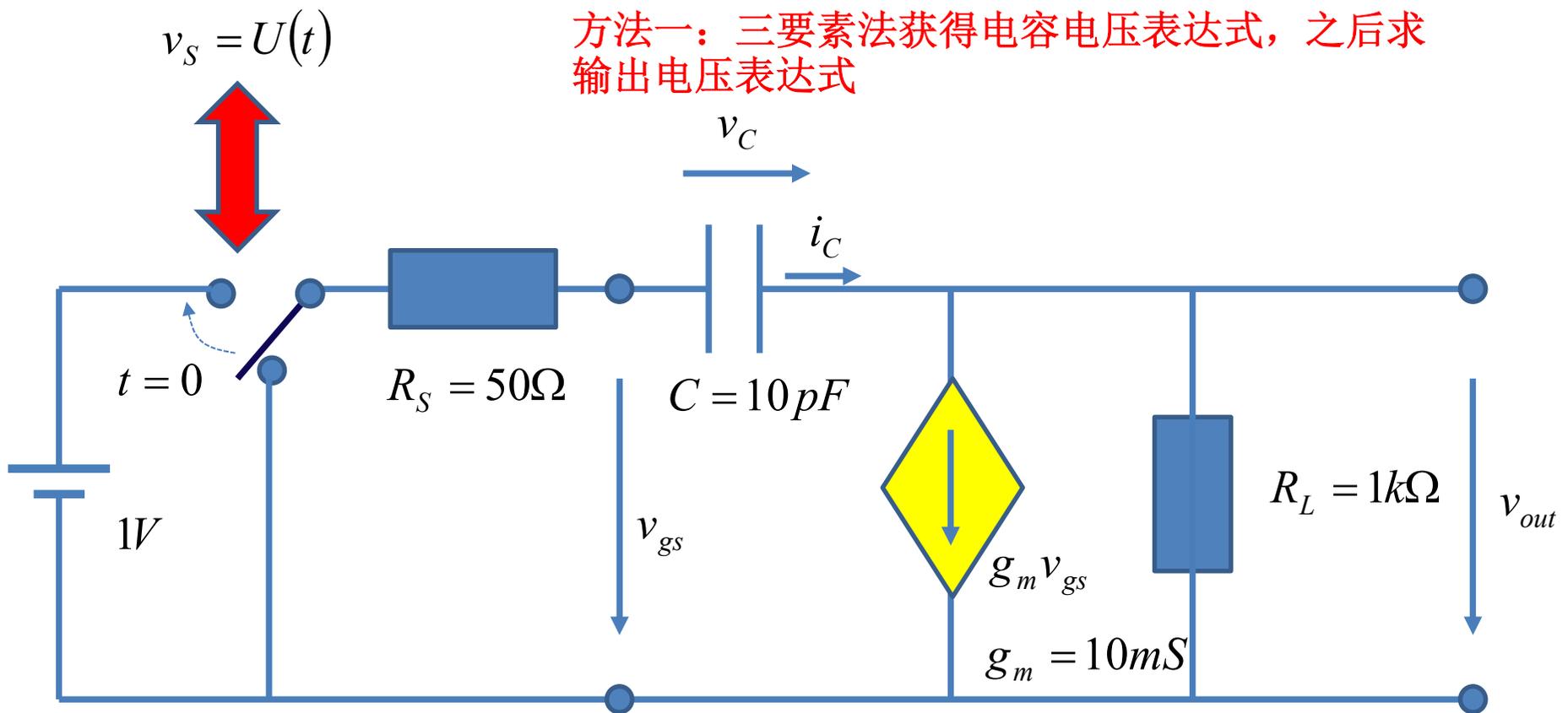
# 作业4 三要素法适用一阶RC电路



方法一、用三要素法获得电容时域波形  $v_C(t)$ ，进而获得输出电压时域波形  $v_{out}(t)$ ，表达式和曲线

方法二（选作）、用三要素法直接获得输出电压时域波形  $v_{out}(t)$





方法一：三要素法获得电容电压表达式，之后求输出电压表达式

$$v_C(0^+) = v_C(0^-) = 0$$

$$v_{C\infty}(t) = ?$$

$$i_{C\infty}(t) = 0$$

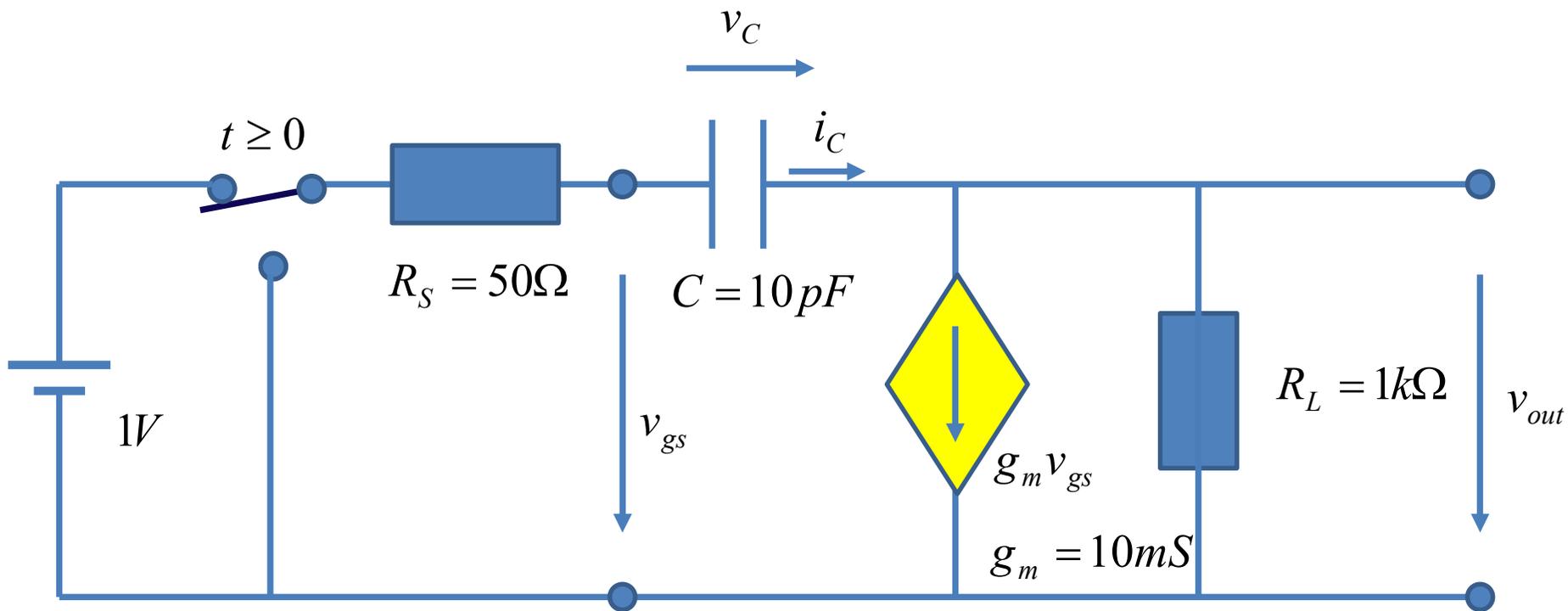
**t=∞则直流电容开路**

电容上的电压正常情况下不会跳变：它是连续的

$$v_{gs\infty}(t) = V_{S0} = 1(V)$$

$$g_m v_{gs\infty}(t) = 10mS \cdot 1V = 10mA$$

$$v_{out\infty}(t) = -(g_m v_{gs\infty}(t))R_L = -10mA \cdot 1k\Omega = -10V$$



$$v_{gs\infty}(t) = 1(V)$$

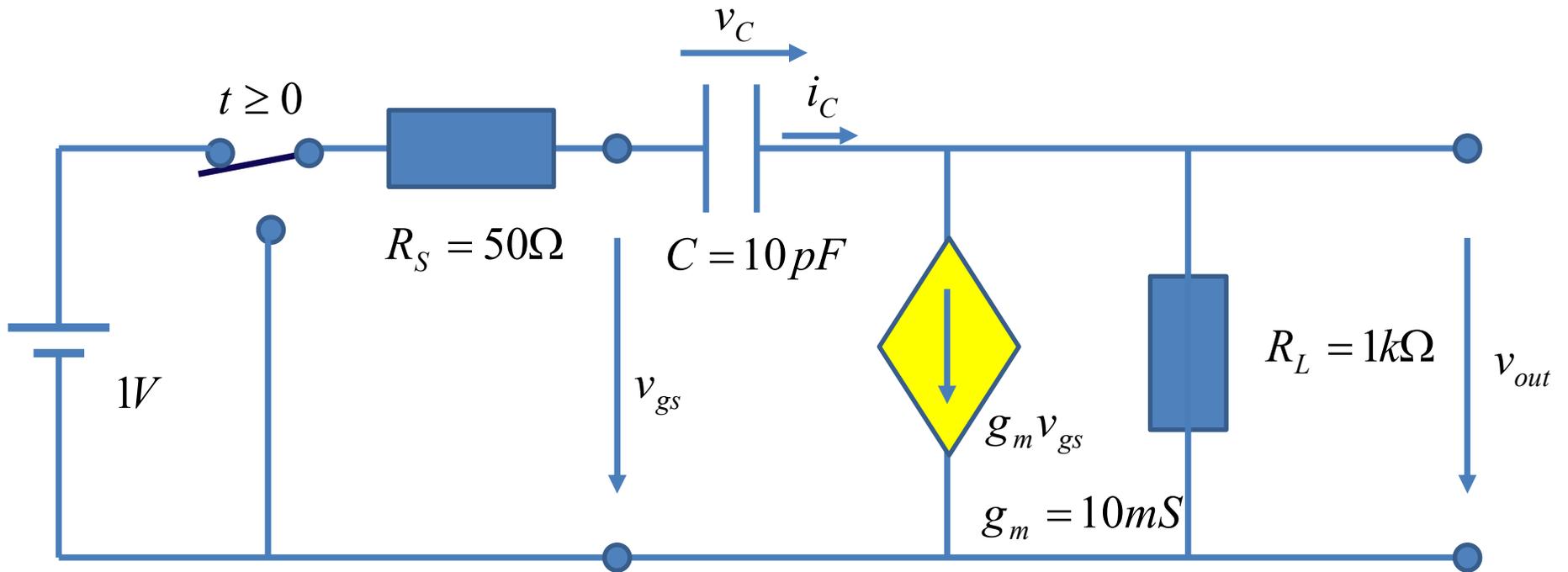
$$v_{out\infty}(t) = -10(V)$$

$$v_{C\infty}(t) = v_{gs\infty}(t) - v_{out\infty}(t) = 11(V)$$

$$\tau = ? R_{eq} C$$

$$\begin{aligned} R_{eq} &= R_S + R_L + g_m R_S R_L \\ &= 50 + 1000 + 10 \times 10^{-3} \cdot 50 \cdot 1000 \\ &= 1550(\Omega) \end{aligned}$$

$$\tau = R_{eq} C = 1550 \times 10 \times 10^{-12} = 15.5(ns)$$



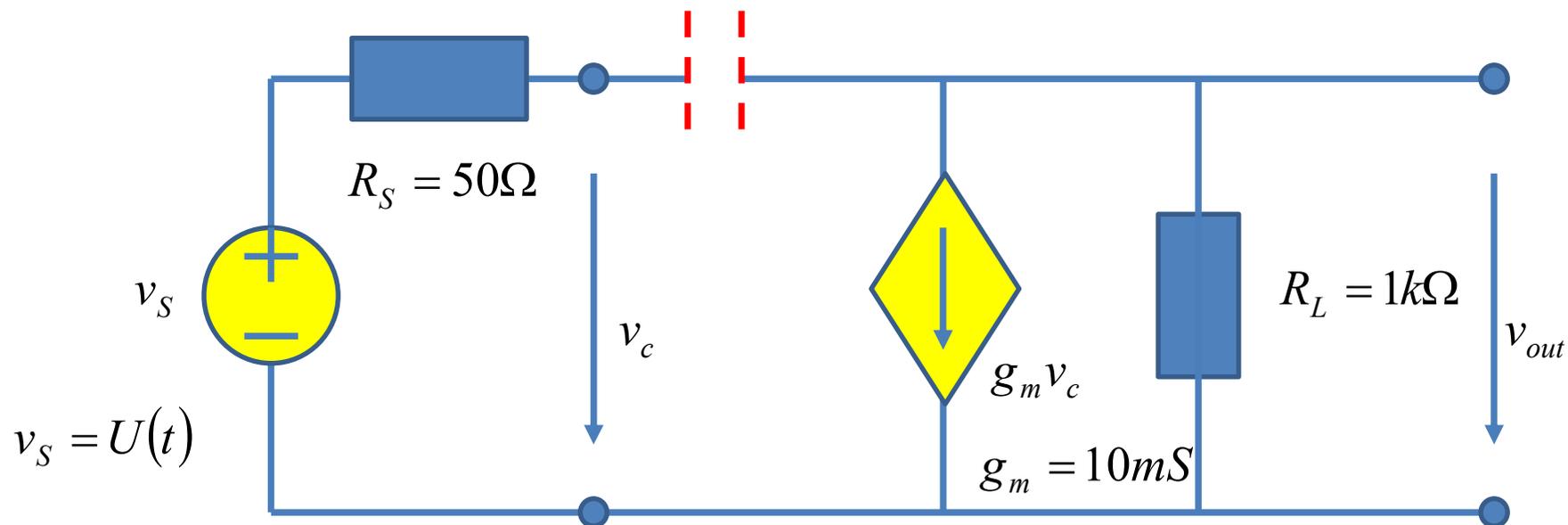
$$v_C(0^+) = 0 \quad v_{C\infty}(t) = 11(V) \quad \tau = 15.5(ns)$$

$$v_C(t) = v_{C\infty}(t) + (v_C(0^+) - v_{C\infty}(0^+))e^{-\frac{t}{\tau}} = 11 \left( 1 - e^{-\frac{t}{15.5 \times 10^{-9}}} \right)$$

$$i_C(t) = C \frac{dv_C(t)}{dt} = 7e^{-\frac{t}{15.5 \times 10^{-9}}} (mA)$$

$$v_{out}(t) = v_S(t) - i_C(t)R_S - v_C(t) = -10 + 10.65e^{-\frac{t}{15.5 \times 10^{-9}}} (V) \quad (t \geq 0)$$

# 电容的影响



上学期电阻电路结果  
输出是输入的即时响应：无记忆

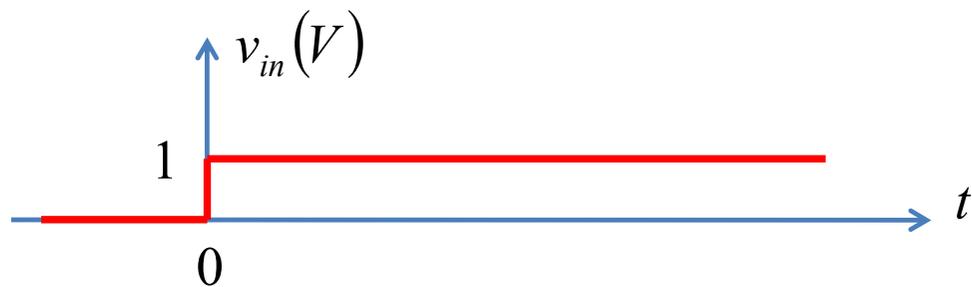
$$v_{out}(t) = -g_m R_L v_S(t) = -10U(t)$$

$$v_{out}(t) = \left( -10 + 10.65e^{-\frac{t}{15.5 \times 10^{-9}}} \right) U(t)$$

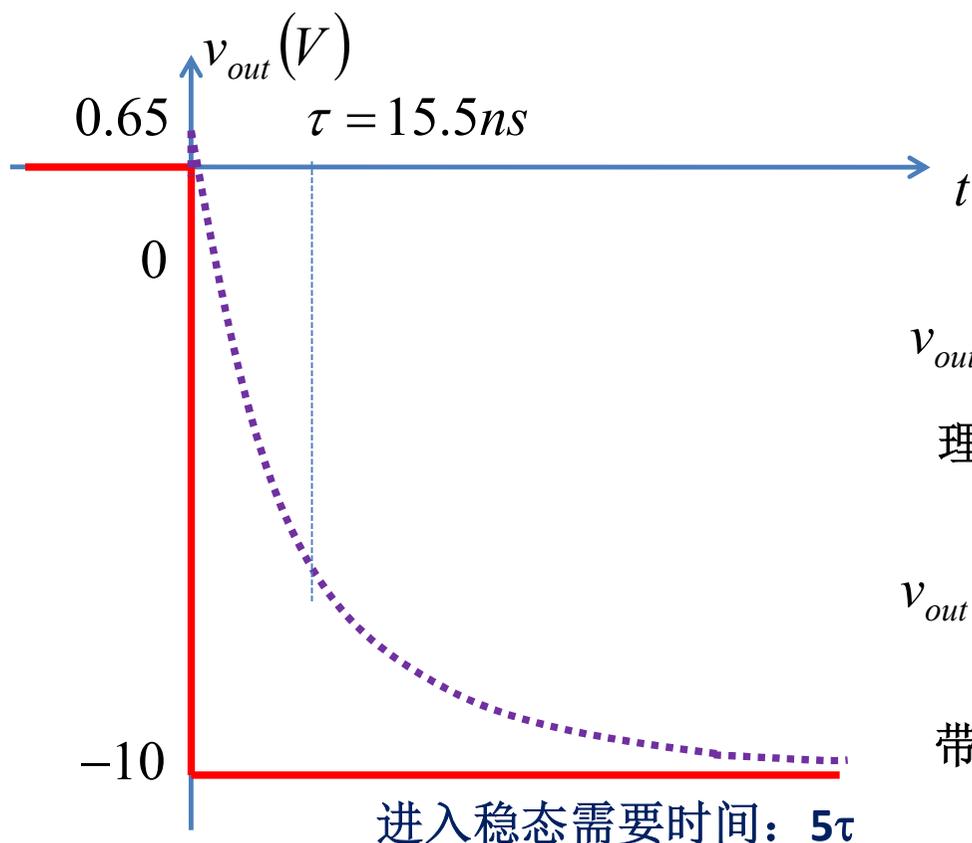
稳态响应 瞬态响应

本学期动态电路结果  
=稳态+瞬态：有记忆  
在阶跃电压激励下：  
稳态响应就是电阻电路结果  
(电容开路，电感短路结果)

# 电容的影响：产生延时



$$v_{in}(t) = U(t)$$



输出想要达到理想的稳态，需要等待一段时间：这个等待时间一般称为延时

$$v_{out}(t) = -10U(t)$$

理想反相放大器输出响应

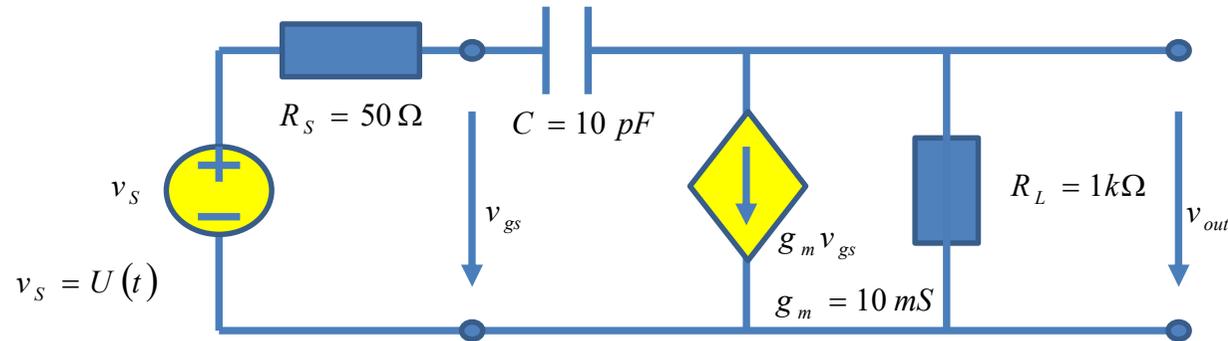
$$v_{out}(t) = \left( -10 + 10.65e^{-\frac{t}{15.5 \times 10^{-9}}} \right) U(t)$$

带跨接寄生电容的反相放大器输出响应

## 方法2：直接三要素

$$v_o(t) = v_{o\infty}(t) + (v_o(0^+) - v_{o\infty}(0^+))e^{-\frac{t}{\tau}}$$

$$(t \geq 0)$$



$$\tau = CR_{eq} = C(R_S + R_L + g_m R_S R_L) = 15.5ns$$

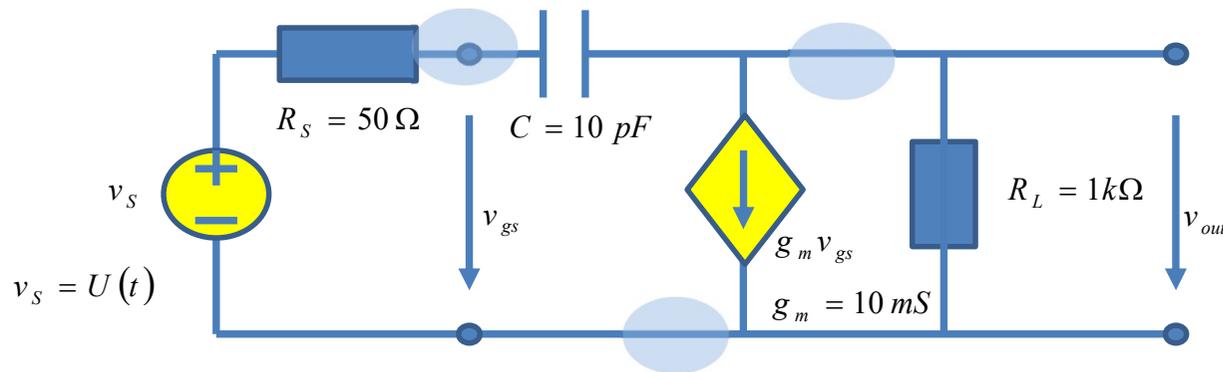
$$v_{o\infty}(t) = -g_m R_L U(t) = -10U(t) \quad v_{o\infty}(0^+) = -g_m R_L = -10$$

$$v_o(0^+) = \frac{\frac{1}{g_m} \parallel R_L}{R_S + \frac{1}{g_m} \parallel R_L} \cdot 1 = \frac{\frac{1}{g_m + G_L}}{R_S + \frac{1}{g_m + G_L}} = \frac{R_L}{R_{eq}} = 0.645$$

$$v_o(t) = -10 + 10.645e^{-\frac{t}{\tau}} \quad (t \geq 0)$$

# 方法3：微分方程求解

如果掌握了三要素法，就不要采用微分方程求解  
这里列写这个过程，只是说明晶体管放大器跨接电容的作用！



结点电压法实质：以两个结点电压为未知量，列写两个结点的KCL方程

$$\frac{v_S - v_{gs}}{R_S} = i_C = C \frac{dv_C}{dt} = C \frac{d}{dt}(v_{gs} - v_{out})$$

$$C \frac{d}{dt}(v_{gs} - v_{out}) = i_C = g_m v_{gs} + \frac{v_{out}}{R_L}$$

两个结点电压 $v_{gs}$ 和 $v_{out}$ 为未知量  
两个结点的KCL方程

$$\frac{v_S - v_{gs}}{R_S} = i_C = C \frac{dv_C}{dt} = C \frac{d}{dt}(v_{gs} - v_{out})$$

## 关于 $v_{out}$ 的电路方程

$$C \frac{d}{dt}(v_{gs} - v_{out}) = i_C = g_m v_{gs} + \frac{v_{out}}{R_L}$$



$$\frac{v_S - v_{gs}}{R_S} = i_C = g_m v_{gs} + \frac{v_{out}}{R_L}$$



$$v_{gs} = \frac{\frac{v_S}{R_S} - \frac{v_{out}}{R_L}}{g_m + \frac{1}{R_S}}$$



$$C \frac{d}{dt} \left( \frac{\frac{v_S}{R_S} - \frac{v_{out}}{R_L}}{g_m + \frac{1}{R_S}} - v_{out} \right) = g_m \frac{\frac{v_S}{R_S} - \frac{v_{out}}{R_L}}{g_m + \frac{1}{R_S}} + \frac{v_{out}}{R_L}$$



$$(R_S + R_L + g_m R_S R_L) C \frac{dv_{out}}{dt} + v_{out} = R_L C \frac{dv_S}{dt} - g_m R_L v_S$$

$$\frac{dv_{out}}{dt} = -\frac{1}{R_{eq} C} v_{out} + \frac{R_L}{R_{eq}} \frac{dv_S}{dt} - \frac{g_m R_L}{R_{eq} C} v_S$$

$$\frac{dx(t)}{dt} = -\frac{1}{\tau} x(t) + s(t)$$

$$(R_S + R_L + g_m R_S R_L)C \frac{dv_{out}}{dt} + v_{out} = R_L C \frac{dv_S}{dt} - g_m R_L v_S \quad v_S(t) = U(t)$$

$$\tau \frac{dv_{out}(t)}{dt} + v_{out}(t) = R_L C \cdot \delta(t) - g_m R_L \cdot U(t) \quad \text{对比}$$

省略中间的积分过程

$$v_{out}(t) = R_L C \cdot h_{RC}(t) - g_m R_L \cdot g_{RC}(t)$$

$$= R_L C \cdot \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t) - g_m R_L \cdot \left(1 - e^{-\frac{t}{\tau}}\right) \cdot U(t)$$

$$v_{out}(t) = \left[ R_L C \cdot \frac{1}{R_{eq} C} e^{-\frac{t}{\tau}} - g_m R_L \cdot \left(1 - e^{-\frac{t}{\tau}}\right) \right] \cdot U(t)$$

$$= \left[ -g_m R_L + \left( \frac{R_L}{R_{eq}} - (-g_m R_L) \right) \cdot e^{-\frac{t}{\tau}} \right] \cdot U(t)$$

$$= \left[ -10 + (0.65 - (-10)) \cdot e^{-\frac{t}{\tau}} \right] \cdot U(t)$$

稳态响应 初值

指数衰减

$$RC \frac{dv_C(t)}{dt} + v_C(t) = v_S(t)$$

一阶RC电路

电阻电压+电容电压=电源电压

$$h_{RC,lowpass}(t) = \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t)$$

$$g_{RC,lowpass}(t) = \left(1 - e^{-\frac{t}{\tau}}\right) \cdot U(t)$$

虽然解形式一致，但问题变得复杂化了

不论是冲激、阶跃、正弦、方波，均可采用三要素法

跨接电容：低通+高通

# 方法4 时频对应法

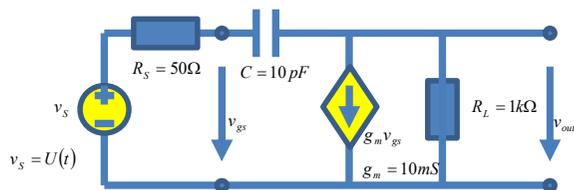
频域分析

波特图

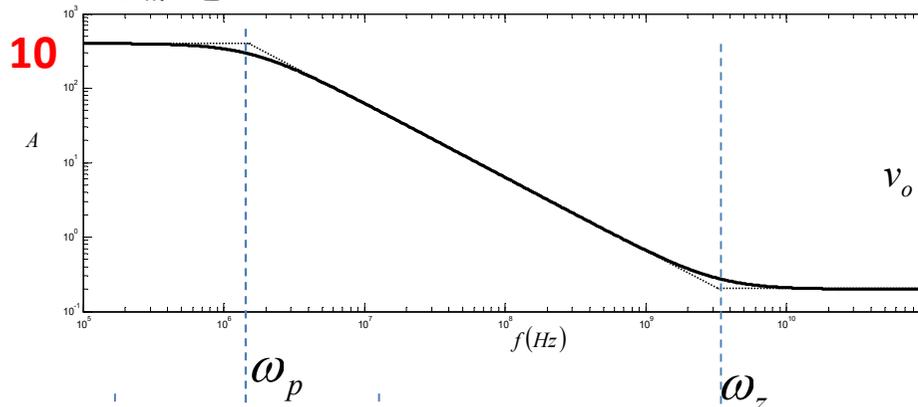
$$\frac{\dot{V}_{out}}{\dot{V}_S} = \frac{R_L j\omega C - g_m R_L}{1 + j\omega C(R_S + R_L + g_m R_S R_L)} = -g_m R_L \frac{1 - j\omega \frac{C}{g_m}}{1 + j\omega C(R_S + R_L + g_m R_S R_L)}$$

$$= -g_m R_L \frac{1 - \frac{j\omega}{\omega_z}}{1 + \frac{j\omega}{\omega_p}}$$

可用结点电压法等方法获得传递函数



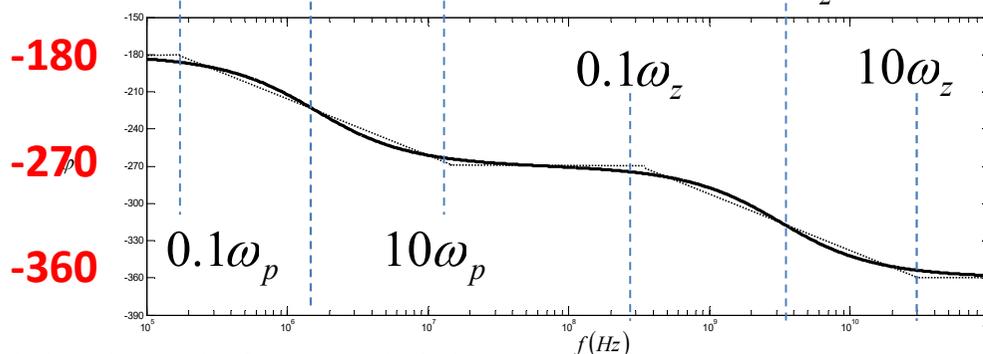
$$v_{o\infty} = -g_m R_L$$



$$v_o(0^+) = \frac{R_L}{R_{eq}}$$

0.645

$g_m R_L$



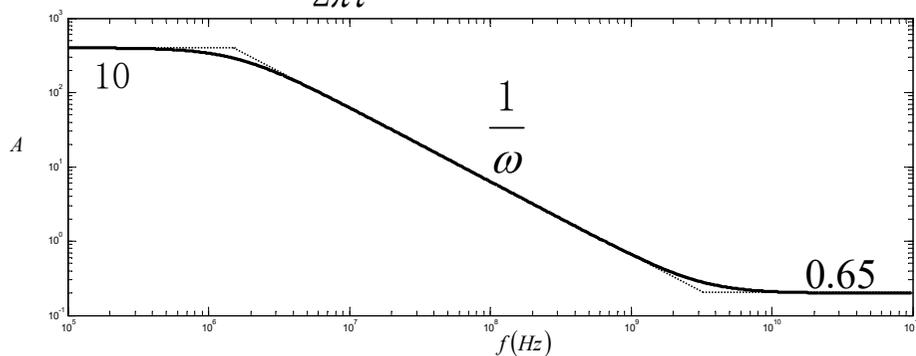
# 时频对应关系

$$H(j\omega) = \frac{\dot{V}_{out}}{\dot{V}_s} = -g_m R_L \frac{1 - j\omega \frac{C}{g_m}}{1 + j\omega C(R_S + R_L + g_m R_S R_L)} = -g_m R_L \frac{1 - j\omega \frac{C}{g_m}}{1 + j\omega C R_{eq}}$$

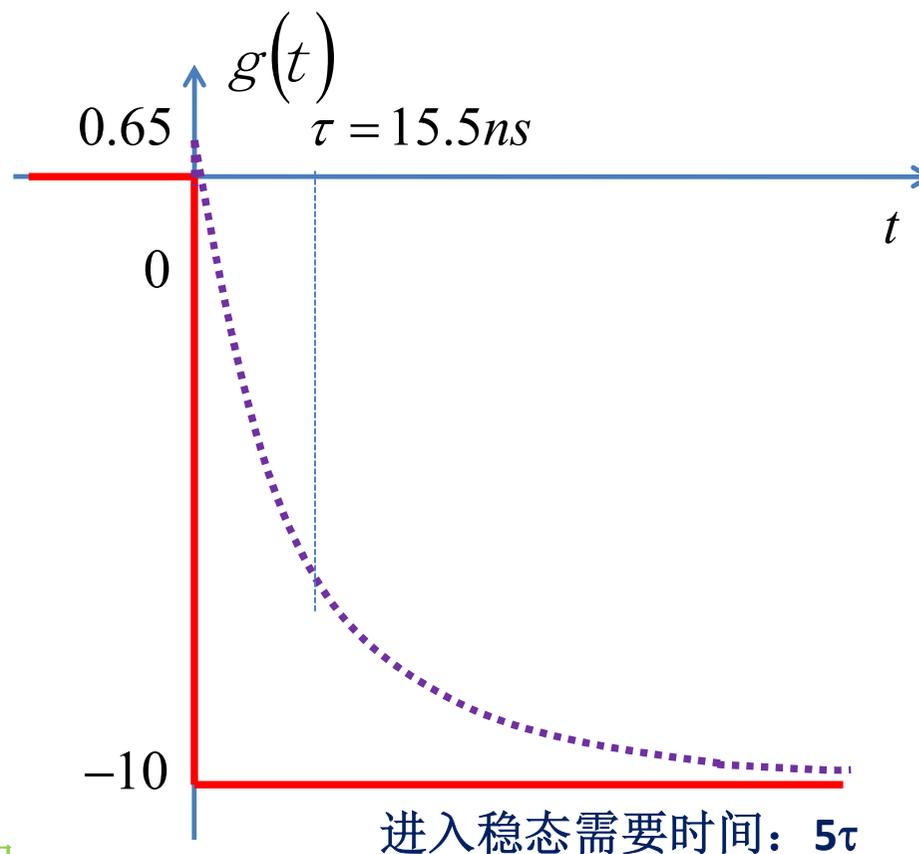
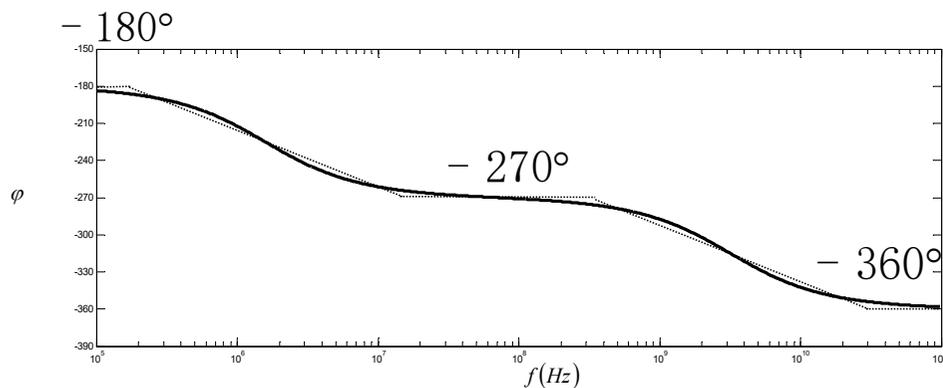
是否可以直接从频域传递函数获得阶跃或冲激响应呢？

$$g(t) = \left( -10 + 10.65e^{-\frac{t}{15.5 \times 10^{-9}}} \right) U(t) = \left[ -g_m R_L + \left( \frac{R_L}{R_{eq}} - (-g_m R_L) \right) \cdot e^{-\frac{t}{\tau}} \right] \cdot U(t)$$

$$f_0 = \frac{1}{2\pi\tau} = 10.27 \text{ MHz}$$



$$10 \times f_0 = 0.65 \times f_z$$



图属教材例9.2.10数值结果，和本题结果不匹配

# 时频对应关系表

典型  
一阶  
高低通

非典型  
一阶  
系统

$h(t)$	$H(s)$	
$\delta(t)$	1	直通电路
$U(t)$	$\frac{1}{s}$	纯电容
$e^{-\omega_0 t} \cdot U(t)$	$\frac{1}{s + \omega_0}$	RC电路

其实是《信号与系统》中的拉普拉斯变换，不要求掌握，只需了解即可

# 一阶低通和一阶高通

$$H(j\omega) = A_0 \frac{1}{1+j\omega\tau} \stackrel{\omega_0 = \frac{1}{\tau}}{=} A_0 \frac{\omega_0}{\omega_0 + j\omega} \stackrel{s=j\omega}{=} A_0 \frac{\omega_0}{s + \omega_0}$$

$$h(t) = A_0 \omega_0 e^{-\omega_0 t} U(t) = A_0 \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t)$$

变换表

$$\frac{1}{s} H(s) = A_0 \frac{1}{s} \frac{\omega_0}{s + \omega_0} = A_0 \left( \frac{1}{s} - \frac{1}{s + \omega_0} \right)$$

$$g(t) = A_0 (1 - e^{-\omega_0 t}) U(t) = A_0 \left( 1 - e^{-\frac{t}{\tau}} \right) \cdot U(t)$$

$$H(j\omega) = A_0 \frac{j\omega\tau}{1+j\omega\tau} \stackrel{\omega_0 = \frac{1}{\tau}}{=} A_0 \frac{j\omega}{\omega_0 + j\omega} \stackrel{s=j\omega}{=} A_0 \frac{s}{s + \omega_0} = A_0 - A_0 \frac{\omega_0}{s + \omega_0}$$

$$h(t) = A_0 \delta(t) - A_0 \omega_0 e^{-\omega_0 t} \cdot U(t) = A_0 \delta(t) - A_0 \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t)$$

$$\frac{1}{s} H(s) = A_0 \frac{1}{s} \frac{s}{s + \omega_0} = A_0 \frac{1}{s + \omega_0}$$

$$g(t) = A_0 e^{-\omega_0 t} \cdot U(t) = A_0 e^{-\frac{t}{\tau}} \cdot U(t)$$

# 任意一阶系统

$$H(s) = \frac{\alpha s + \beta}{s + \omega_0} = \frac{\alpha(s + \omega_0) - \alpha\omega_0 + \beta}{s + \omega_0} = \alpha + (\beta - \alpha\omega_0) \frac{1}{s + \omega_0}$$

$$h(t) = \alpha \cdot \delta(t) + (\beta - \alpha\omega_0) e^{-\omega_0 t} \cdot U(t)$$

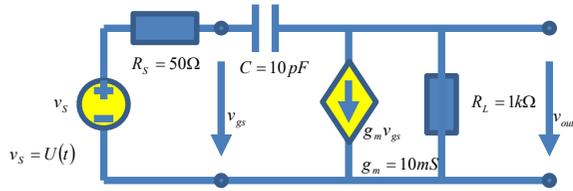
$$\frac{1}{s} H(s) = \frac{1}{s} \frac{\alpha s + \beta}{s + \omega_0} = \frac{\beta}{\omega_0} \frac{1}{s} + \left( \alpha - \frac{\beta}{\omega_0} \right) \frac{1}{s + \omega_0}$$

$$g(t) = \left( \frac{\beta}{\omega_0} + \left( \alpha - \frac{\beta}{\omega_0} \right) e^{-\omega_0 t} \right) \cdot U(t)$$

$$\begin{aligned} \frac{d}{dt} g(t) &= \left( \frac{\beta}{\omega_0} + \left( \alpha - \frac{\beta}{\omega_0} \right) e^{-\omega_0 t} \right) \cdot \delta(t) + \left( -\omega_0 \left( \alpha - \frac{\beta}{\omega_0} \right) e^{-\omega_0 t} \right) \cdot U(t) \\ &= \alpha \cdot \delta(t) + (\beta - \alpha\omega_0) e^{-\omega_0 t} \cdot U(t) = h(t) \end{aligned}$$

变换表

# 时频对应关系



$$H(j\omega) = \frac{\dot{V}_{out}}{\dot{V}_s} = -g_m R_L \frac{1 - j\omega \frac{C}{g_m}}{1 + j\omega C (R_s + R_L + g_m R_s R_L)} = -g_m R_L \frac{1 - j\omega \frac{C}{g_m}}{1 + j\omega C R_{eq}}$$

$$\frac{1}{s} H(s) = -g_m R_L \frac{1}{s} \frac{1 - s \frac{C}{g_m}}{1 + s C R_{eq}} = -g_m R_L \frac{1}{s} \frac{\omega_0 - s \frac{1}{g_m R_{eq}}}{s + \omega_0} = -g_m R_L \left( \frac{1}{s} - \frac{1 + \frac{1}{g_m R_{eq}}}{s + \omega_0} \right)$$

$$\begin{aligned} g(t) &= -g_m R_L \left( U(t) - \left( 1 + \frac{1}{g_m R_{eq}} \right) e^{-\omega_0 t} U(t) \right) \\ &= \left( -g_m R_L + \left( g_m R_L + \frac{R_L}{R_{eq}} \right) e^{-\omega_0 t} \right) U(t) \end{aligned}$$

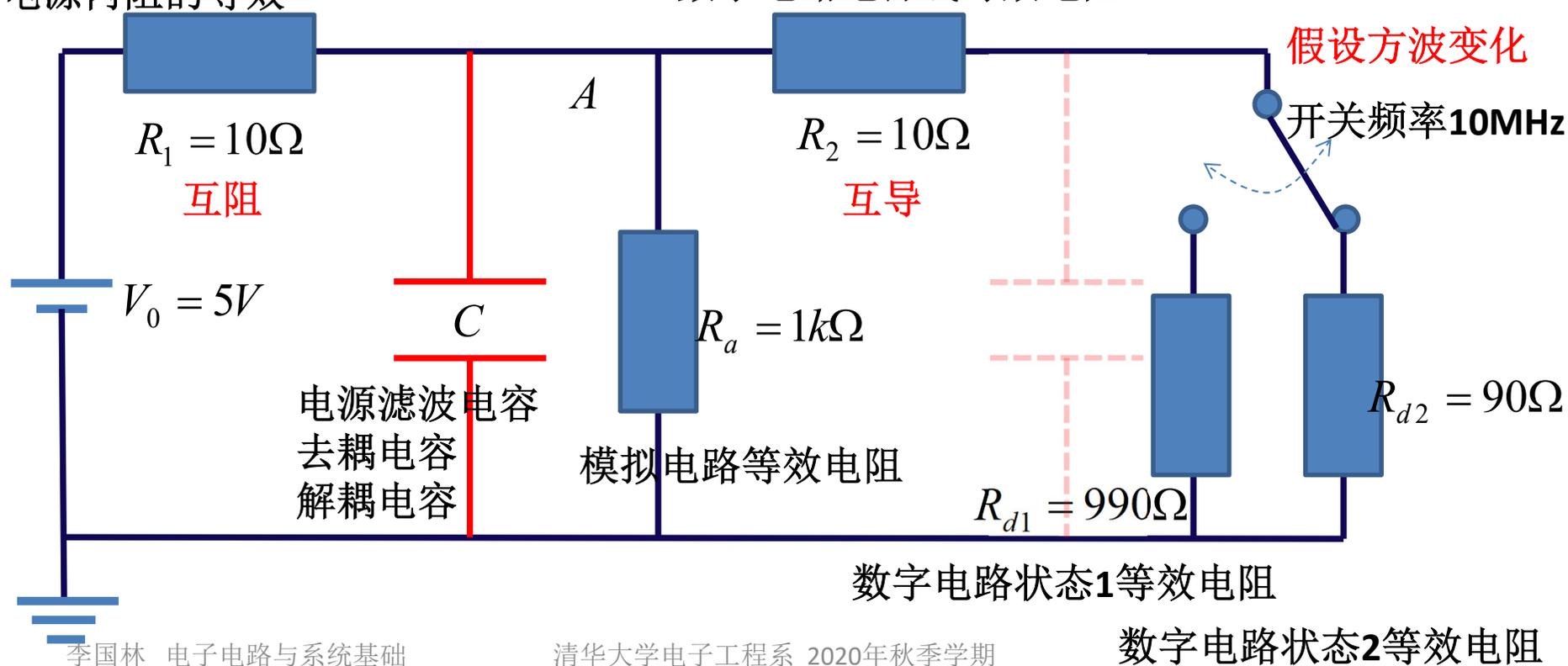
时频对应法就是拉普拉斯变换方法，本课程不要求掌握

# 作业5：用电容做电源滤波

- (1) 假设没有滤波电容，求模拟电路电源端A点的电压波形
- (2) 多大的电容，可以使得A点电压波形起伏是没有电容时的1/10

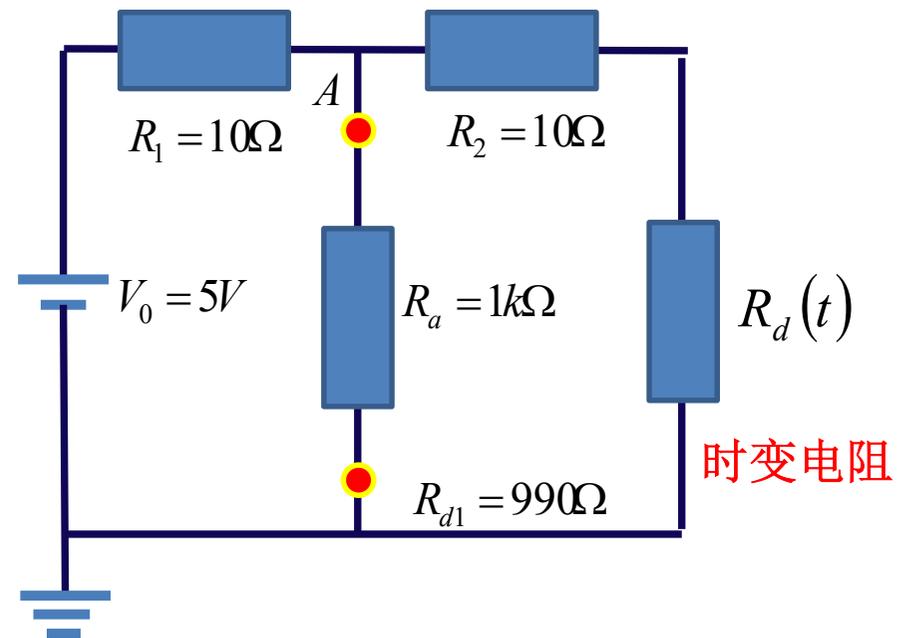
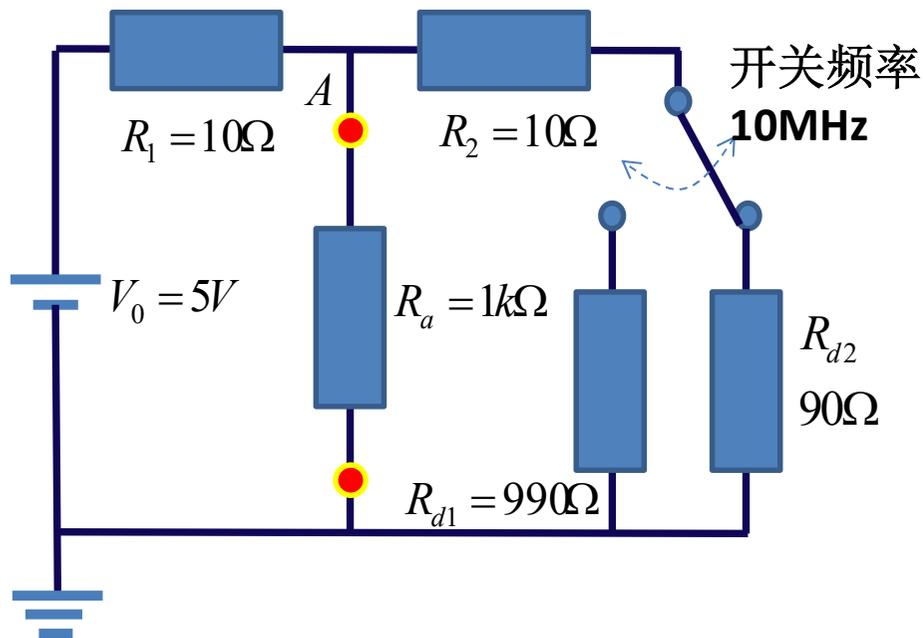
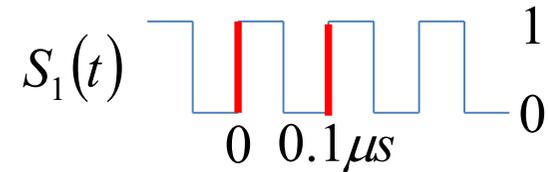
模拟电路电源线等效电阻  
电源内阻的等效

数字电路电源线等效电阻

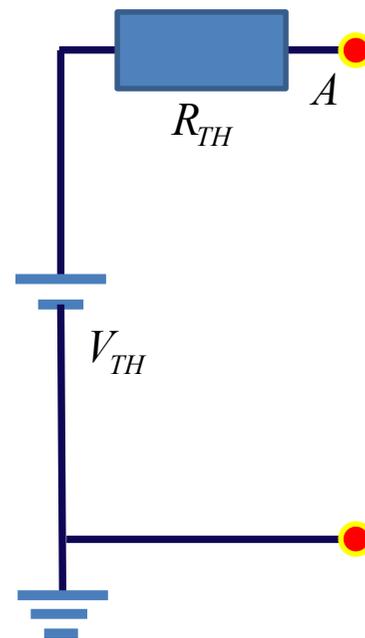
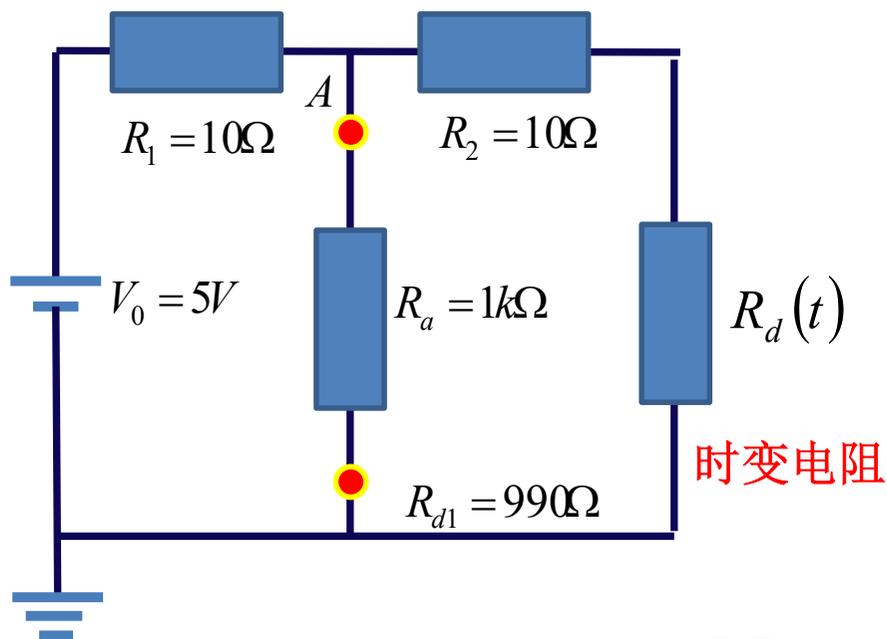


# 时变电阻

$$R_d(t) = R_{d1}S_1(t) + R_{d2}(1 - S_1(t))$$



# 戴维南等效

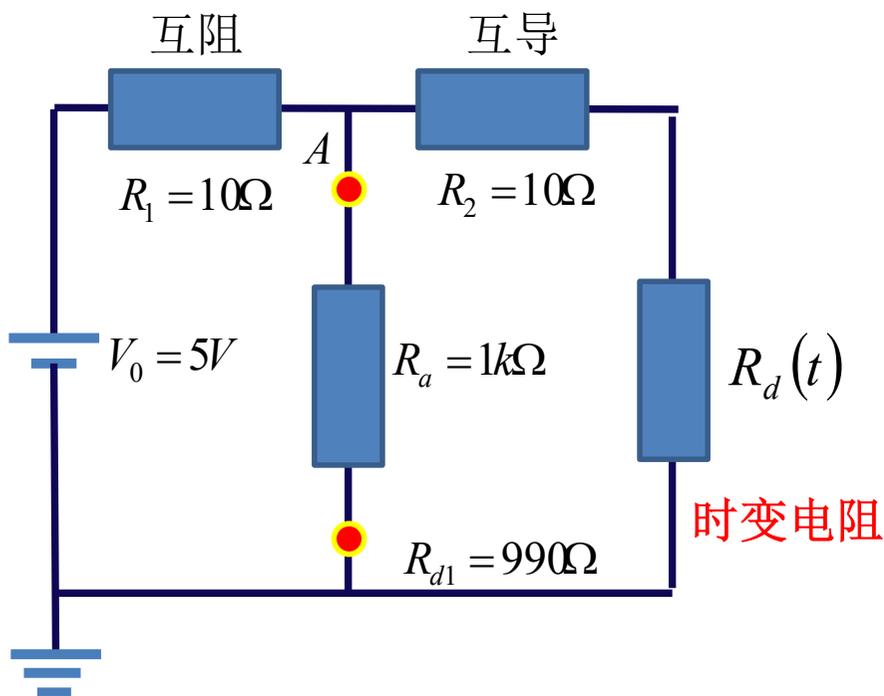


$$R_{TH} = R_1 \parallel R_a \parallel (R_2 + R_d) = \frac{R_a R_1}{R_1 + R_a + \frac{R_a R_1}{R_2 + R_d}}$$

$$V_{TH} = \frac{(R_2 + R_d) \parallel R_a}{R_1 + (R_2 + R_d) \parallel R_a} V_0 = \frac{R_a}{R_1 + R_a + \frac{R_1 R_a}{R_2 + R_d}} V_0$$

可以直接数值计算，但表达式可以更清晰地表明互阻和互导的影响

# 互阻和互导的影响



互阻 $R_1$ 和互导 $G_2$ 导致数字芯片和模拟芯片相互耦合，数字芯片的电流变化导致模拟芯片电源电压波动：不开避免的干扰

- (1) 电源内阻不为0
- (2) 无法为每个芯片单独供电

$$R_{TH} = R_1 \parallel R_a \parallel (R_2 + R_d) = \frac{R_a R_1}{R_1 + R_a + \frac{R_a R_1}{R_2 + R_d}}$$

$$V_{TH} = \frac{(R_2 + R_d) \parallel R_a}{R_1 + (R_2 + R_d) \parallel R_a} V_0 = \frac{R_a}{R_1 + R_a + \frac{R_1 R_a}{R_2 + R_d}} V_0$$

$$R_{TH} \stackrel{R_1=0}{=} 0$$

$$V_{TH} \stackrel{R_1=0}{=} V_0$$

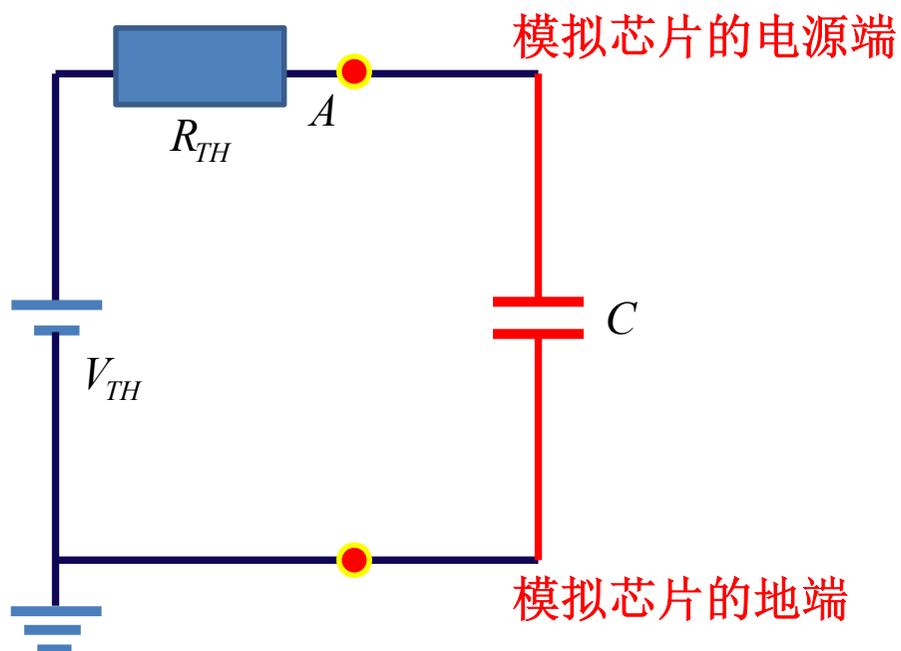
如果没有互阻（互阻 $R_1=0$ ），AG端口等效为恒压源，数字芯片的变化（时变电阻 $R_d$ ）无法影响模拟芯片电压

$$R_{TH} \stackrel{R_2=\infty}{=} \frac{R_a R_1}{R_1 + R_a}$$

$$V_{TH} \stackrel{R_2=\infty}{=} \frac{R_a}{R_1 + R_a} V_0$$

如果没有互导（ $G_2=0$ ，分别单独提供供电电源），AG端口等效源电压和源内阻均不受数字芯片（时变电阻 $R_d$ ）的影响，即数字芯片的电流变化无法影响模拟芯片的电源电压

# 滤波电容 降低波动 解除耦合



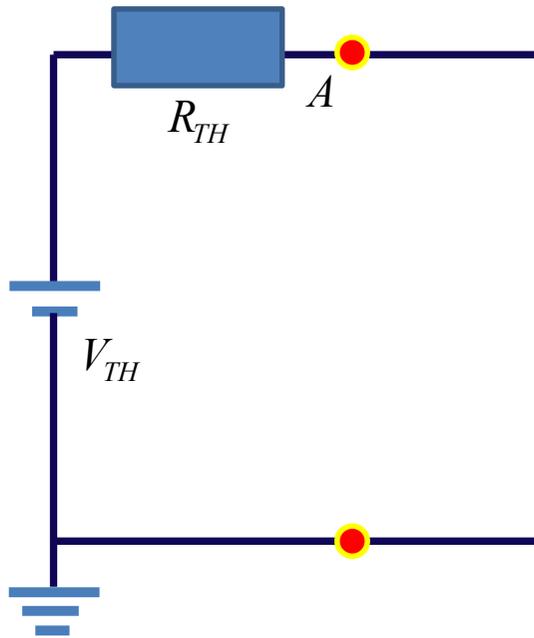
电容C具有电压保持功能，具有求平均功能，只要电容足够大， $V_{TH}$ 和 $R_{TH}$ 的变化就会被电容抹平：电源滤波，芯片解耦

$$R_{TH}(t) = \frac{R_a R_1}{R_1 + R_a + \frac{R_a R_1}{R_2 + R_d(t)}}$$

$$V_{TH}(t) = \frac{R_a}{R_1 + R_a + \frac{R_1 R_a}{R_2 + R_d(t)}} V_0$$

数字芯片的电流变化用时变电阻 $R_d(t)$ 抽象， $R_d(t)$ 对模拟芯片的影响通过 $R_1$ 、 $R_2$ 实现

# 未加电容时，A点波动情况



$$R_{TH1} = 9.804\Omega$$

$$R_{TH2} = 9.010\Omega$$

等效内阻同时变化

$$R_{TH}(t) = \frac{R_a R_1}{R_1 + R_a + \frac{R_a R_1}{R_2 + R_d(t)}}$$

$$R_d(t) = R_{d1} S_1(t) + R_{d2} (1 - S_1(t))$$

$$V_{TH,1}(t) = \frac{R_a}{R_1 + R_a + \frac{R_1 R_a}{R_2 + R_{d1}}} V_0$$

$$= \frac{1000}{10 + 1000 + \frac{10 \cdot 1000}{10 + 990}} \times 5$$

$$= \frac{1000}{10 + 1000 + \underline{\underline{10}}} \times 5$$

$$= 4.902V$$

$$V_{TH}(t) = \frac{R_a}{R_1 + R_a + \frac{R_1 R_a}{R_2 + R_d(t)}} V_0$$

$$V_{TH,2}(t) = \frac{R_a}{R_1 + R_a + \frac{R_1 R_a}{R_2 + R_{d2}}} V_0$$

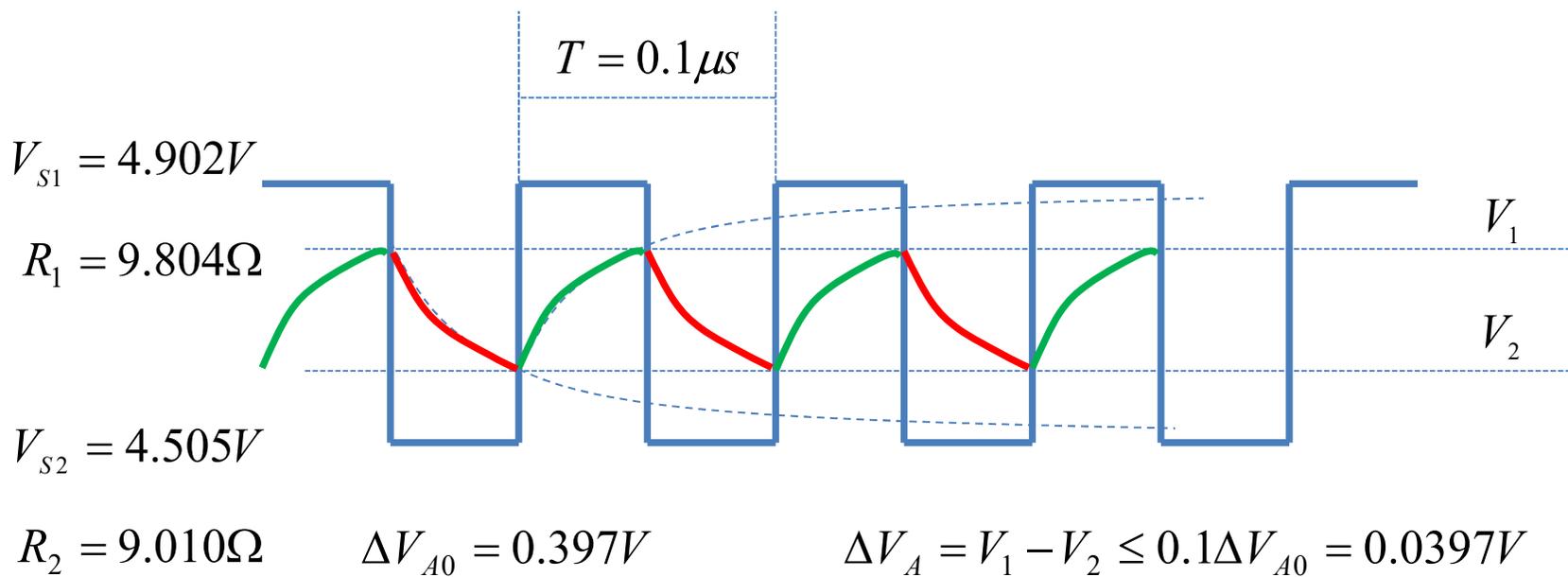
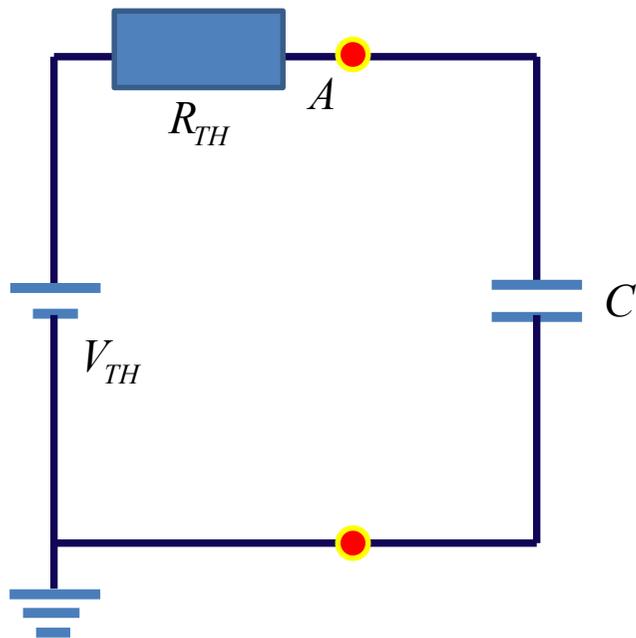
$$= \frac{1000}{10 + 1000 + \frac{10 \cdot 1000}{10 + 90}} \times 5$$

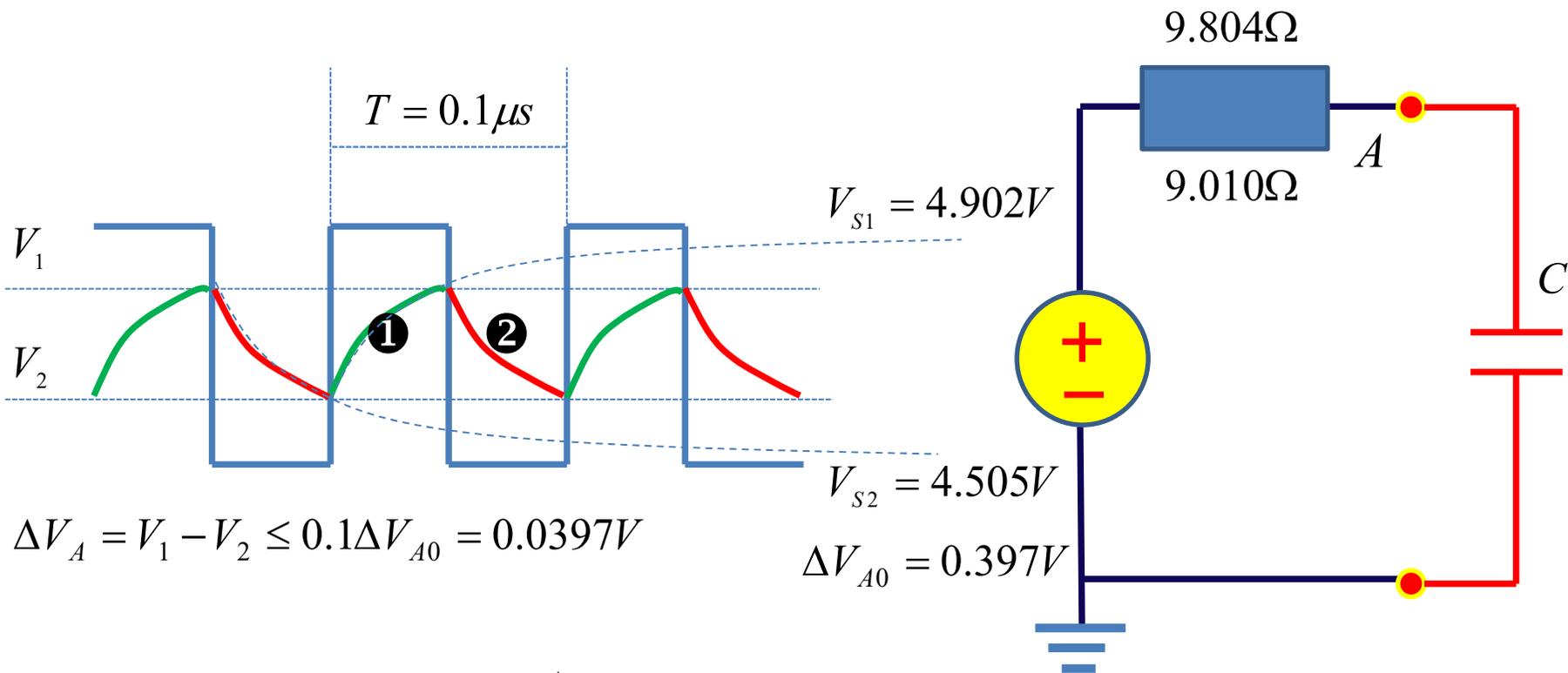
$$= \frac{1000}{10 + 1000 + \underline{\underline{100}}} \times 5$$

$$= 4.505V$$

$$\Delta V_{A0} = 4.902 - 4.505 = 0.397V \quad \text{电压波动} \mathbf{0.4V}$$

# 加电容，A点波动变缓





$$\textcircled{1} \quad v_r(t) = V_{S1} + (V_2 - V_{S1})e^{-\frac{\Delta t_1}{\tau_1}}$$

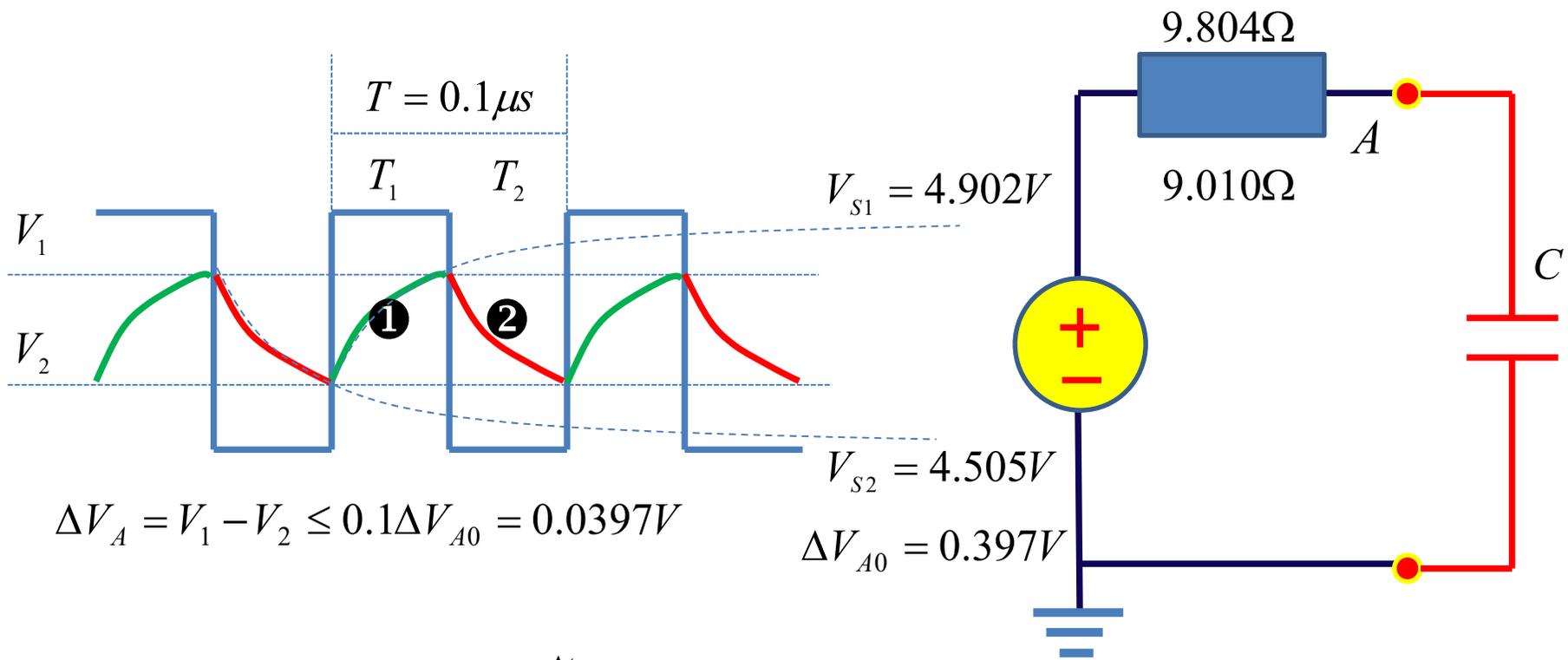
$$\tau_1 = R_1 C$$

$$R_1 = 9.804(\Omega)$$

$$\textcircled{2} \quad v_f(t) = V_{S2} + (V_1 - V_{S2})e^{-\frac{\Delta t_2}{\tau_2}}$$

$$\tau_2 = R_2 C$$

$$R_2 = 9.010(\Omega)$$



①  $v_r(t) = V_{S1} + (V_2 - V_{S1})e^{-\frac{\Delta t_1}{\tau_1}}$

$\tau_1 = R_1 C$

$V_1 = V_{S1} + (V_2 - V_{S1})e^{-\frac{0.5T}{\tau_1}}$

$\tau_2 = R_2 C$

②  $v_f(t) = V_{S2} + (V_1 - V_{S2})e^{-\frac{\Delta t_2}{\tau_2}}$

$\Delta V = V_1 - V_2 \leq 0.1 \Delta V_S$

$V_2 = V_{S2} + (V_1 - V_{S2})e^{-\frac{0.5T}{\tau_2}}$

$T = 0.1 \mu s$

$C = ?$

$$V_1 = V_{S1} + (V_2 - V_{S1})e^{-\frac{0.5T}{\tau_1}} = V_2 a_1 + V_{S1}(1 - a_1) \quad a_1 = e^{-\frac{0.5T}{\tau_1}}$$

$$V_2 = V_{S2} + (V_1 - V_{S2})e^{-\frac{0.5T}{\tau_2}} = V_1 a_2 + V_{S2}(1 - a_2) \quad a_2 = e^{-\frac{0.5T}{\tau_2}}$$

$$V_1 - V_2 a_1 = V_{S1}(1 - a_1) \quad V_1 = \frac{V_{S1}(1 - a_1) + V_{S2}(1 - a_2)a_1}{1 - a_1 a_2}$$

$$V_2 - V_1 a_2 = V_{S2}(1 - a_2) \quad V_2 = \frac{V_{S2}(1 - a_2) + V_{S1}(1 - a_1)a_2}{1 - a_1 a_2}$$

$$\Delta V_A = V_1 - V_2 = (V_{S1} - V_{S2}) \frac{(1 - a_1)(1 - a_2)}{1 - a_1 a_2} \leq 0.1(V_{S1} - V_{S2})$$

$$\frac{(1 - a_1)(1 - a_2)}{1 - a_1 a_2} \leq 0.1$$

$$\frac{(1-a_1)(1-a_2)}{1-a_1a_2} \leq 0.1$$

$$a_1 = e^{-\frac{0.5T}{R_1C}}$$

$$a_2 = e^{-\frac{0.5T}{R_2C}}$$

非线性方程求解，可以用牛顿拉夫逊迭代法，过于复杂

假设C足够大，时间常数足够大，充放电时间足够长，可以做如下估算：

$$a_1 = e^{-\frac{0.5T}{R_1C}} \approx 1 - \frac{0.5T}{R_1C}$$

$$a_2 = e^{-\frac{0.5T}{R_2C}} \approx 1 - \frac{0.5T}{R_2C}$$

$$0.1 \geq \frac{(1-a_1)(1-a_2)}{1-a_1a_2} \approx \frac{\frac{0.5T}{\tau_1} \frac{0.5T}{\tau_2}}{\frac{0.5T}{\tau_1} + \frac{0.5T}{\tau_2} - \frac{0.5T}{\tau_1} \frac{0.5T}{\tau_2}} \approx \frac{\frac{0.5T}{\tau_1} \frac{0.5T}{\tau_2}}{\frac{0.5T}{\tau_1} + \frac{0.5T}{\tau_2}} = \frac{0.5T}{\tau_1 + \tau_2} = \frac{0.5T}{C(R_1 + R_2)}$$

$$C \geq \frac{0.5T}{0.1(R_1 + R_2)} = \frac{5T}{R_1 + R_2} = \frac{5 \times 0.1 \mu s}{9.8 + 9.0} = 0.0266 \mu F$$

$$C \geq \frac{0.5T}{0.1(R_1 + R_2)} = \frac{5T}{R_1 + R_2} = \frac{5 \times 0.1 \mu s}{9.8 + 9.0} = 0.0266 \mu F \quad \text{取} \quad C = 0.03 \mu F$$

验证正确性

$$\tau_1 = R_1 C = 9.8 \times 0.03 \mu F = 0.294 \mu s$$

$$\tau_2 = R_2 C = 9.0 \times 0.03 \mu F = 0.270 \mu s$$

$$a_1 = e^{-\frac{0.5T}{\tau_1}} = e^{-\frac{0.05}{0.294}} = e^{-0.1701} = 0.847$$

$$a_2 = e^{-\frac{0.5T}{\tau_2}} = e^{-\frac{0.05}{0.270}} = e^{-0.1852} = 0.831$$

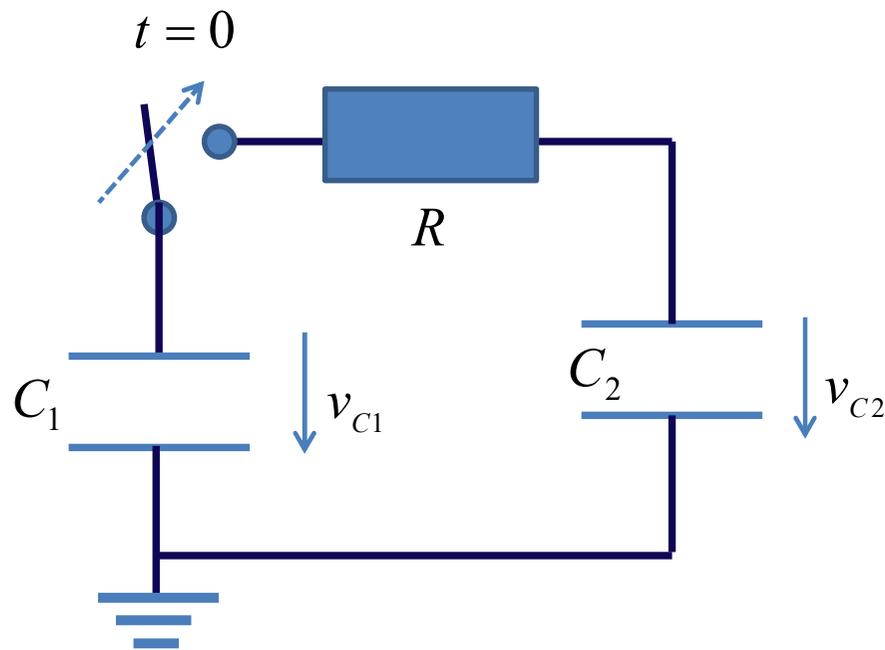
$$V_1 = \frac{V_{S1}(1-a_1) + V_{S2}(1-a_2)a_1}{1-a_1a_2} = \frac{4.902 \times 0.153 + 4.505 \times 0.169 \times 0.847}{0.296} = 4.712V$$

$$V_2 = \frac{V_{S2}(1-a_2) + V_{S1}(1-a_1)a_2}{1-a_1a_2} = \frac{4.505 \times 0.169 + 4.902 \times 0.153 \times 0.831}{0.296} = 4.678V$$

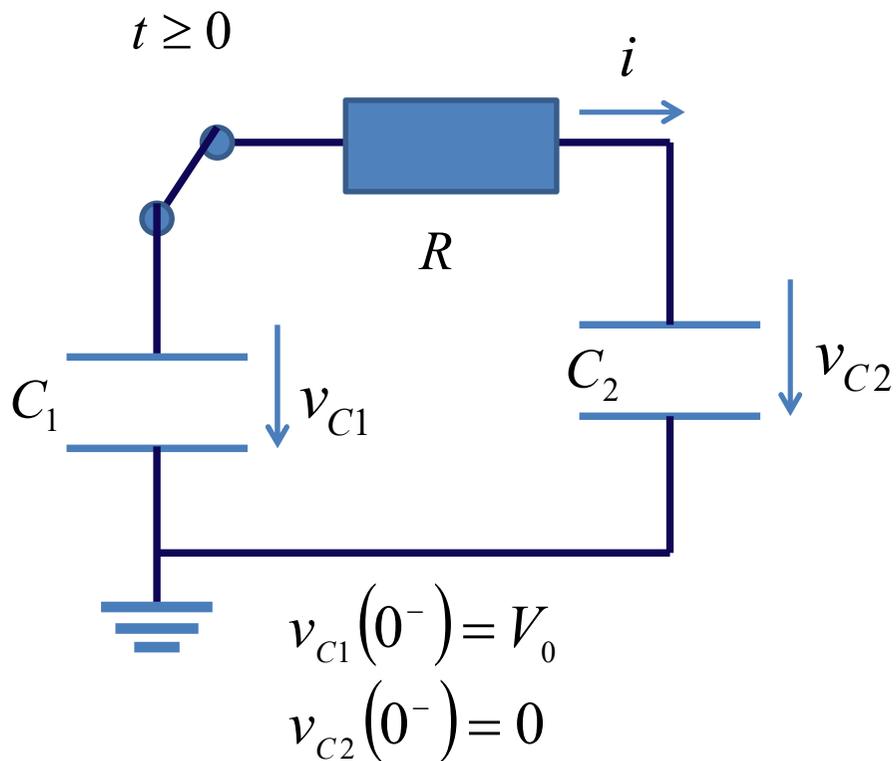
$$\Delta V_A = V_1 - V_2 = 4.712 - 4.678 = 0.034V \quad \Delta V_{A0} = 4.902 - 4.505 = 0.397V$$

**确实满足**  $\Delta V_A \leq 0.1V_{A0}$

# 作业6 电容电荷的重新分配



- $t < 0$ 时刻,  $C_1$ 电容初始电压为  $V_0$ ,  $C_2$ 初始电压为  $0$
- 在  $t = 0$ 时刻, 开关闭合, 求电容  $C_1$ 、 $C_2$ 两端电压变化规律, 写出表达式, 画出时域波形
  - 电荷重新分配过程中, 电阻消耗多少能量? 能量是否守恒?
- 考察  $R$  越来越小趋于  $0$  的变化过程中, 回路电流是如何变化的? 电容电荷的重新分配情况怎样?
  - 当  $R = 0$  (短接线连接) 时, 电容电荷的重新分配是瞬间完成的, 电容电压发生突变! 出现无界电流!



$$v_{C1} = iR + v_{C2}$$

$$-i = C_1 \frac{dv_{C1}}{dt}$$

$$i = C_2 \frac{dv_{C2}}{dt}$$

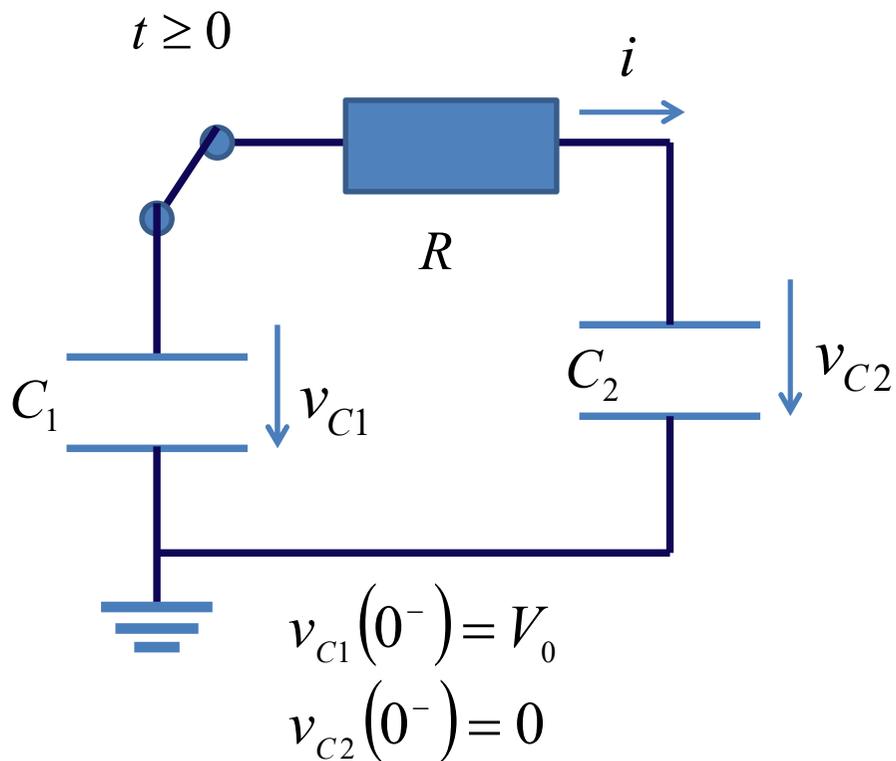
$$\frac{dv_{C1}}{dt} = R \frac{di}{dt} + \frac{dv_{C2}}{dt}$$

$$-\frac{i}{C_1} = R \frac{di}{dt} + \frac{i}{C_2}$$

$$R \frac{di}{dt} + i \left( \frac{1}{C_2} + \frac{1}{C_1} \right) = 0$$

$$R \frac{di}{dt} + \frac{i}{C} = 0$$

$$RC \frac{di}{dt} + i = 0$$



$$RC \frac{di}{dt} + i = 0 \quad \text{零输入}$$

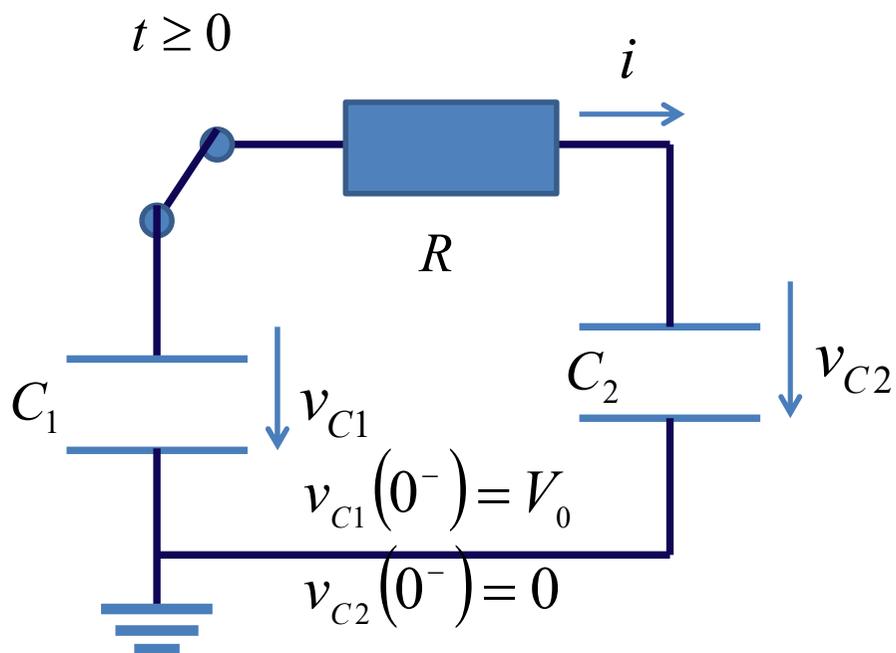
$$\frac{di}{dt} = -\frac{1}{RC} i$$

$$C = \frac{C_1 C_2}{C_1 + C_2}$$

$$i = i(0^+) e^{-\frac{t}{\tau}} \quad \text{零输入响应}$$

$$i(0^+) = \frac{v_{C1}(0^+) - v_{C2}(0^+)}{R} = \frac{v_{C1}(0^-) - v_{C2}(0^-)}{R} = \frac{V_0}{R}$$

$$i(t) = \frac{V_0}{R} e^{-\frac{t}{\tau}} \quad (t \geq 0)$$



$$i(t) = \frac{V_0}{R} e^{-\frac{t}{\tau}} \quad (t \geq 0)$$

$$\tau = RC$$

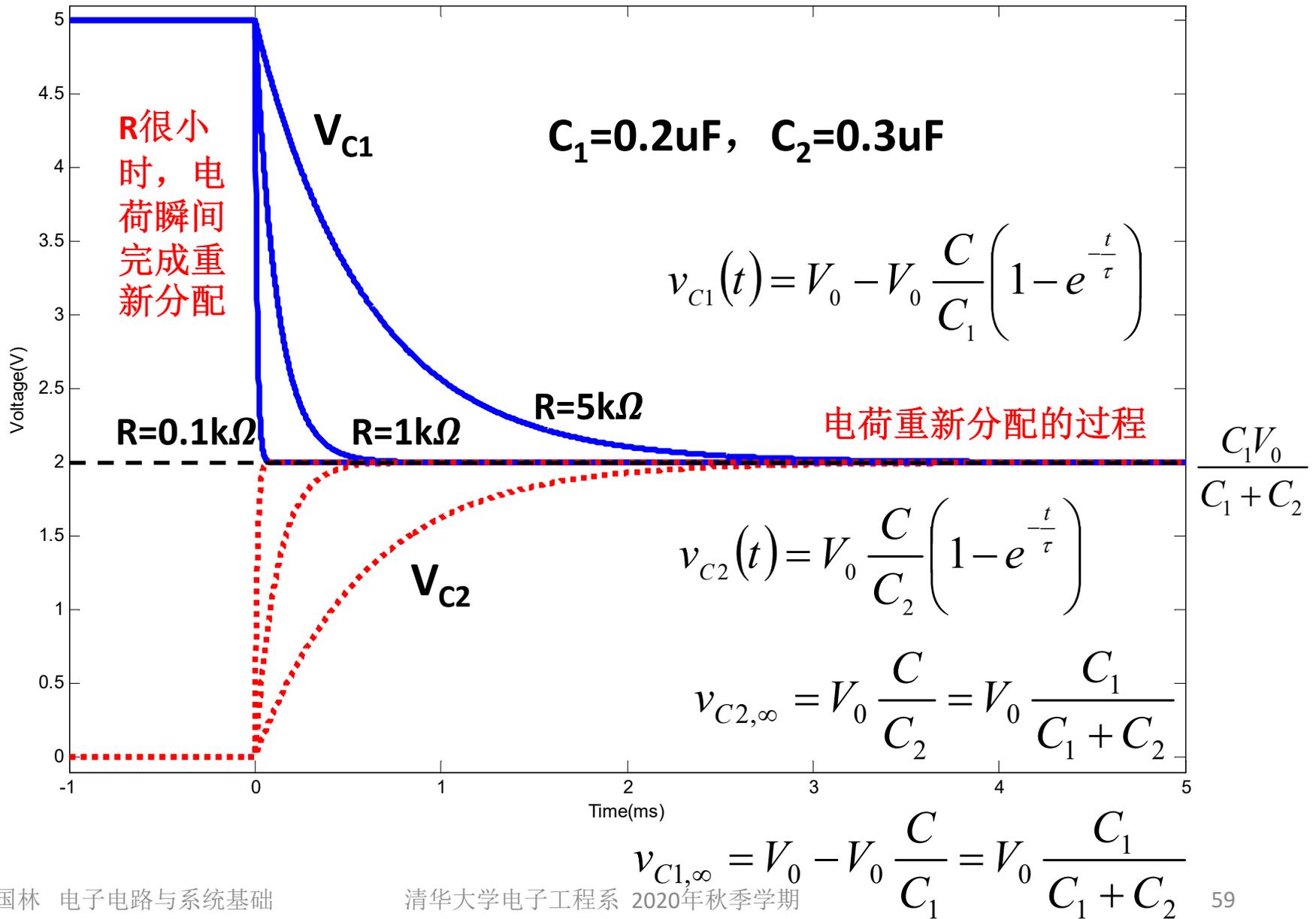
$$C = \frac{C_1 C_2}{C_1 + C_2}$$

$$v_{C1}(t) = v_{C1}(0) + \frac{1}{C_1} \int_0^t (-i(t)) dt = V_0 - \frac{1}{C_1} \frac{V_0}{R} (-\tau) e^{-\frac{t}{\tau}} \Big|_0^t$$

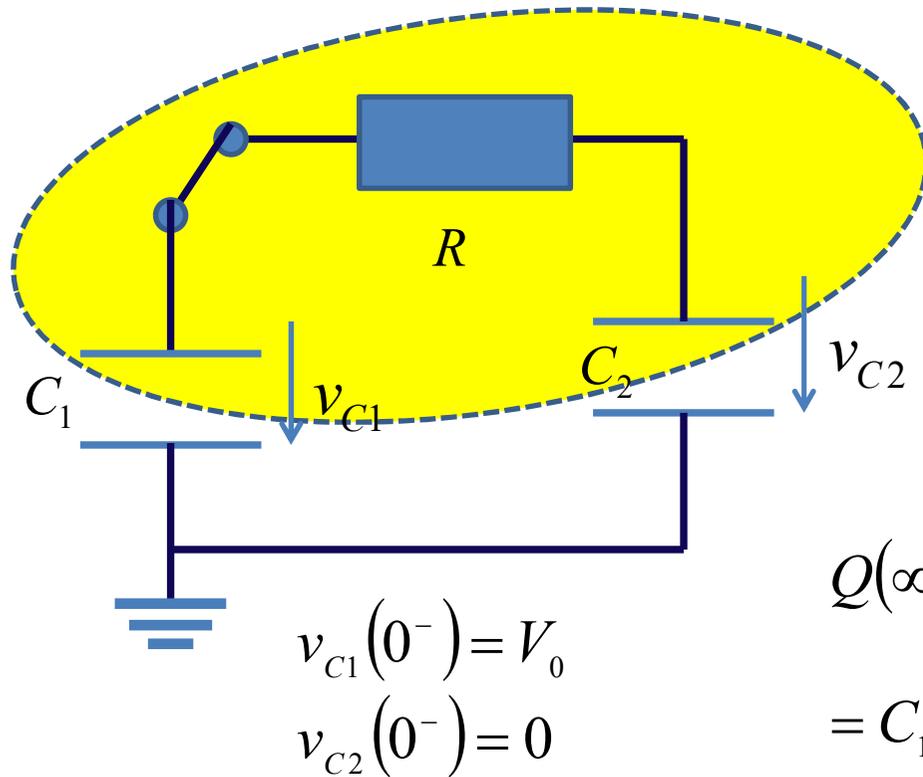
$$= V_0 - \frac{1}{C_1} \frac{V_0}{R} (-RC) \left( e^{-\frac{t}{\tau}} - 1 \right) = V_0 - V_0 \frac{C}{C_1} \left( 1 - e^{-\frac{t}{\tau}} \right)$$

$$v_{C2}(t) = v_{C2}(0) + \frac{1}{C_2} \int_0^t i(t) dt = 0 + \frac{1}{C_2} \frac{V_0}{R} (-\tau) e^{-\frac{t}{\tau}} \Big|_0^t = V_0 \frac{C}{C_2} \left( 1 - e^{-\frac{t}{\tau}} \right)$$

# 电容两端电压波形



# 解的解析：电荷重新分配



$$Q(0^-) = C_1 v_{C_1}(0^-) + C_2 v_{C_2}(0^-) = C_1 V_0$$

$$Q(0^+) = Q(0^-) = C_1 V_0$$

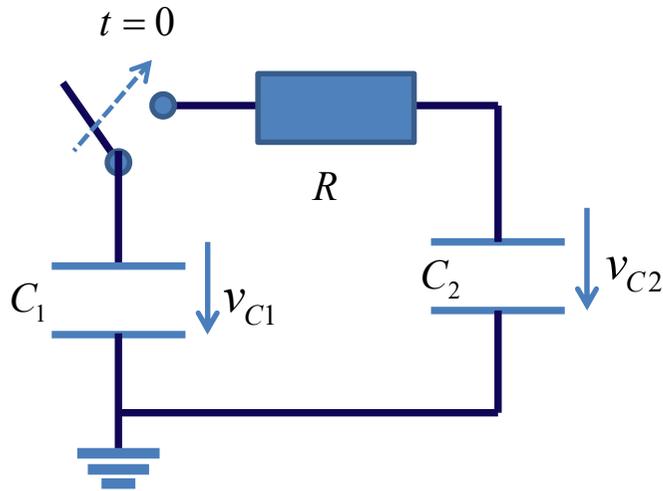
可验证电荷守恒

$$Q(\infty) = C_1 v_{C_1}(\infty) + C_2 v_{C_2}(\infty)$$

$$= C_1 \left( \frac{C_1}{C_1 + C_2} V_0 \right) + C_2 \left( \frac{C_1}{C_1 + C_2} V_0 \right) = C_1 V_0$$

两个电容上极板没有其他释放电荷的通路，于是两个极板上的总电荷始终守恒不变  
电荷重新分配结束后，两个电容电压相等，于是不再有电荷转移

**R → 0**



$$i(t) = \frac{V_0}{R} e^{-\frac{t}{RC}} \cdot U(t)$$

$$= CV_0 \left( \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t) \right)$$

$$\xrightarrow{R \rightarrow 0} CV_0 \cdot \delta(t)$$

**t=0**趋于无穷大，面积为**CV<sub>0</sub>**

$$i(t) = \frac{V_0}{R} e^{-\frac{t}{RC}} \cdot U(t) \quad C = \frac{C_1 C_2}{C_1 + C_2}$$

$$Q(t) = \int_{-\infty}^t i(t) dt = \int_{-\infty}^t \frac{V_0}{R} e^{-\frac{t}{RC}} \cdot U(t) \cdot dt$$

$$= \int_0^t \frac{V_0}{R} e^{-\frac{t}{RC}} \cdot dt = CV_0 \int_0^t \frac{1}{RC} e^{-\frac{t}{RC}} \cdot dt$$

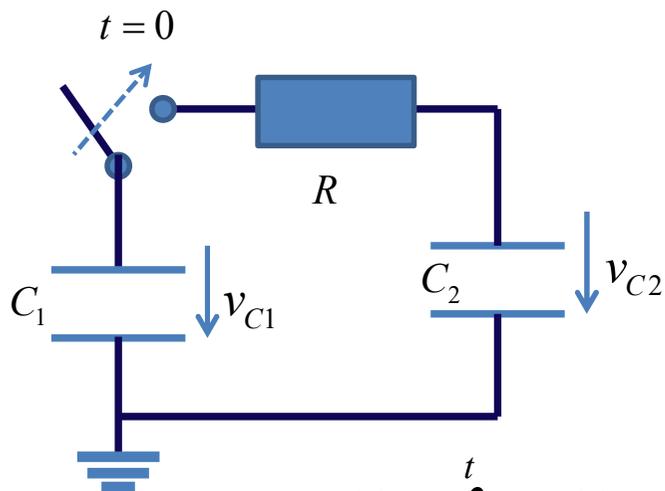
$$= -CV_0 \cdot e^{-\frac{t}{RC}} \Big|_0^t = -CV_0 \cdot \left( e^{-\frac{t}{RC}} - 1 \right)$$

$$= CV_0 \left( 1 - e^{-\frac{t}{RC}} \right)$$

物理上如何理解这个结论？

$$Q(\infty) = CV_0$$

电荷转移是瞬间完成的



$$i(t) = \frac{V_0}{R} e^{-\frac{t}{\tau}} \xrightarrow{R \rightarrow 0} CV_0 \cdot \delta(t)$$

$$p_R(t) = i^2(t)R = \frac{V_0^2}{R} e^{-2\frac{t}{\tau}} = \frac{1}{2} C \frac{V_0^2}{0.5\tau} e^{-\frac{t}{0.5\tau}} \xrightarrow{R \rightarrow 0} \frac{1}{2} CV_0^2 \cdot \delta(t)$$

电阻为0，也有能耗！

$$E_R(t) = \int_0^t p_R(t) dt = \frac{V_0^2}{R} \left( \frac{\tau}{2} \right) \left( 1 - e^{-2\frac{t}{\tau}} \right) = \frac{1}{2} CV_0^2 \left( 1 - e^{-2\frac{t}{\tau}} \right) \xrightarrow{\tau \rightarrow 0} \frac{1}{2} CV_0^2$$

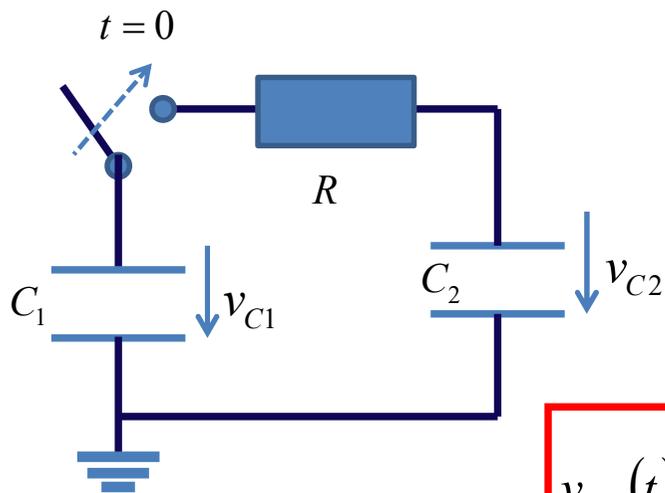
$$E_{C1}(t) = \frac{1}{2} C_1 v_{C1}^2(t) = \frac{1}{2} C_1 V_0^2 \left( \frac{C_1}{C_1 + C_2} + \frac{C_2}{C_1 + C_2} e^{-\frac{t}{\tau}} \right)^2 \xrightarrow{\tau \rightarrow 0} \frac{1}{2} C_1 V_{1\infty}^2$$

$$E_{C2}(t) = \frac{1}{2} C_2 v_{C2}^2(t) = \frac{1}{2} C_2 V_0^2 \left( \frac{C_1}{C_1 + C_2} - \frac{C_1}{C_1 + C_2} e^{-\frac{t}{\tau}} \right)^2 \xrightarrow{\tau \rightarrow 0} \frac{1}{2} C_2 V_{2\infty}^2$$

$$E_R(t) + E_{C1}(t) + E_{C2}(t) = \frac{1}{2} C_1 V_0^2 = E_{C1}(0^-) + E_{C2}(0^-)$$

考虑电阻影响后，能量始终守恒

**R→0: 冲激电流抽象本身就代表了能耗**



### 电容 $C_2$ 充电

可以直接用三要素法获得解的表达式

$$v_{C_2}(0) = 0 \quad \text{①}$$

$$v_{C_2,\infty}(t) = \frac{C_1}{C_1 + C_2} V_0 \quad \text{②}$$

$$\tau = R \frac{C_1 C_2}{C_1 + C_2} \quad \text{③}$$

前提：会应用电荷守恒

$$v_{C_2}(t) = v_{C_2,\infty}(t) + (v_{C_2}(0) - v_{C_2,\infty}(0)) e^{-\frac{t}{\tau}}$$

$$= \frac{C_1}{C_1 + C_2} V_0 \left( 1 - e^{-\frac{t}{\tau}} \right)$$

$$C_1 V_0 + 0 = C_1 V_\infty + C_2 V_\infty$$

$$V_\infty = \frac{C_1}{C_1 + C_2} V_0$$

$$v_{C_1}(0) = V_0 \quad \text{①}$$

$$v_{C_1,\infty}(t) = \frac{C_1}{C_1 + C_2} V_0 \quad \text{②}$$

$$\tau = R \frac{C_1 C_2}{C_1 + C_2} \quad \text{③}$$

### 电容 $C_1$ 放电

$R=0, \tau=0$ : 电荷分配瞬间完成

$$v_{C_1}(t) = v_{C_1,\infty}(t) + (v_{C_1}(0) - v_{C_1,\infty}(0)) e^{-\frac{t}{\tau}}$$

$$= \frac{C_1}{C_1 + C_2} V_0 + \left( V_0 - \frac{C_1}{C_1 + C_2} V_0 \right) e^{-\frac{t}{\tau}}$$

$$= \frac{C_1}{C_1 + C_2} V_0 + \frac{C_2}{C_1 + C_2} V_0 e^{-\frac{t}{\tau}}$$