

电子电路与系统基础II

习题课第四讲 动态元件和动态电路分析

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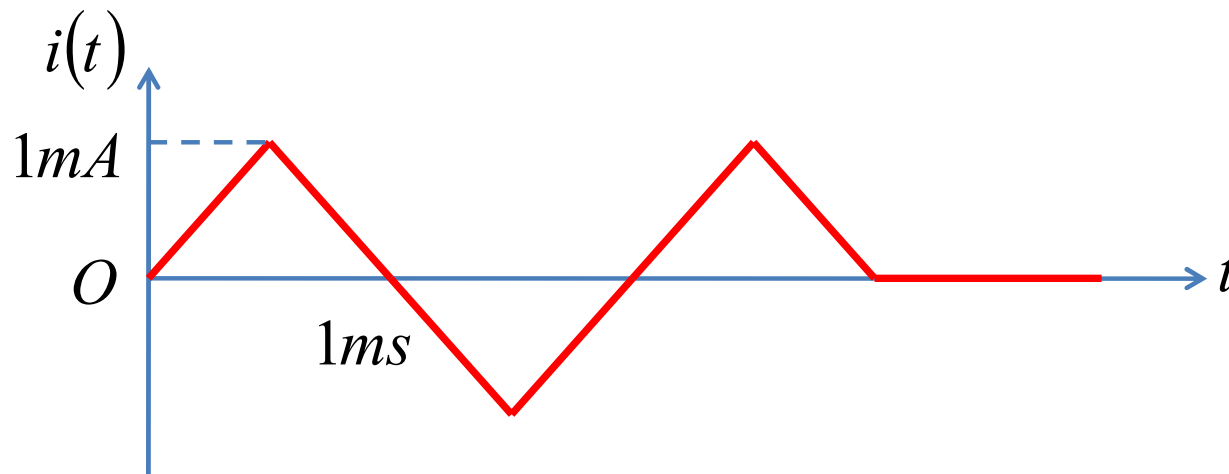
大纲

- 第二讲习题 电容和电感
 - 电容电感特性与状态方程列写及数值法求解
- 第三讲习题 动态电路分析方法（部分）
 - 相图和相量法

第2讲 电容和电感特性

作业1 电容电压、电荷与电能存储

- 某电容器电容容值为 $1\mu\text{F}$ ，电容初始电压为 5V ，加在电容两端电流源的电流变化规律如图所示
 - (1) 求电容上最终存储的电荷量为多大
 - (2) 列写电流、电容电压、电荷量、电容存储电能随时间变化的表达式（教材例题缺）
 - (3) 画出电流、电压、电荷、电能时域波形



电容电量

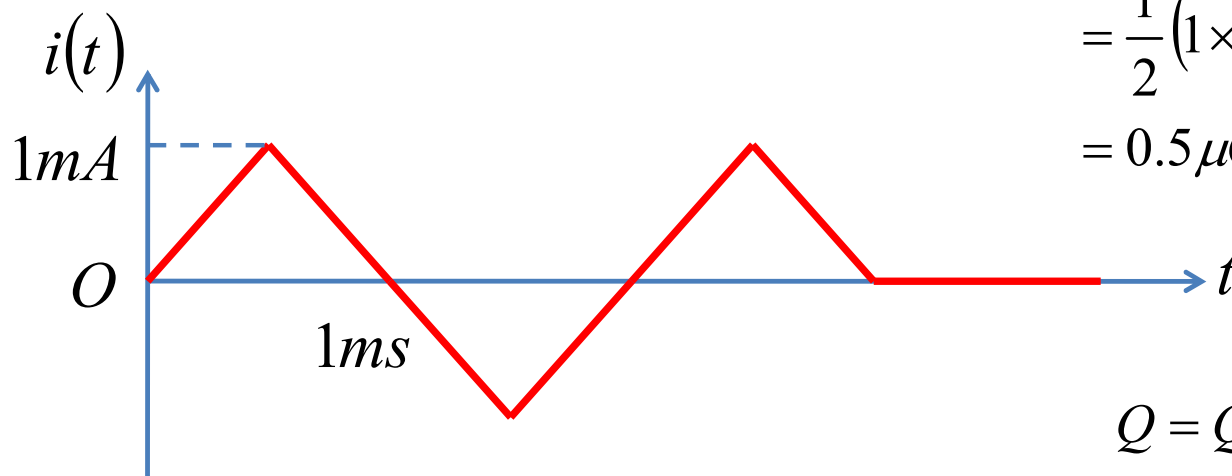
$$\begin{aligned}v(1ms) &= V_0 + \frac{1}{C} \int_0^{1ms} i(\tau) \cdot d\tau \\ &= 5 + \frac{1}{1 \times 10^{-6}} \frac{1}{2} (1 \times 10^{-3} \times 1 \times 10^{-3}) \\ &= 5.5(V)\end{aligned}$$

$$Q = C \cdot V = 1 \times 10^{-6} \times 5.5 = 5.5 \mu C$$

$$Q_0 = C \cdot V_0 = 5 \mu C$$

$$\Delta Q = \int_0^{1ms} i(\tau) \cdot d\tau$$

$$\begin{aligned}&= \frac{1}{2} (1 \times 10^{-3} \times 1 \times 10^{-3}) \\ &= 0.5 \mu C\end{aligned}$$



$$Q = Q_0 + \Delta Q = 5.5 \mu C$$

求数学表达式

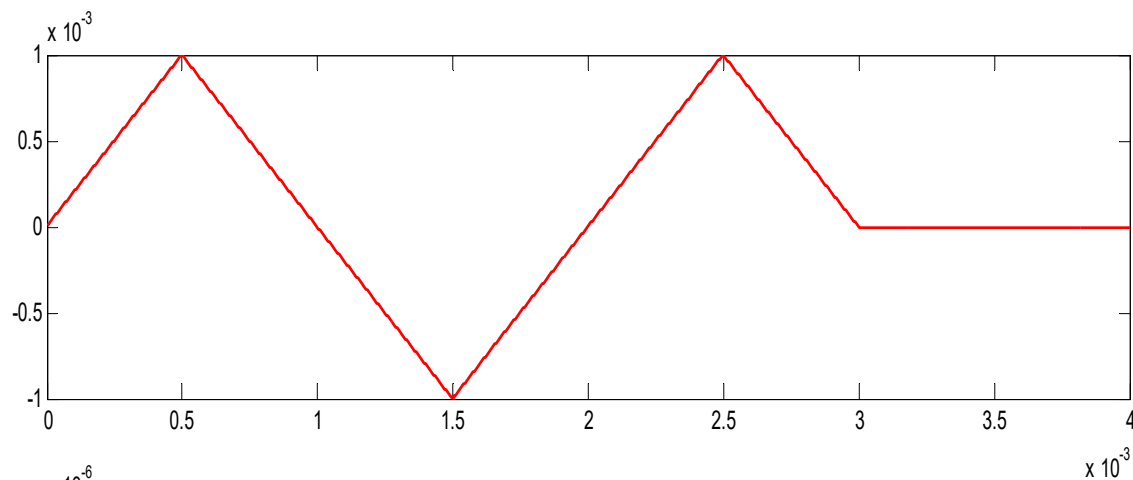
$$Q(t) = \int_{-\infty}^t i(\tau) \cdot d\tau$$

$$= Q_0 + \int_0^t i(\tau) \cdot d\tau$$

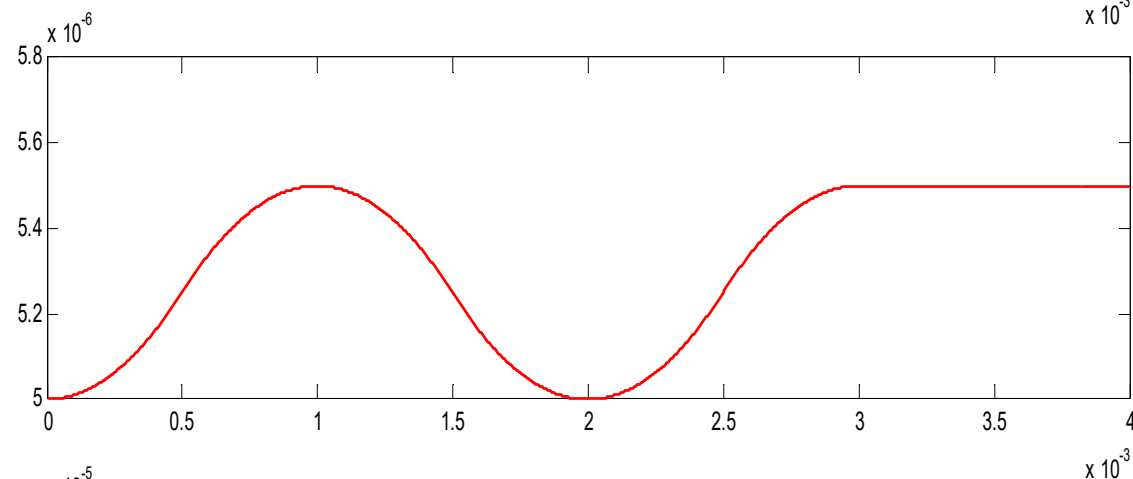
$$v(t) = \frac{Q(t)}{C}$$

$$E_C(t) = \frac{1}{2} C v^2(t)$$

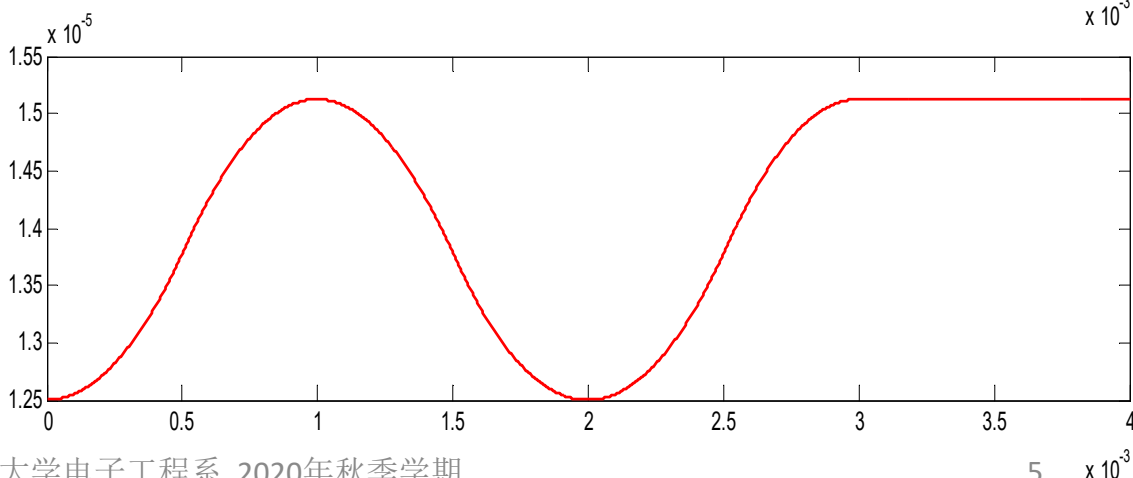
$i(t)$



$Q(t)$



$E_C(t)$



数学表达式

$$i(t) = \begin{cases} 2t \text{ mA} & 0 \leq t < 0.5 \text{ ms} \\ -2(t-1) \text{ mA} & 0.5 \leq t < 1.5 \text{ ms} \\ 2(t-2) \text{ mA} & 1.5 \leq t < 2.5 \text{ ms} \\ -2(t-3) \text{ mA} & 2.5 \leq t < 3 \text{ ms} \\ 0 & t \geq 3 \text{ ms} \end{cases}$$

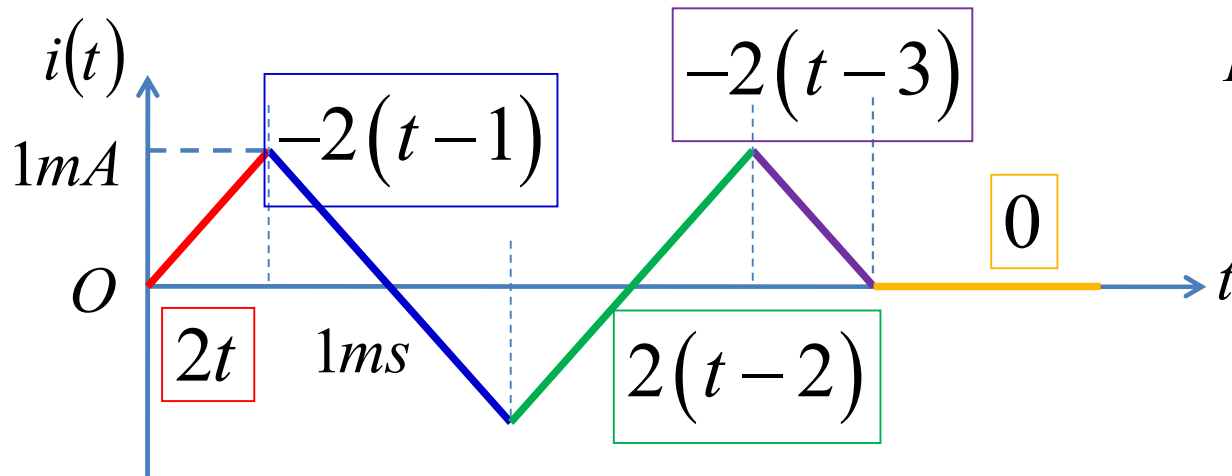
特别注意：时间单位ms，电流单位mA

$$Q(t) = Q_0 + \int_0^t i(\tau) \cdot d\tau$$

$$v(t) = \frac{Q(t)}{C}$$

$$= V_0 + \frac{1}{C} \int_0^t i(\tau) \cdot d\tau$$

$$E_C(t) = \frac{1}{2} C v^2(t)$$

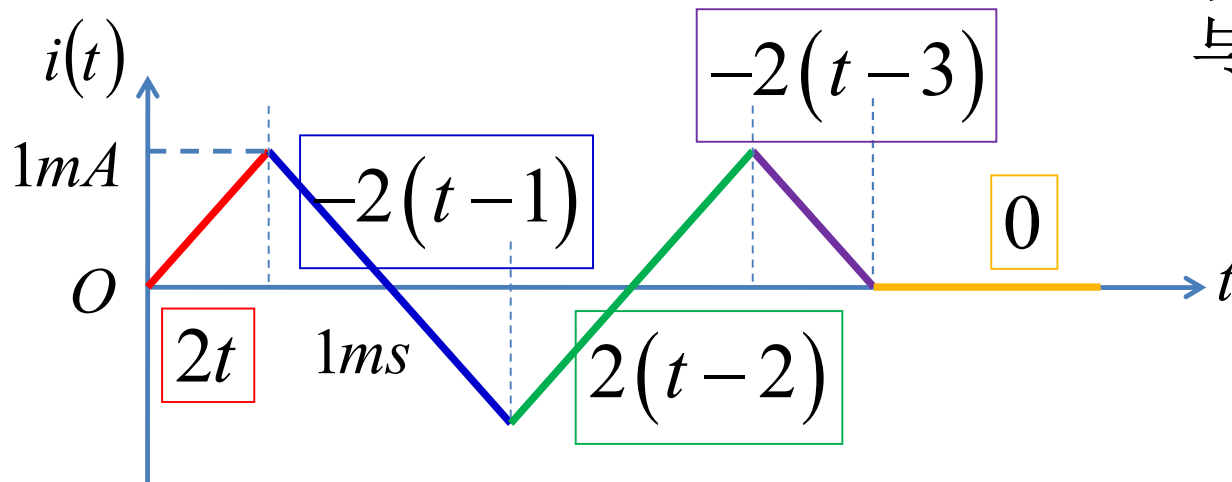


$$Q(t) = Q(0) + \int_0^t i(t) dt = CV(t)$$

$$= \begin{cases} 5 + t^2 \mu\text{C} & 0 \leq t < 0.5 \text{ ms} \\ 5.5 - (t-1)^2 \mu\text{C} & 0.5 \leq t < 1.5 \text{ ms} \\ 5 + (t-2)^2 \mu\text{C} & 1.5 \leq t < 2.5 \text{ ms} \\ 5.5 - (t-3)^2 \mu\text{C} & 2.5 \leq t < 3 \text{ ms} \\ 5.5 \mu\text{C} & t \geq 3 \text{ ms} \end{cases}$$

$$i(t) = \begin{cases} 2t \text{ mA} & 0 \leq t < 0.5 \text{ ms} \\ -2(t-1) \text{ mA} & 0.5 \leq t < 1.5 \text{ ms} \\ 2(t-2) \text{ mA} & 1.5 \leq t < 2.5 \text{ ms} \\ -2(t-3) \text{ mA} & 2.5 \leq t < 3 \text{ ms} \\ 0 & t \geq 3 \text{ ms} \end{cases}$$

- 分段线性电流的积分为分段二次函数
- 线性时不变电容，电压与电荷相同变化规律



$$V(t) = \frac{Q(t)}{C}$$

$$= \dots(V)$$

$$Q(t) = Q(0) + \int_0^t i(t) dt = CV(t)$$

$$= \begin{cases} 5+t^2 \mu\text{C} & 0 \leq t < 0.5 \text{ ms} \\ 5.5-(t-1)^2 \mu\text{C} & 0.5 \leq t < 1.5 \text{ ms} \\ 5+(t-2)^2 \mu\text{C} & 1.5 \leq t < 2.5 \text{ ms} \\ 5.5-(t-3)^2 \mu\text{C} & 2.5 \leq t < 3 \text{ ms} \\ 5.5 \mu\text{C} & t \geq 3 \text{ ms} \end{cases}$$

$$V(t) = V(0) + \frac{1}{C} \int_0^t i(t) dt$$

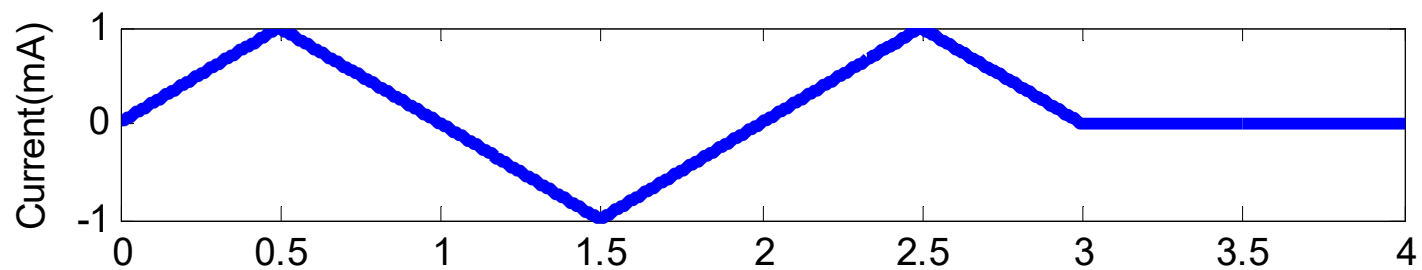
$$= \begin{cases} 5+t^2 \text{ V} & 0 \leq t < 0.5 \text{ ms} \\ 5.5-(t-1)^2 \text{ V} & 0.5 \leq t < 1.5 \text{ ms} \\ 5+(t-2)^2 \text{ V} & 1.5 \leq t < 2.5 \text{ ms} \\ 5.5-(t-3)^2 \text{ V} & 2.5 \leq t < 3 \text{ ms} \\ 5.5 \text{ V} & t \geq 3 \text{ ms} \end{cases}$$

$$E_C(t) = \frac{1}{2} C v^2(t)$$

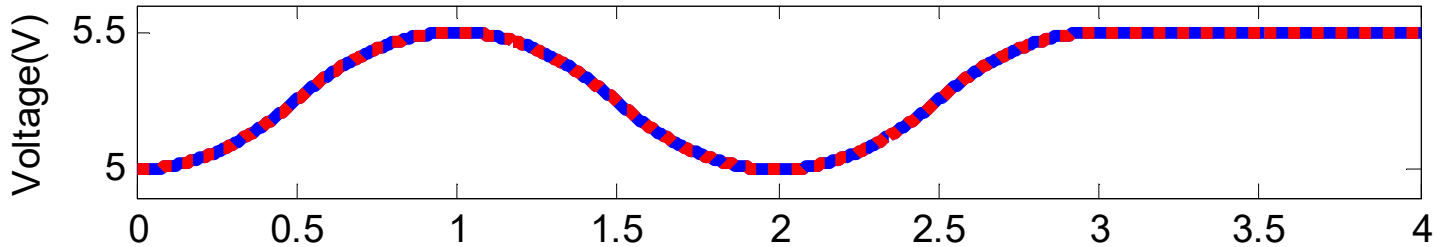
$$= \begin{cases} 0.5(5+t^2)^2 \mu\text{J} & 0 \leq t \leq 0.5 \text{ ms} \\ 0.5(5.5-(t-1)^2)^2 \mu\text{J} & 0.5 \text{ ms} \leq t \leq 1.5 \text{ ms} \\ 0.5(5+(t-2)^2)^2 \mu\text{J} & 1.5 \text{ ms} \leq t \leq 2.5 \text{ ms} \\ 0.5(5.5-(t-3)^2)^2 \mu\text{J} & 2.5 \text{ ms} \leq t \leq 3 \text{ ms} \\ 5.5 \mu\text{J} & t \geq 3 \text{ ms} \end{cases}$$

- 电容电能存储正比于电容电压的平方

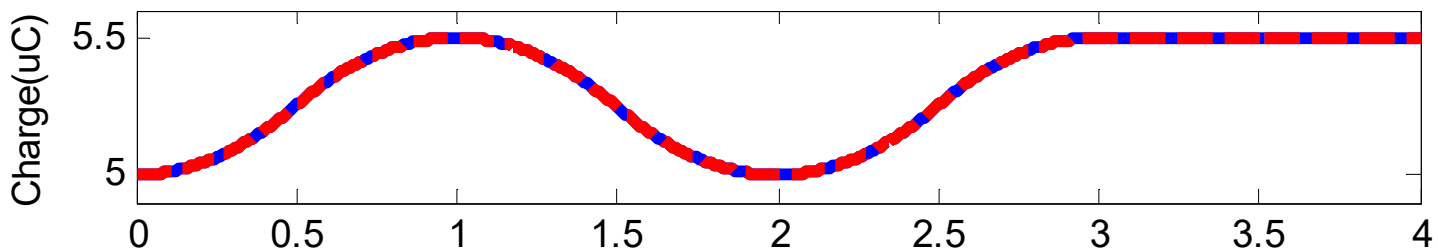
电流



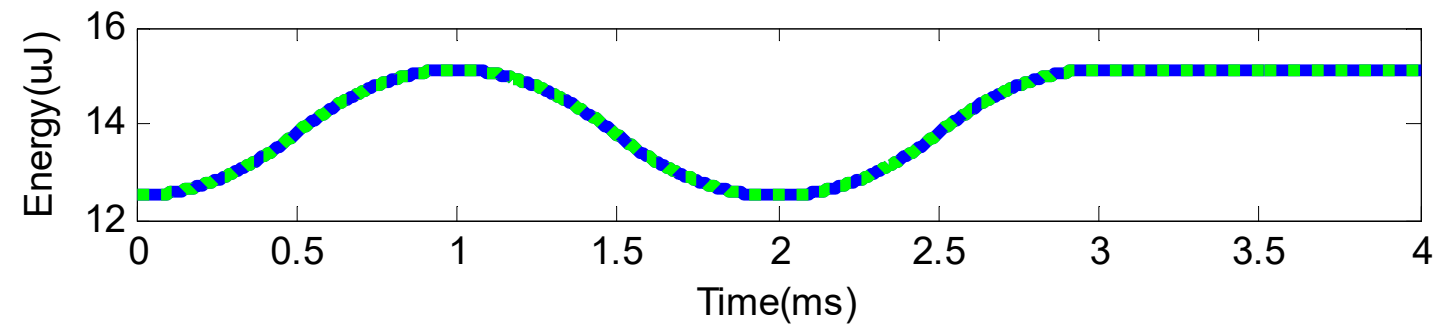
电压



电荷

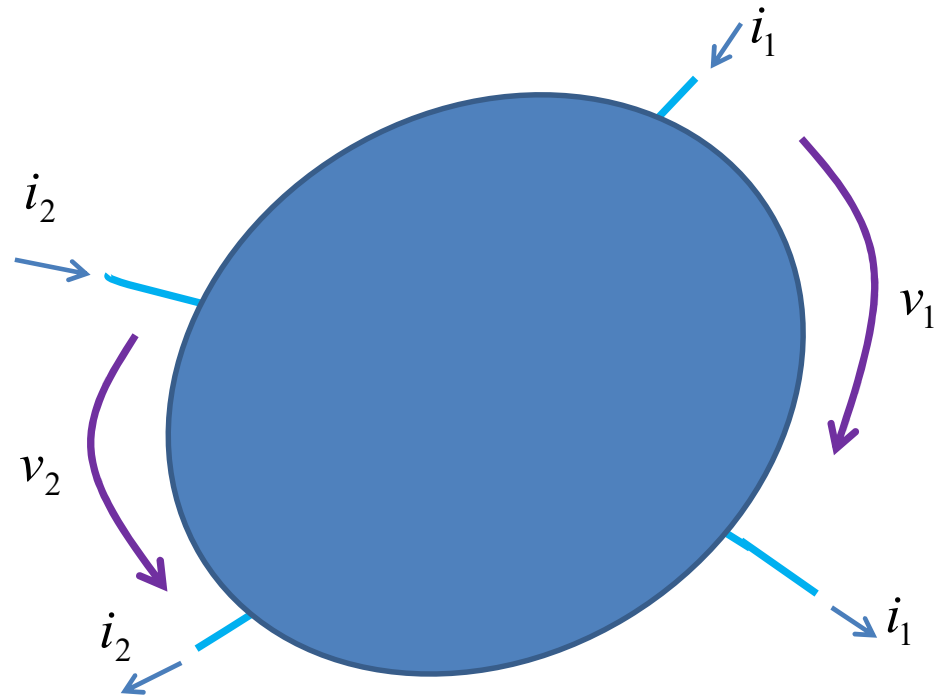


能量



作业2：同名端判定

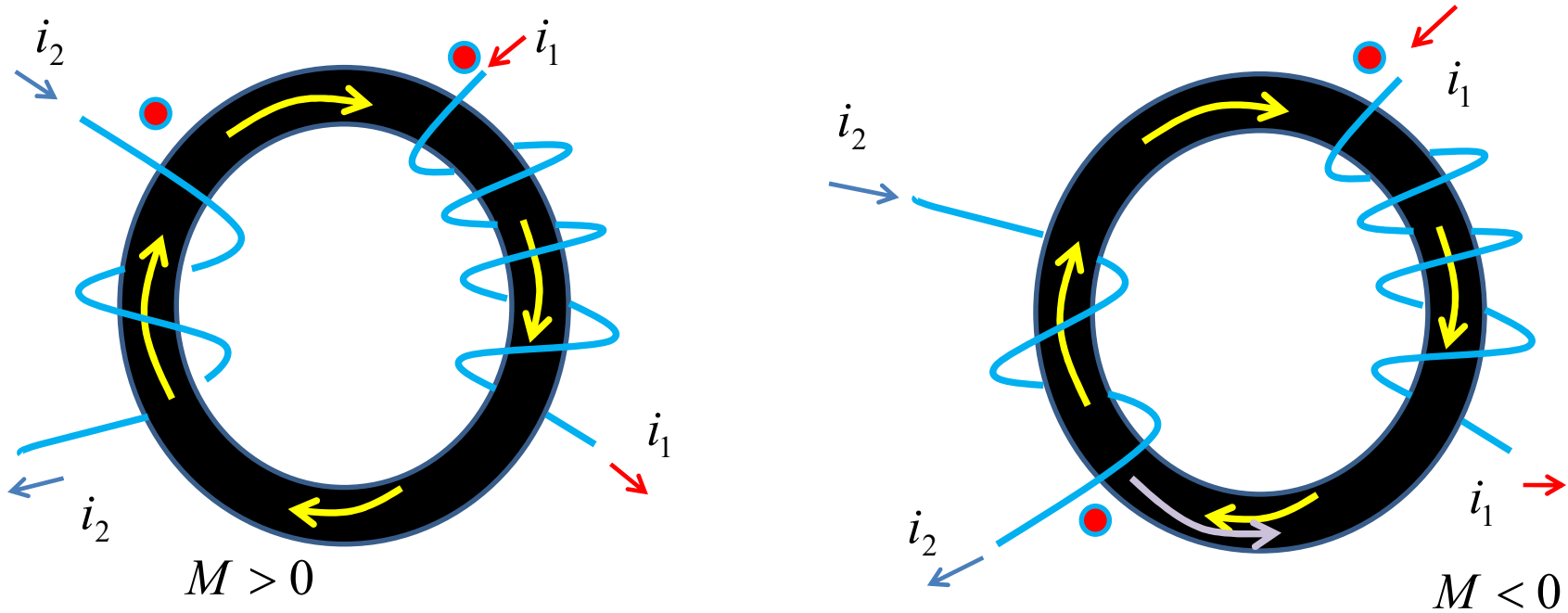
- 如果知道线圈绕向，可以判定同名端
- 如果被封装为黑匣子，内部绕向未知，请设计一个测试方案，判定同名端



知道绕向：流入电流使得磁通加强的两个端点是同名端

不知绕向：???

考察感生电动势



同名端方向和端口电压、电流关联参考方向一致，互感大于0，否则小于0

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

令端口2开路

$$i_2 = 0$$

$$\frac{v_2}{v_1} = \frac{M}{L_1}$$

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} L_1 \\ M \end{bmatrix} \frac{d}{dt} i_1$$

不知绕向：只需判定两个端口电压变化是否具有同相性即可：同相则同名

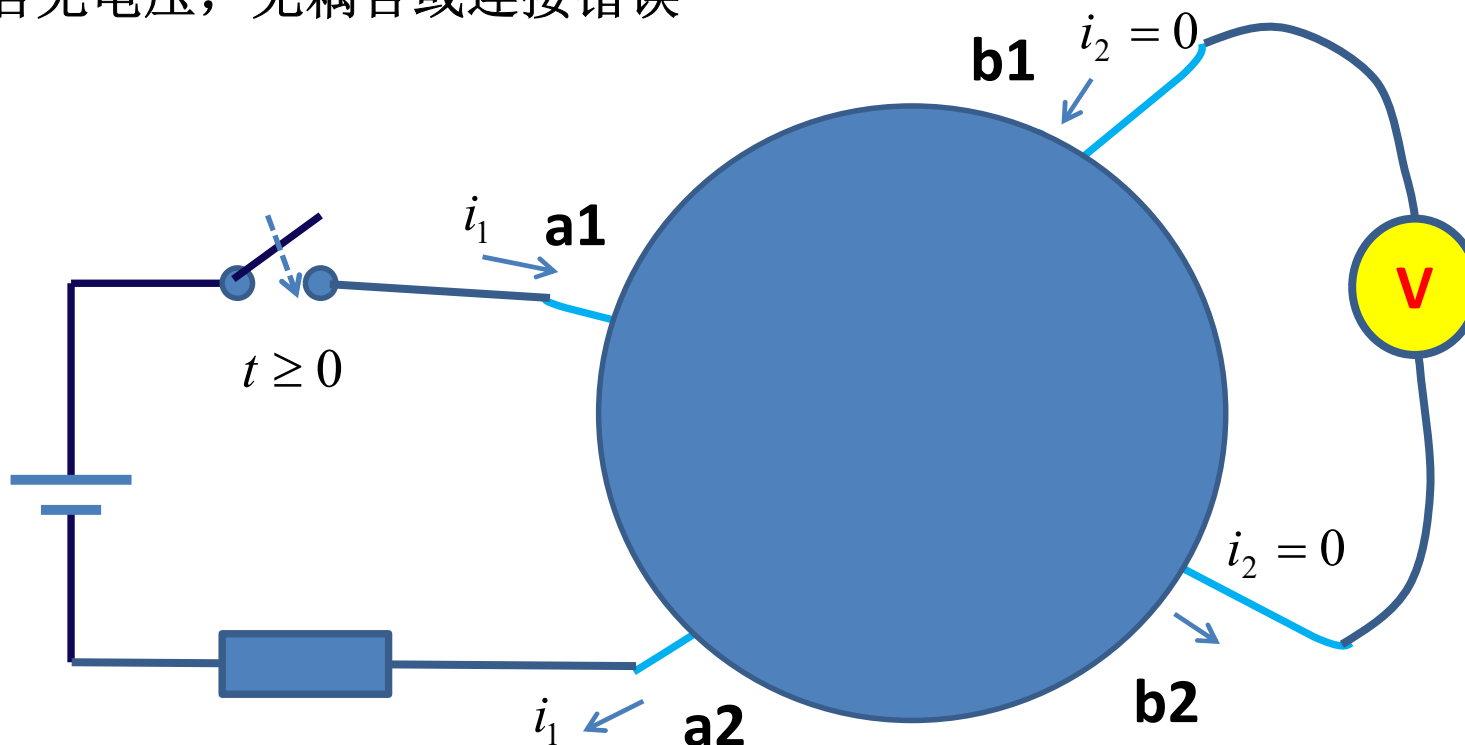
根据前述规律设计测试电路如下：

输入回路接电压源并串联开关和限流电阻，电源极性为正极接**a1**，输出回路接电压表，假定上接正极

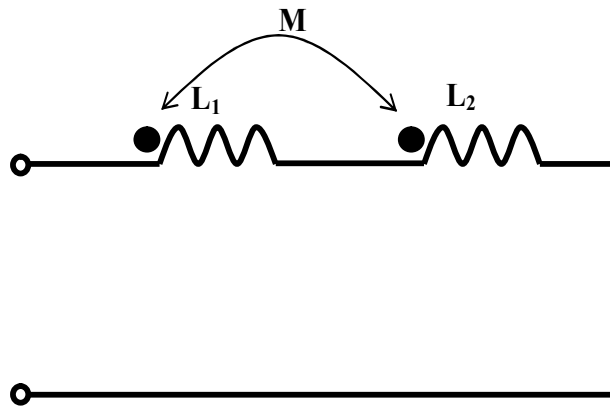
测试时，开关闭合，观察电压表视数

- 1) 若为正电压，则**a1**和**b1**为同名端
- 2) 若为负电压，则**a1**和**b2**为同名端
- 3) 若无电压，无耦合或连接错误

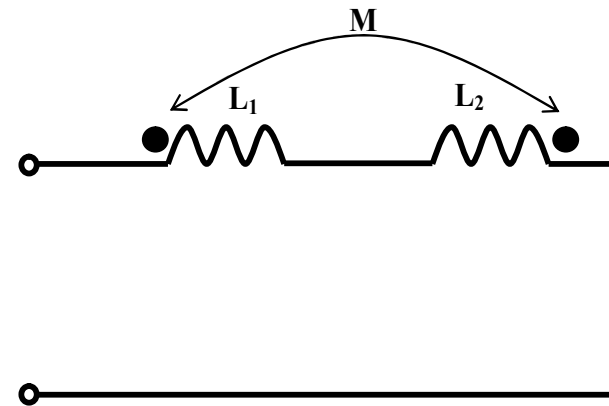
$$\frac{v_2}{v_1} = \frac{M}{L_1} > ? < 0$$



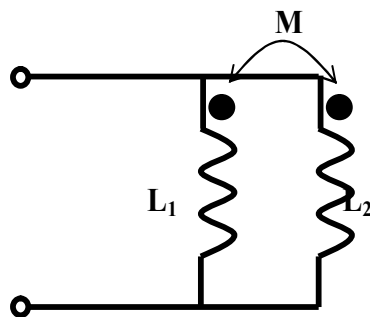
作业3：等效电感计算



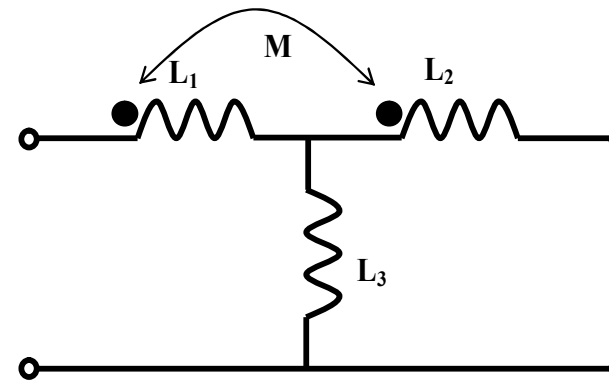
(a) 电感串联：带互感



(b) 电感串联：带互感，绕线反向



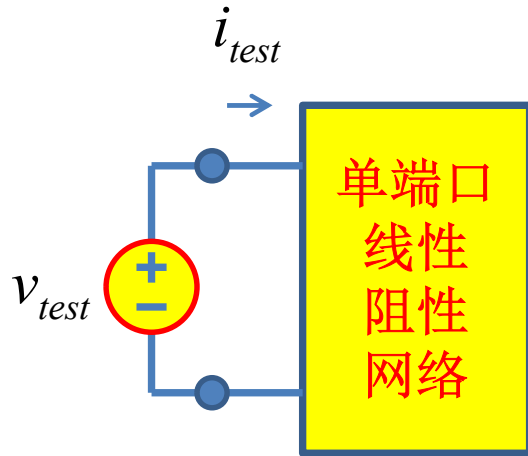
(c) 电感并联：带互感



(d) 二端口电感等效

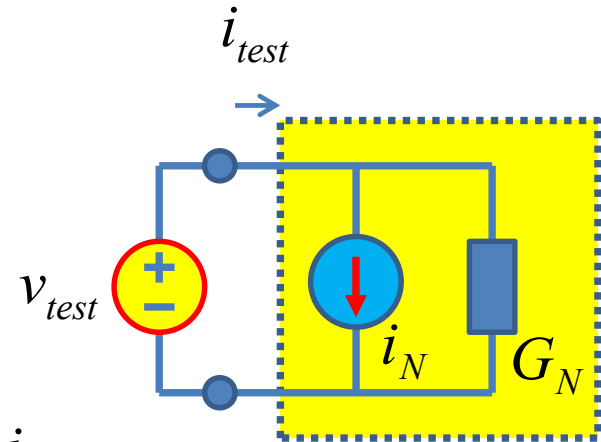
回顾：单端口线性电阻网络等效电路模型

加压求流、加流求压



加压求流

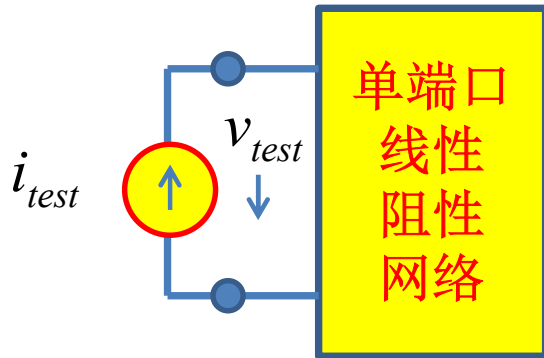
$$i_{test} = \alpha \cdot v_{test} + \beta$$



$$i_{test} = G_N \cdot v_{test} + i_N$$

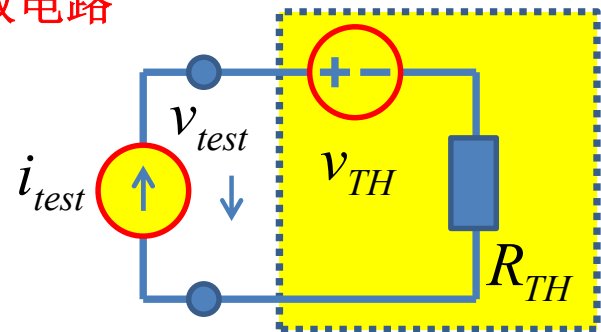
$$i_N = \beta \quad G_N = \alpha$$

加压测试获得压控形式的等效电路
加流测试获得流控形式的等效电路



加流求压

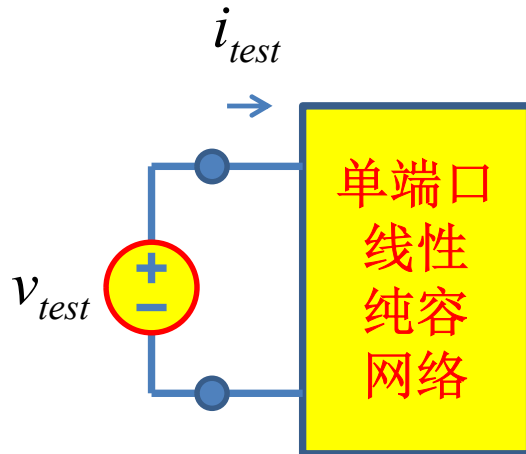
$$v_{test} = \alpha \cdot i_{test} + \beta$$



$$v_{test} = R_{TH} \cdot i_{test} + v_{TH}$$

$$v_{TH} = \beta \quad R_{TH} = \alpha$$

单端口纯容或纯感网络



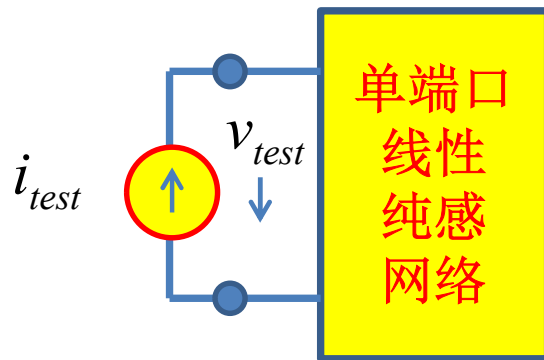
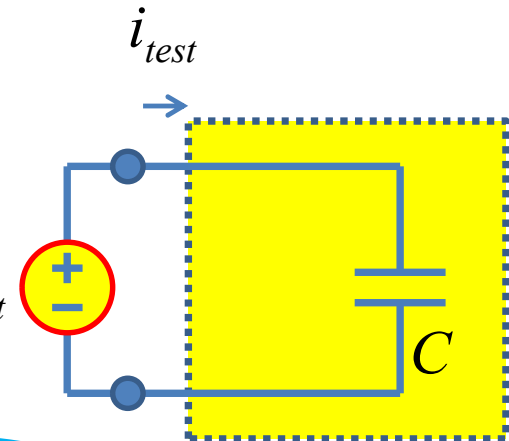
加压求流

$$i_{test} = \alpha \cdot \frac{dv_{test}}{dt}$$

$$i_{test} = C \cdot \frac{dv_{test}}{dt}$$

$$\dot{I}_{test} = \alpha \cdot j\omega \dot{V}_{test} \quad \dot{I}_{test} = j\omega C \dot{V}_{test}$$

$$C = \alpha$$



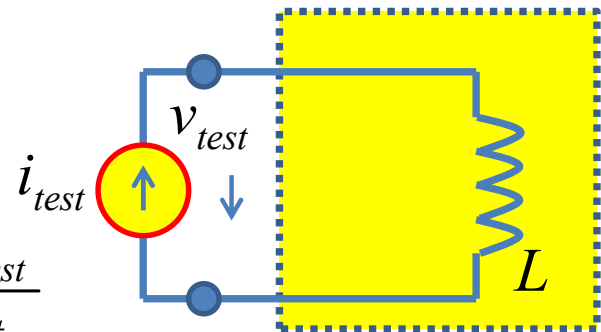
加流求压

$$v_{test} = \alpha \cdot \frac{di_{test}}{dt}$$

$$v_{test} = L \cdot \frac{di_{test}}{dt}$$

$$\dot{V}_{test} = \alpha \cdot j\omega \dot{I}_{test} \quad \dot{V}_{test} = j\omega L \dot{I}_{test}$$

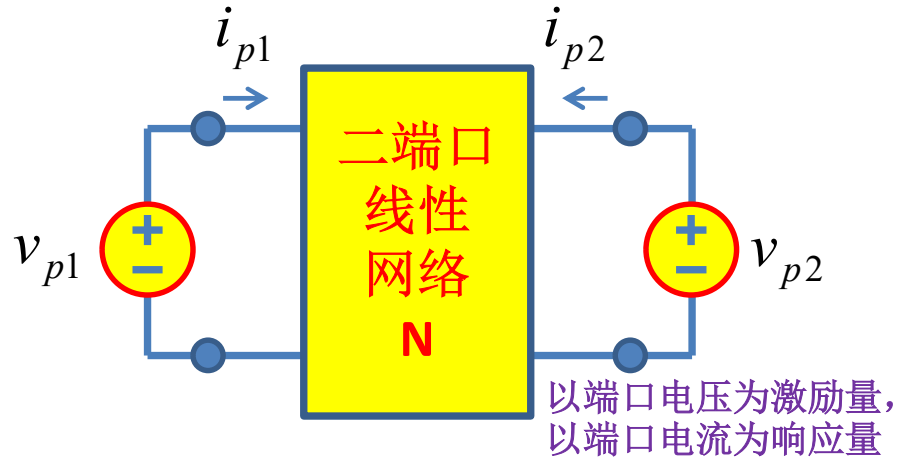
$$L = \alpha$$



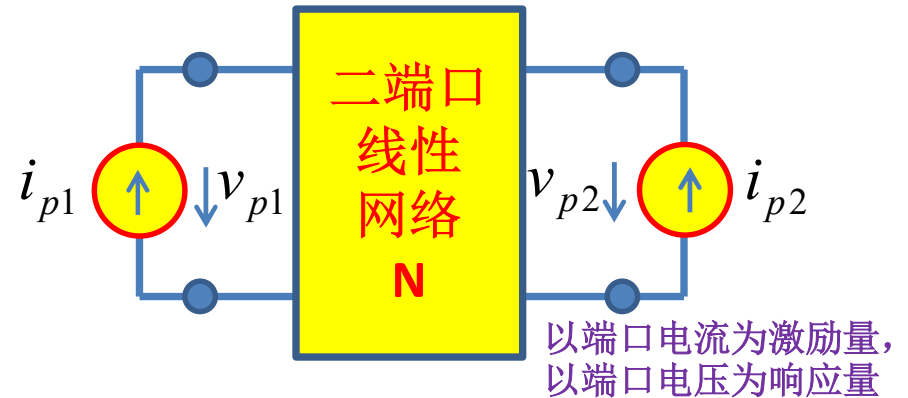
原理上可以这样分析

端口加压、加流方法

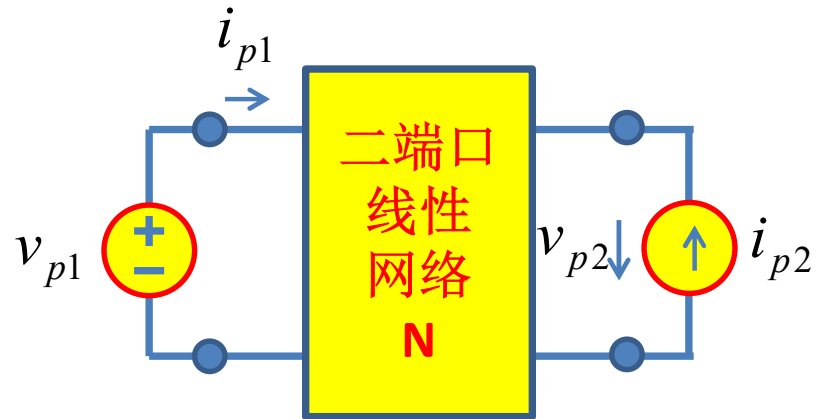
对LTI二端口网络的测量：4种基本测量手段



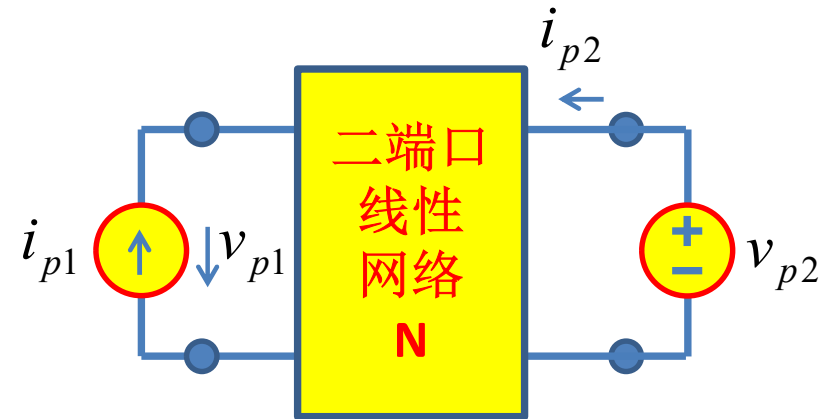
两个端口同时加独立变化的测试电压
y参量：在相量域，复数**Y**参量矩阵



两个端口同时加独立变化的测试电流
z参量：在相量域，复数**Z**参量矩阵

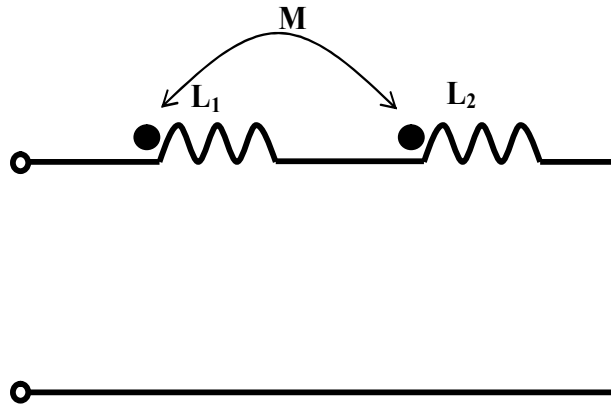


g参量：在相量域，复数**g**参量矩阵

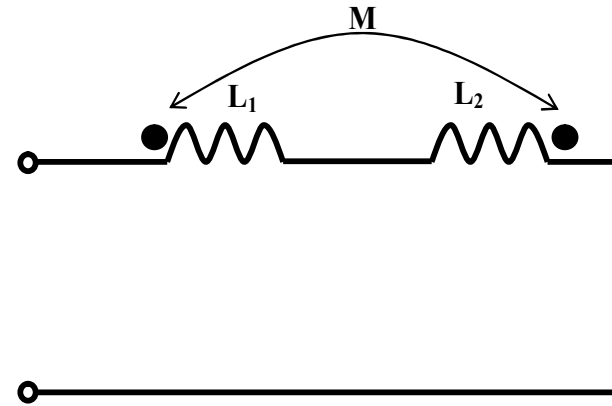


h参量：在相量域，复数**h**参量矩阵

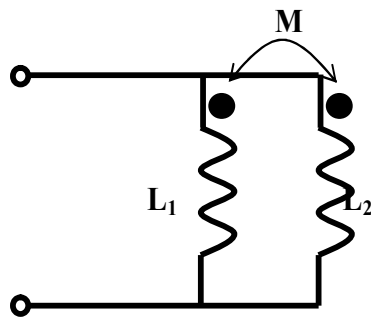
纯感网络，加流求压



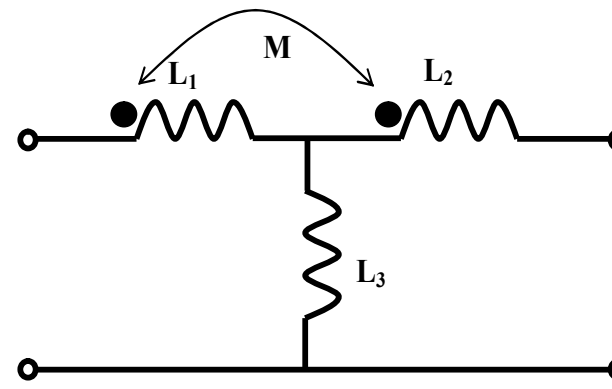
(a) 电感串联：带互感



(b) 电感串联：带互感，绕线反向

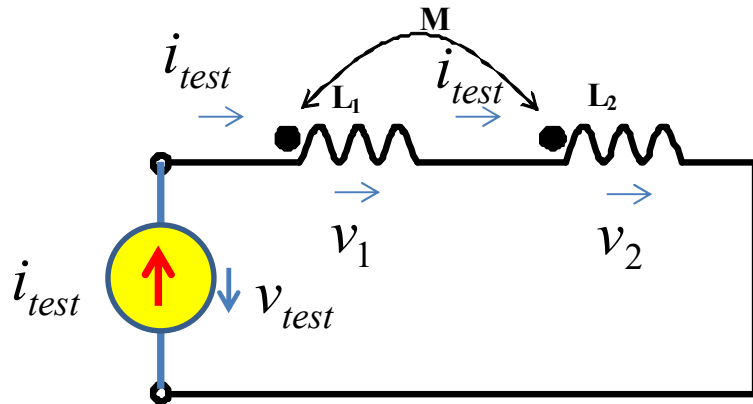


(c) 电感并联：带互感



(d) 二端口电感等效

带互感的电感串联 (1)



$$L = L_1 + L_2 + 2M$$

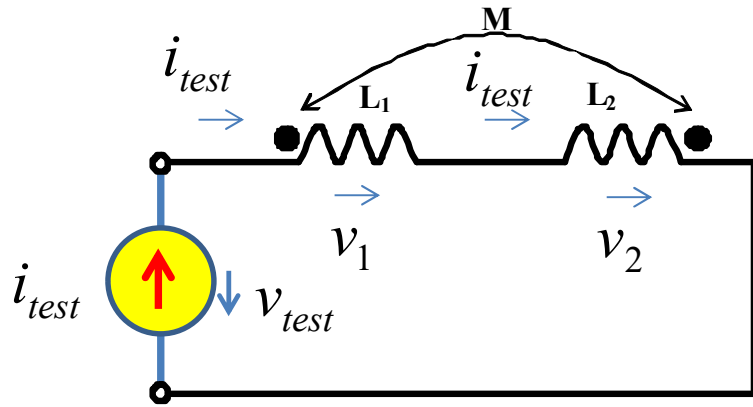
$$\begin{aligned} v_{test} &= v_1 + v_2 \\ &= \left(L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} \right) + \left(L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \right) \\ &= \left(L_1 \frac{di_{test}}{dt} + M \frac{di_{test}}{dt} \right) + \left(L_2 \frac{di_{test}}{dt} + M \frac{di_{test}}{dt} \right) \\ &= (L_1 + L_2 + 2M) \frac{di_{test}}{dt} \\ &= L \frac{di_{test}}{dt} \end{aligned}$$

磁芯电感

$$\begin{aligned} L &= N_1^2 \Xi + N_2^2 \Xi + 2kN_1N_2 \Xi \\ &= \sum_{k=1} (N_1^2 + N_2^2 + 2N_1N_2) \Xi \\ &= (N_1 + N_2)^2 \Xi = N^2 \Xi \end{aligned}$$

在磁环上绕 $N=N_1+N_2$ 圈的电感，可视为全耦合的 L_1 和 L_2 的电感串联，总电感 $L=L_1+L_2+2M$

带互感的电感串联 (2)



$$L = L_1 + L_2 - 2M$$

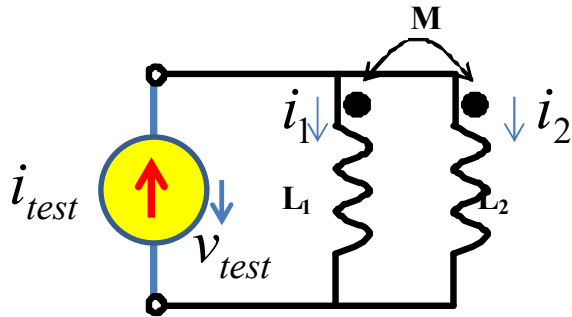
$$\begin{aligned}
 v_{test} &= v_1 + v_2 \\
 &= \left(L_1 \frac{di_1}{dt} - M \frac{di_2}{dt} \right) + \left(L_2 \frac{di_2}{dt} - M \frac{di_1}{dt} \right) \\
 &= \left(L_1 \frac{di_{test}}{dt} - M \frac{di_{test}}{dt} \right) + \left(L_2 \frac{di_{test}}{dt} - M \frac{di_{test}}{dt} \right) \\
 &= (L_1 + L_2 - 2M) \frac{di_{test}}{dt} \\
 &= L \frac{di_{test}}{dt}
 \end{aligned}$$

磁芯电感

$$\begin{aligned}
 L &= N_1^2 \Xi + N_2^2 \Xi - 2kN_1N_2 \Xi \\
 &\stackrel{k=1}{=} (N_1^2 + N_2^2 - 2N_1N_2) \Xi \\
 &= (N_1 - N_2)^2 \Xi
 \end{aligned}$$

在磁环上绕N1圈，再反向绕N1圈，则形成无电感导线回路。

带互感的电感并联 (1)



$$v_1 = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} = v_{test}$$

$$v_2 = L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} = v_{test}$$

$$\begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} \frac{di_1}{dt} \\ \frac{di_2}{dt} \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} v_{test}$$

$$i_{test} = i_1 + i_2$$

$$\frac{di_{test}}{dt} = \frac{di_1}{dt} + \frac{di_2}{dt} = \frac{L_2 - M + L_1 - M}{L_1 L_2 - M^2} v_{test}$$

$$v_{test} = \frac{L_1 L_2 - M^2}{L_2 + L_1 - 2M} \frac{di_{test}}{dt}$$

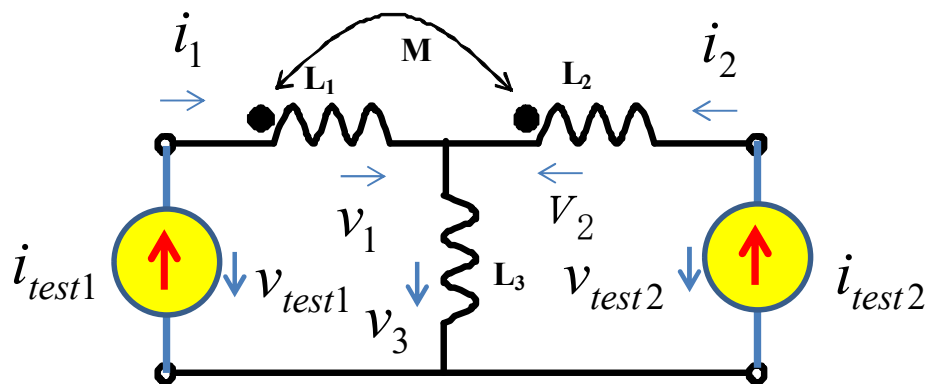
$$L = \frac{L_1 L_2 - M^2}{L_2 + L_1 - 2M}$$

$$\begin{bmatrix} \frac{di_1}{dt} \\ \frac{di_2}{dt} \end{bmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}^{-1} \cdot \begin{bmatrix} 1 \\ 1 \end{bmatrix} v_{test}$$

$$= \frac{1}{L_1 L_2 - M^2} \begin{bmatrix} L_2 & -M \\ -M & L_1 \end{bmatrix} \cdot \begin{bmatrix} 1 \\ 1 \end{bmatrix} v_{test}$$

$$= \frac{1}{L_1 L_2 - M^2} \begin{bmatrix} L_2 - M \\ L_1 - M \end{bmatrix} v_{test}$$

二端口电感等效



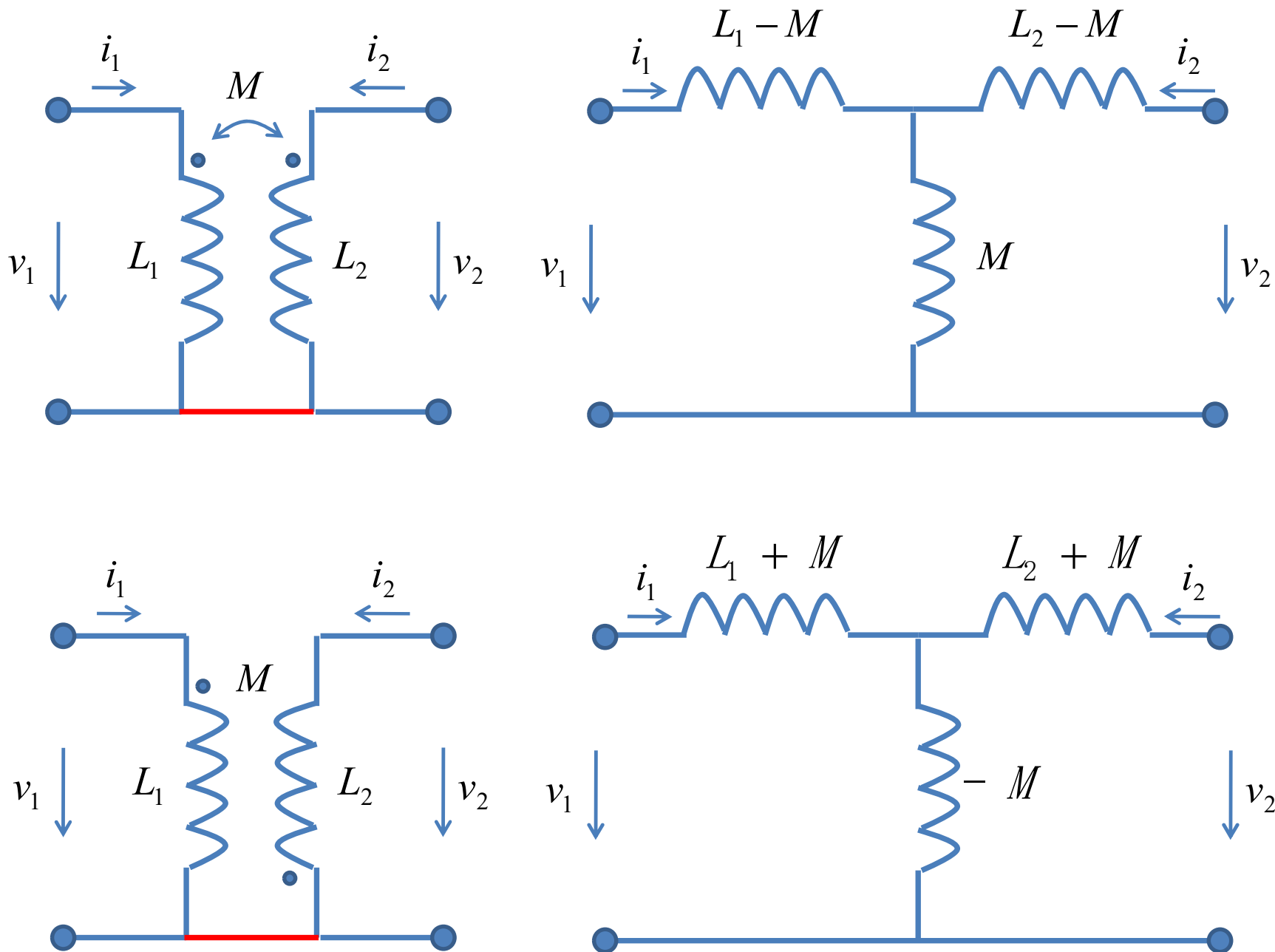
$$\begin{bmatrix} v_{test1} \\ v_{test2} \end{bmatrix} = \begin{bmatrix} L_1 + L_3 & L_3 - M \\ L_3 - M & L_2 + L_3 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} i_{test1} \\ i_{test2} \end{bmatrix}$$

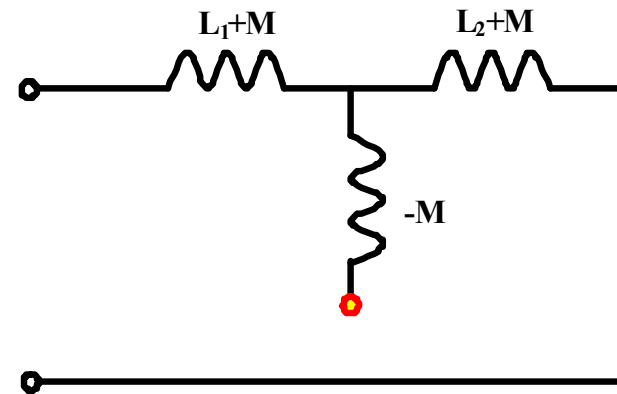
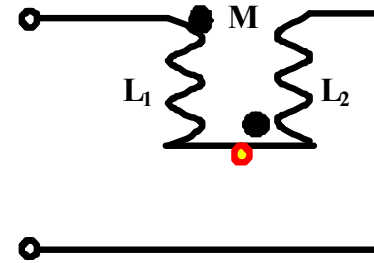
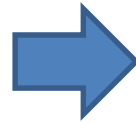
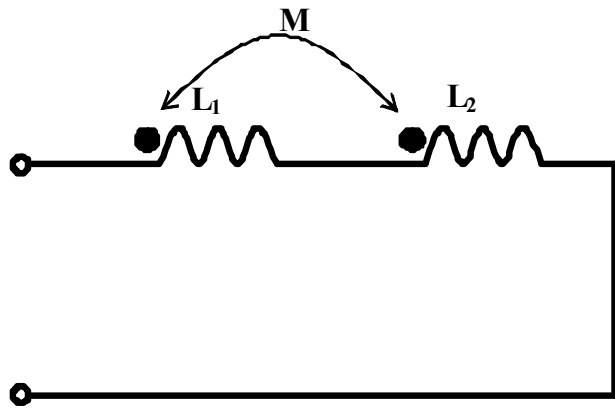
$$\mathbf{L} = \begin{bmatrix} L_1 + L_3 & L_3 - M \\ L_3 - M & L_2 + L_3 \end{bmatrix}$$

$$v_{test1} = v_1 + v_3 = L_1 \frac{di_1}{dt} - M \frac{di_2}{dt} + L_3 \frac{d(i_1 + i_2)}{dt} = (L_1 + L_3) \frac{di_1}{dt} + (L_3 - M) \frac{di_2}{dt}$$

$$v_{test2} = v_2 + v_3 = L_2 \frac{di_2}{dt} - M \frac{di_1}{dt} + L_3 \frac{d(i_1 + i_2)}{dt} = (L_2 + L_3) \frac{di_2}{dt} + (L_3 - M) \frac{di_1}{dt}$$

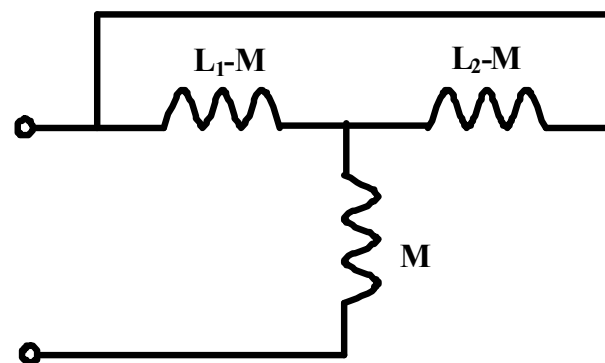
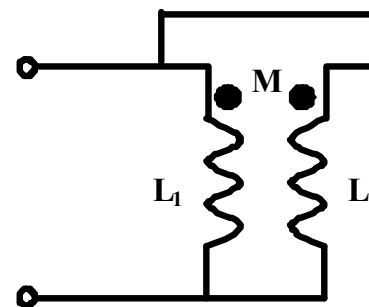
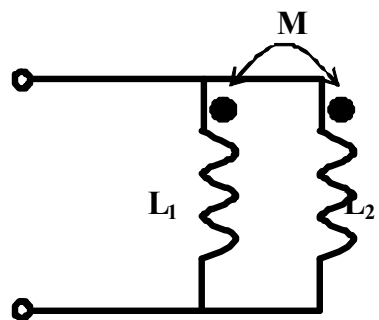
T型网络等效分析





$$L = (L_1 + M) + (L_2 + M)$$

$$= L_1 + L_2 + 2M$$

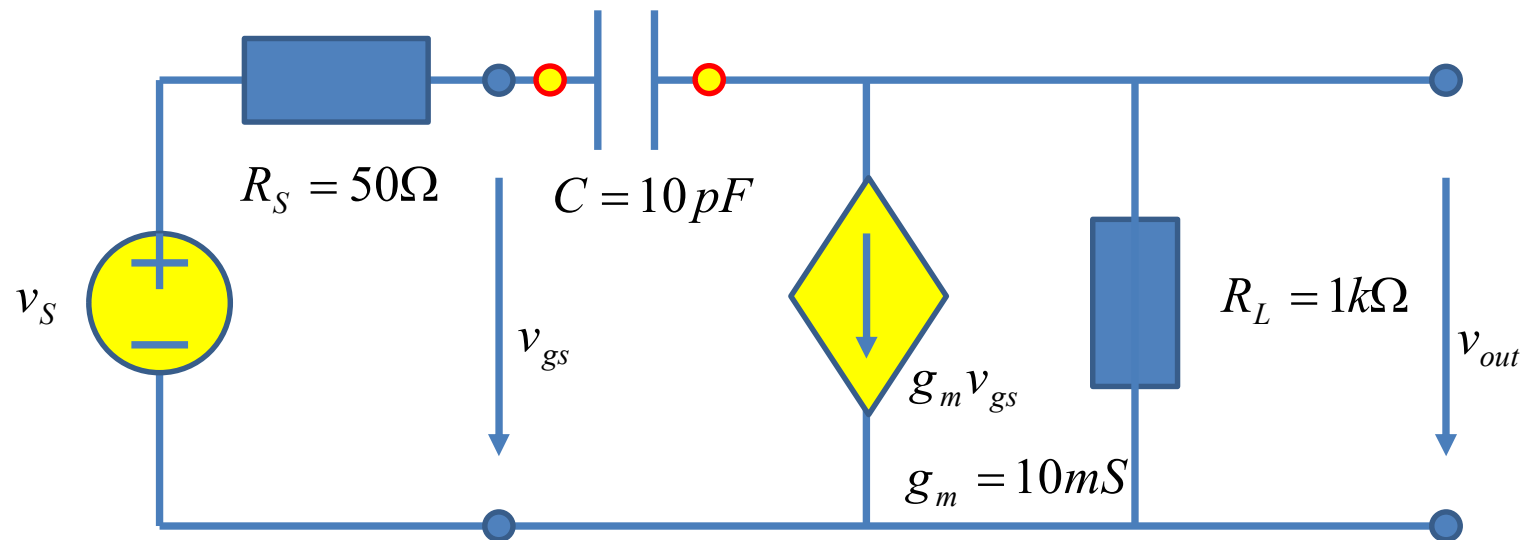


$$\begin{aligned}
 L &= ((L_1 - M) \parallel (L_2 - M)) \text{串} M \\
 &= \frac{1}{\frac{1}{L_1 - M} + \frac{1}{L_2 - M}} + M \\
 &= \frac{(L_1 - M)(L_2 - M)}{L_1 - M + L_2 - M} + M \\
 &= \frac{L_1 L_2 - M L_2 - M L_1 + M^2}{L_1 + L_2 - 2M} + \frac{(L_1 + L_2 - 2M)M}{L_1 + L_2 - 2M} \\
 &= \frac{L_1 L_2 - M^2}{L_1 + L_2 - 2M}
 \end{aligned}$$

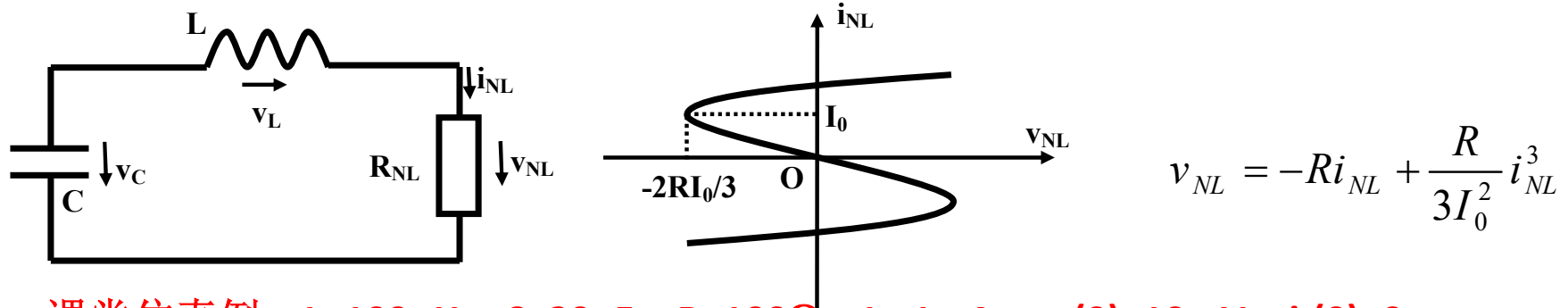
作业4 列写电路方程

(下节课和三要素法作业一并考察)

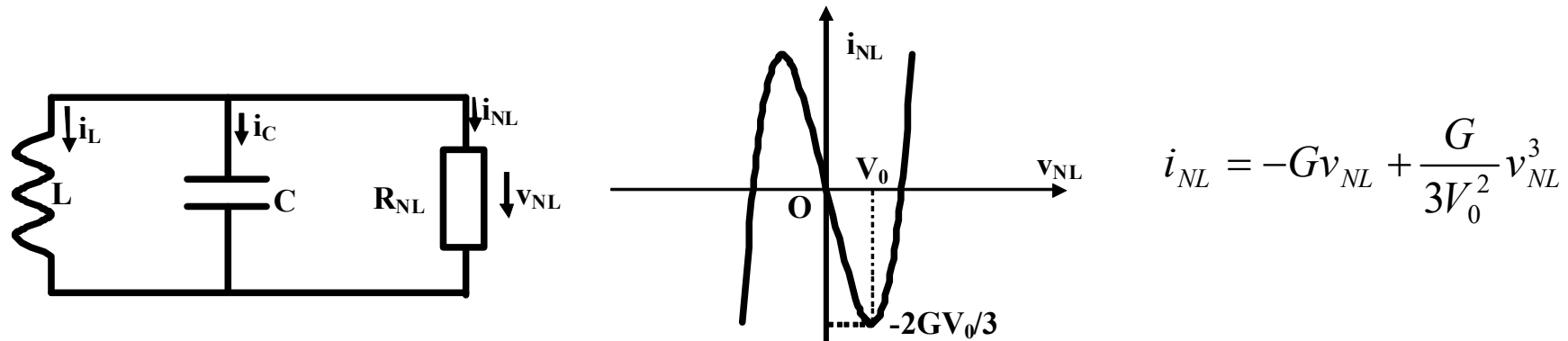
- 带跨接电容的跨导放大器
 - 将电容之外的电阻电路等效为戴维南源，列写关于电容电压 v_c 的电路方程（ v_c 为未知量 x ）
 - 列写关于 v_{out} 的电路方程（ v_{out} 为未知量 x ）



作业5（选作）：后向欧拉法仿真

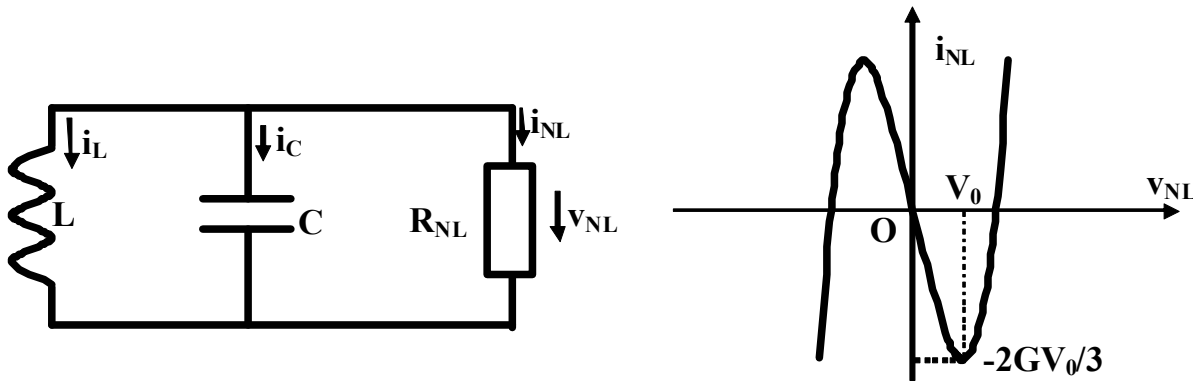


课堂仿真例： $L=100\mu\text{H}$, $C=20\text{pF}$, $R=100\Omega$, $I_0=1\text{mA}$, $v_C(0)=10\text{mV}$, $i_L(0)=0$



作业仿真例： $C=100\text{pF}$, $L=20\mu\text{H}$, $G=100\mu\text{S}$, $V_0=1\text{V}$, $v_C(0)=0$, $i_L(0)=10\text{mA}$

列写状态方程



$$i_{NL} = -Gv_{NL} + \frac{G}{3V_0^2}v_{NL}^3$$

$$0 = i_L + i_C + i_{NL} = i_L + C \frac{dv_C}{dt} - Gv_C + \frac{G}{3V_0^2}v_C^3$$

$$v_C = v_L = L \frac{di_L}{dt}$$

$$\frac{di_L}{dt} = \frac{1}{L}v_C$$

$$\frac{dv_C}{dt} = -\frac{1}{C}i_L + \frac{G}{C}v_C - \frac{G}{3CV_0^2}v_C^3$$

$$\frac{d}{dt} \begin{bmatrix} i_L \\ v_C \end{bmatrix} = \begin{bmatrix} \frac{1}{L}v_C \\ -\frac{1}{C}i_L + \frac{G}{C}v_C - \frac{G}{3CV_0^2}v_C^3 \end{bmatrix}$$

非线性时不变二阶动态系统

$$\frac{d}{dt} \mathbf{x} = f(\mathbf{x})$$

后向欧拉法

$$\frac{d}{dt} \begin{bmatrix} i_L \\ v_C \end{bmatrix} = \begin{bmatrix} \frac{1}{L} v_C \\ -\frac{1}{C} i_L + \frac{G}{C} v_C - \frac{G}{3CV_0^2} v_C^3 \end{bmatrix} \quad \frac{d}{dt} \mathbf{x} = f(\mathbf{x})$$
$$\mathbf{x}(t_{k+1}) = \mathbf{x}(t_k) + \Delta t \cdot f(\mathbf{x}(t_{k+1}))$$

$$\begin{bmatrix} i_L(t_{k+1}) \\ v_C(t_{k+1}) \end{bmatrix} = \begin{bmatrix} i_L(t_k) \\ v_C(t_k) \end{bmatrix} + \Delta t \cdot \begin{bmatrix} \frac{1}{L} v_C(t_{k+1}) \\ -\frac{1}{C} i_L(t_{k+1}) + \frac{G}{C} v_C(t_{k+1}) - \frac{G}{3CV_0^2} v_C^3(t_{k+1}) \end{bmatrix}$$

$$i_L(t_{k+1}) = i_L(t_k) + \frac{\Delta t}{L} v_C(t_{k+1}) = i_L(t_k) + \frac{1}{R_L} v_C(t_{k+1})$$

$$v_C(t_{k+1}) = v_C(t_k) - \frac{\Delta t}{C} i_L(t_{k+1}) + \frac{\Delta t G}{C} v_C(t_{k+1}) - \frac{\Delta t G}{3CV_0^2} v_C^3(t_{k+1})$$

$$= v_C(t_k) - R_C \left(i_L(t_k) + \frac{1}{R_L} v_C(t_{k+1}) \right) + \frac{R_C}{R} v_C(t_{k+1}) - \frac{R_C}{3RV_0^2} v_C^3(t_{k+1})$$

$$f(v_C(t_{k+1})) = \frac{R_C}{3RV_0^2} v_C^3(t_{k+1}) + \left(1 + \frac{R_C}{R_L} - \frac{R_C}{R} \right) v_C(t_{k+1}) - v_C(t_k) + R_C i_L(t_k)$$

此非线性方程可以用等效电路（电容戴维南源，电感诺顿源）同样获得 28

牛顿-拉夫逊迭代法求非线性代数方程

$$f(v_C(t_{k+1})) = \frac{R_C}{3RV_0^2} v_C^3(t_{k+1}) + \left(1 + \frac{R_C}{R_L} - \frac{R_C}{R}\right) v_C(t_{k+1}) - v_C(t_k) + R_C i_L(t_k)$$

$$f'(v_C(t_{k+1})) = \frac{R_C}{R} \frac{v_C^2(t_{k+1})}{V_0^2} + \left(1 + \frac{R_C}{R_L} - \frac{R_C}{R}\right)$$

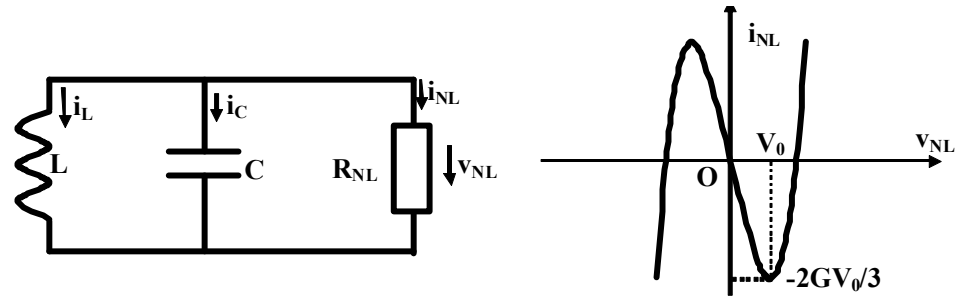
$$v_C^{(0)}(t_{k+1}) = v_C(t_k)$$

用前一时刻的状态做为这一时刻迭代初始值

$$v_C^{(j+1)}(t_{k+1}) = v_C^{(j)}(t_{k+1}) - \frac{f(v_C^{(j)}(t_{k+1}))}{f'(v_C^{(j)}(t_{k+1}))}$$

牛顿拉夫逊迭代格式

matlab初始设置



```
clear all
```

```
G=100E-6;
```

```
V0=1;
```

```
R=1/G;
```

```
L=20E-6;
```

```
C=100E-12;
```

```
vC(1)=0;
```

```
iL(1)=10E-3;
```

```
tt(1)=0;
```

```
Dt=1E-10;
```

```
RC=Dt/C;
```

```
RL=L/Dt;
```

```
%清空内存
```

```
%电路参量设置
```

```
%N型负阻参量
```

```
%并联电感
```

```
%并联电容
```

```
%电容初始电压
```

```
%电感初始电流
```

```
%时间起点
```

```
%时间步长
```

```
%后向欧拉法时间离散化电容等效电压源内阻
```

```
%后向欧拉法时间离散化电感等效电流源内阻
```

作业仿真例: $C=100\text{pF}$,

$L=20\mu\text{H}$, $G=100\mu\text{S}$, $V_0=1\text{V}$,

$v_C(0)=0$, $i_L(0)=10\text{mA}$

如果看不懂可请求帮助: **help**

- >> help clear
- CLEAR Clear variables and functions from memory.
- CLEAR removes all variables from the workspace.
- CLEAR VARIABLES does the same thing.
- CLEAR GLOBAL removes all global variables.
- CLEAR FUNCTIONS removes all compiled M- and MEX-functions.
-
- **CLEAR ALL removes all variables, globals, functions and MEX links.**
- CLEAR ALL at the command prompt also removes the Java packages import list.
-
- CLEAR IMPORT removes the Java packages import list at the command prompt. It cannot be used in a function.
-
- CLEAR CLASSES is the same as CLEAR ALL except that class definitions are also cleared...

后向欧拉法：前一个时间点的状态 是后一个时间状态的激励源

```
k=1;
for t=Dt:Dt:2E-5           %后向欧拉法时间步进计算
    k=k+1;
    tt(k)=t;

    %非线性代数方程的牛顿拉夫逊迭代法求解
    %迭代初始值设置为上个时间点的数值解
    vC(k)=vC(k-1);
    flag=0;
    while flag==0
        f=(1+RC/RL-RC/R)*vC(k)+RC/R/3/VO^2*vC(k)^3-vC(k-1)+RC*iL(k-1); %非线性方程
        fp=1+RC/RL-RC/R+RC/R*(vC(k)/VO)^2;                               %微分斜率
        vC(k)=vC(k)-f/fp;                                                %牛顿拉夫逊迭代

        if abs(f)<1E-9           %迭代结束标记
            flag=1;
        end
    end

    iL(k)=iL(k-1)+vC(k)/RL;      %求电感电流
end
```

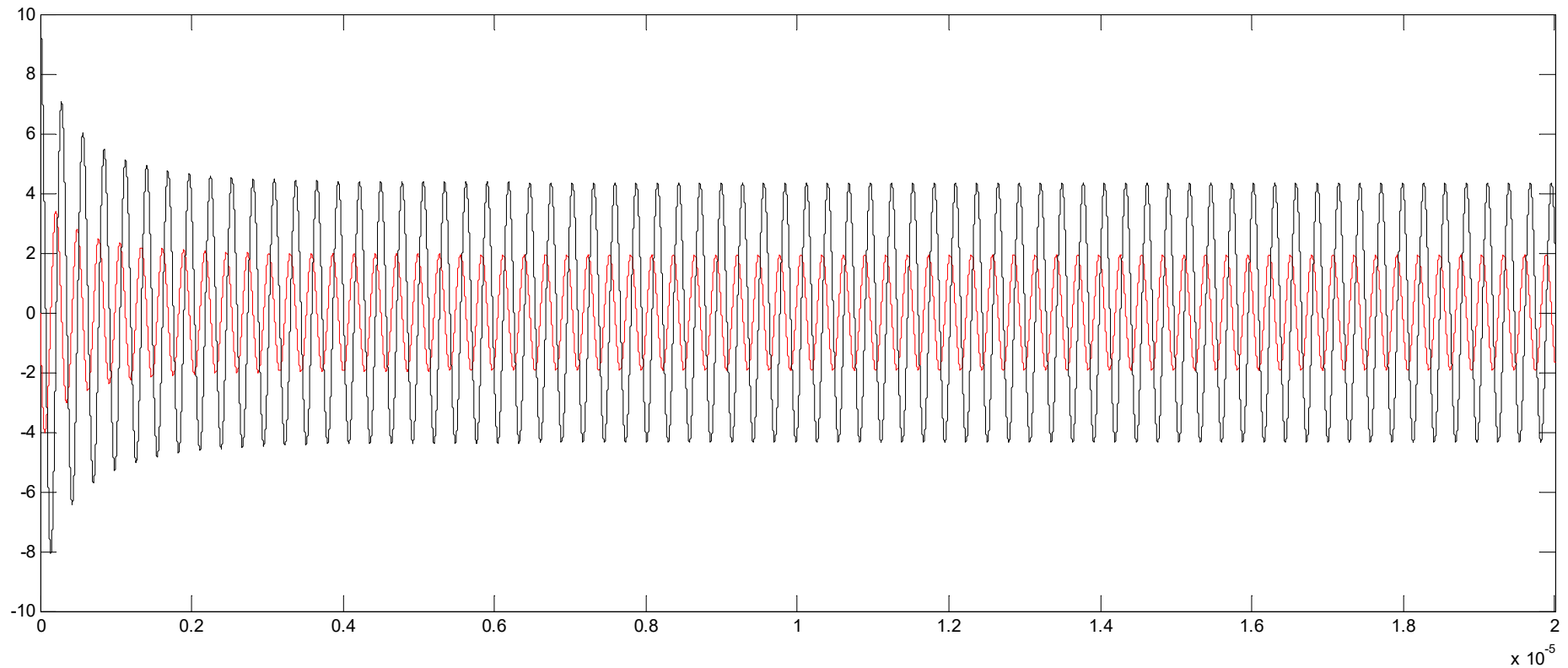
$$f(v_C(t_{k+1})) = \left(1 + \frac{R_C}{R_L} - \frac{R_C}{R}\right) v_C(t_{k+1}) + \frac{R_C}{3RV_0^2} v_C^3(t_{k+1}) - v_C(t_k) + R_C i_L(t_k)$$

$$i_L(t_{k+1}) = i_L(t_k) + \frac{1}{R_L} v_C(t_{k+1})$$

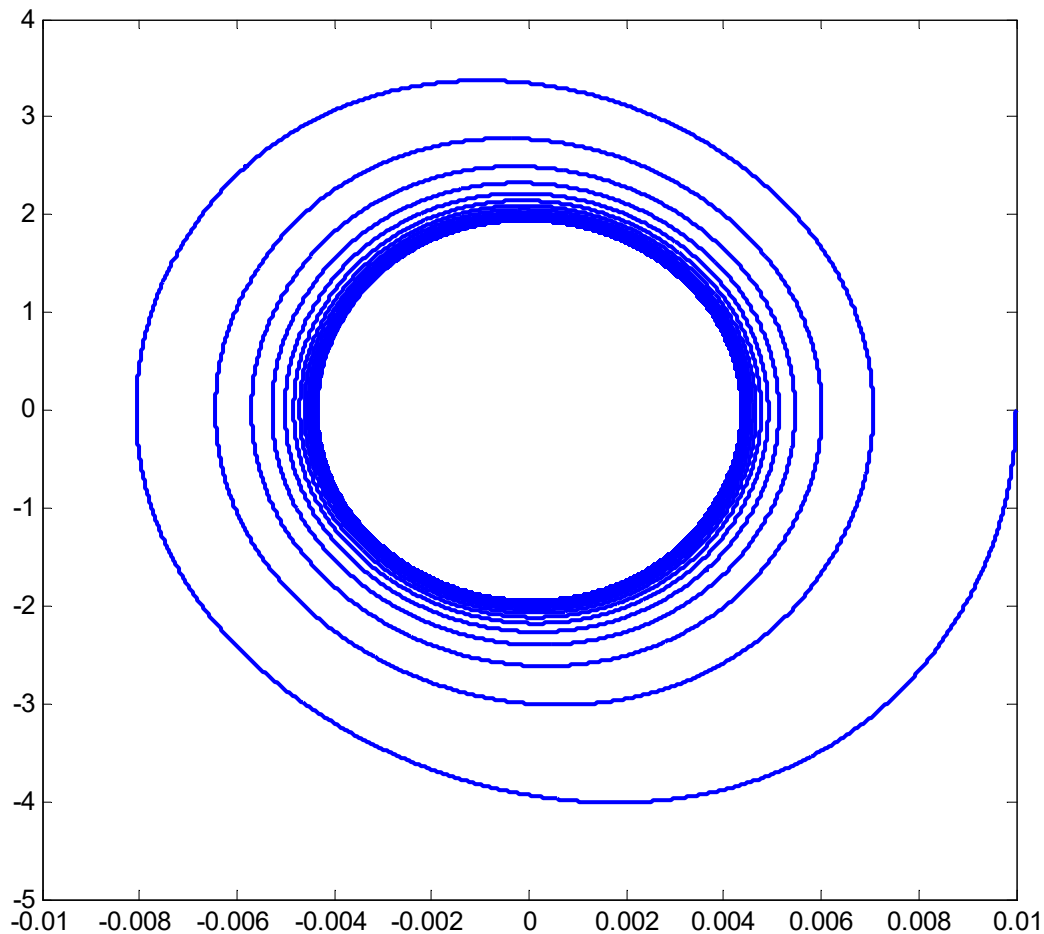
输出：作图

```
figure(1)
hold on      %保持在一张图上画数条曲线
plot(tt,vC,'r') %电容电压时域波形（单位V）
plot(tt,iL*1E3,'k') %电感电流时域波形（单位mA）
```

```
figure(2)    %相图
plot(iL,vC)
```

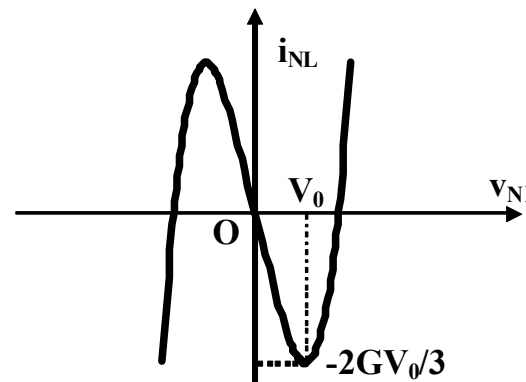
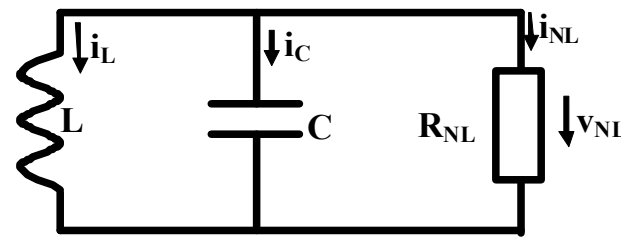


相轨迹



相轨迹收敛到一个圆形极限环上，说明这是一个正弦波振荡器；

由于初始状态较大，使得非线性电阻起始阶段工作在正阻区，故而起始呈现振幅衰减振荡波形，随着振荡幅度的降低，负导效应增强。当负导效应和正导效应相互抵偿时，则电路中只剩下纯的LC谐振腔，能量转换呈现正弦形态

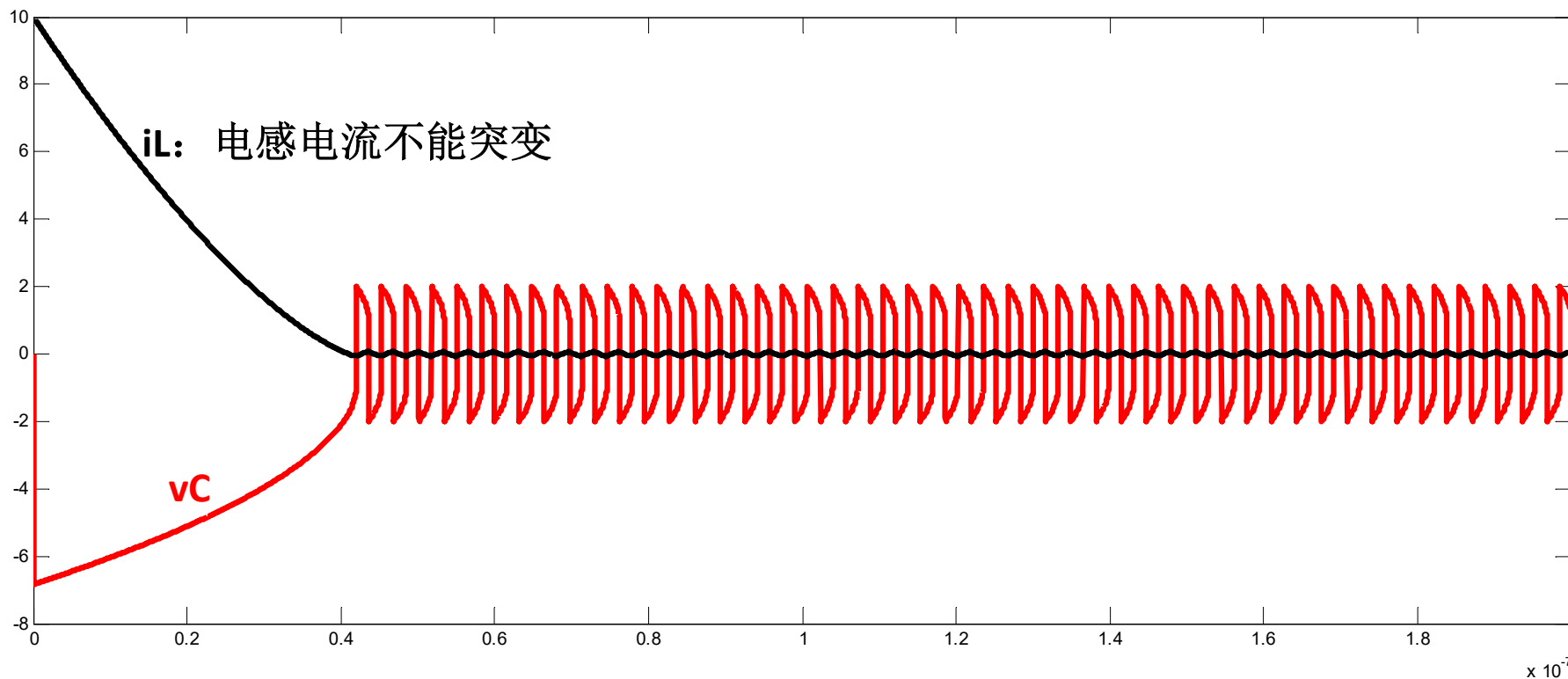
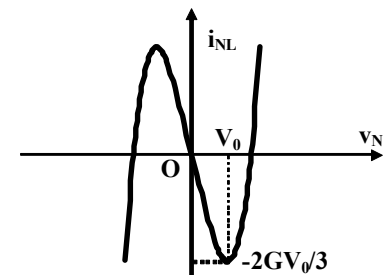
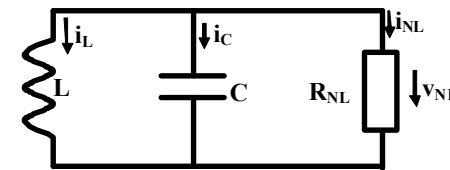


张弛振荡

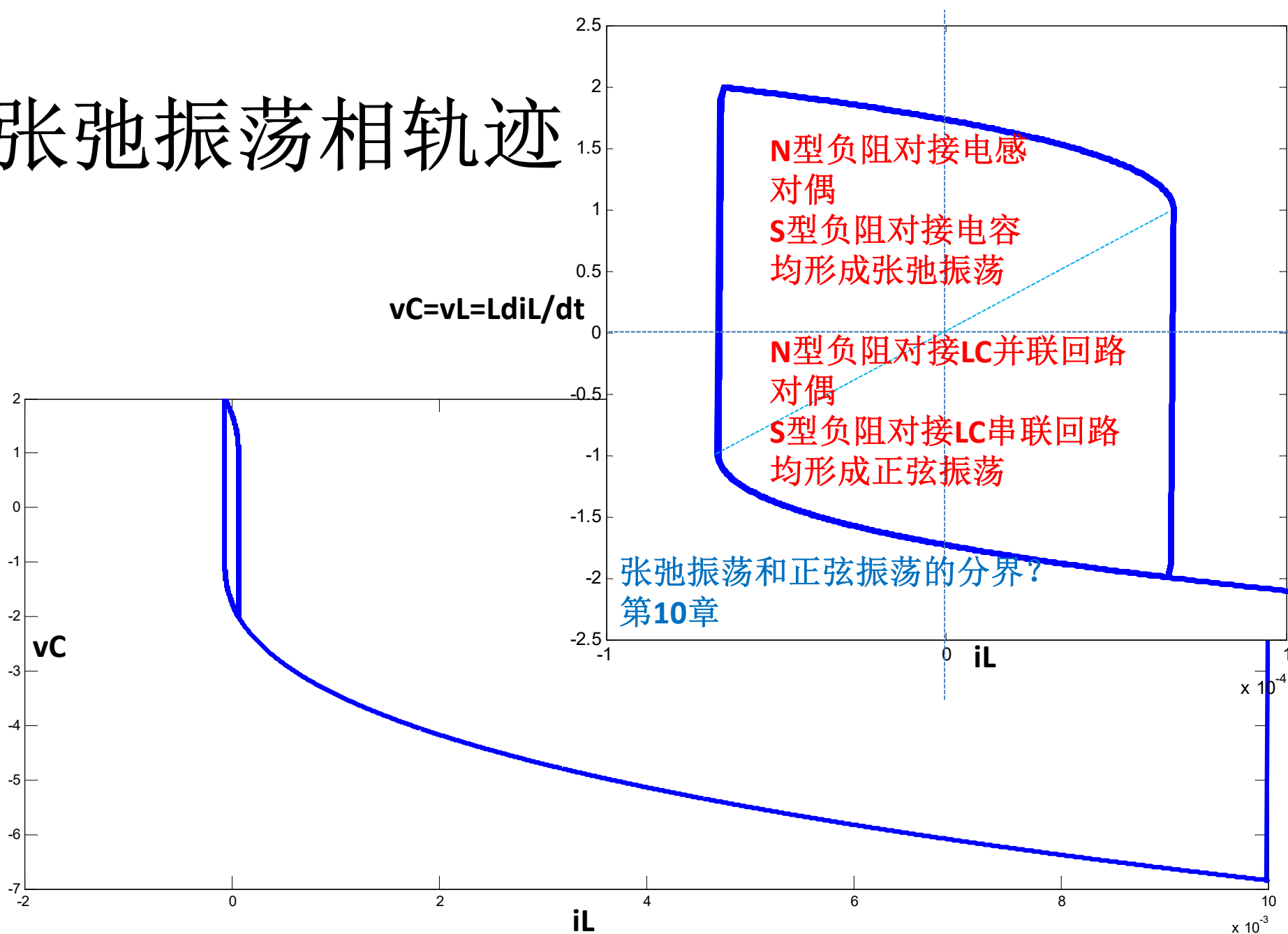
$$C = 100\text{pF} \rightarrow 0.1\text{fF}$$

极小电容视为开路

电感+N型负阻：张弛振荡



张弛振荡相轨迹

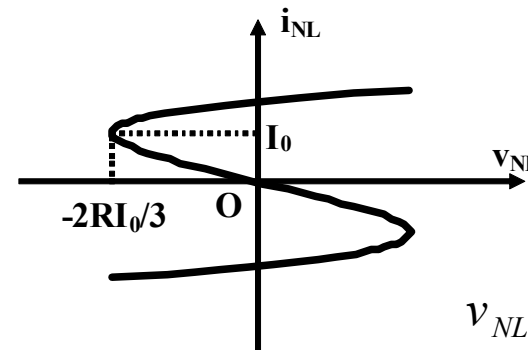
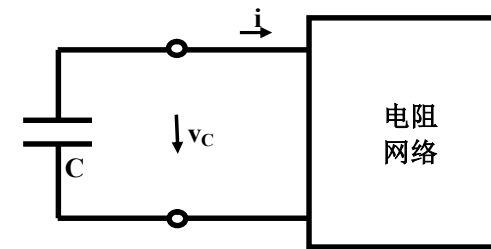


第3讲 动态电路基本分析方法

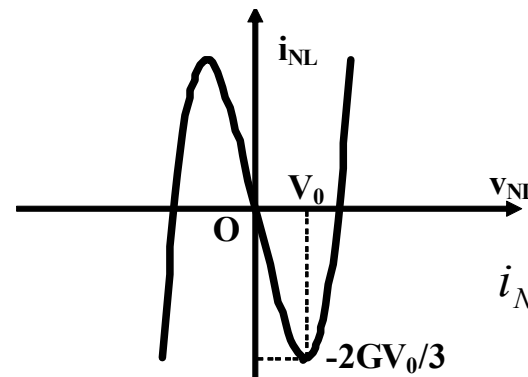
作业1 一阶动态系统的相轨迹

- (练习8.2.9) 图示单电容一阶动态系统中的电阻网络，分别为如下五种情况，请画出相图，并说明平衡点在什么位置？是否稳定？是否会出现振荡？

- 线性电阻 R
- 线性负阻 $-R$
- 戴维南源，源电压为 V_{S0} ，源内阻为 R_S
- S型负阻
- N型负阻

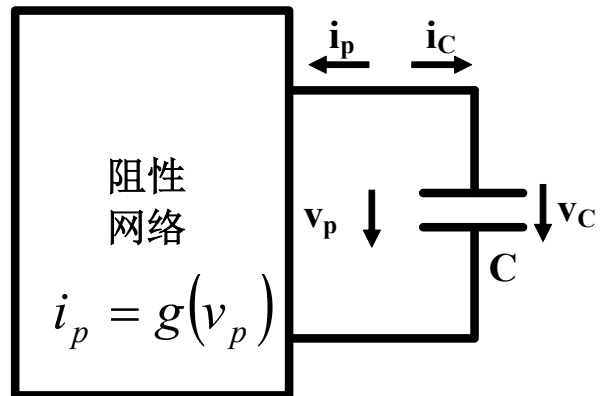


$$v_{NL} = -Ri_{NL} + \frac{R}{3I_0^2} i_{NL}^3$$



$$i_{NL} = -Gv_{NL} + \frac{G}{3V_0^2} v_{NL}^3$$

一阶RC电路：相图



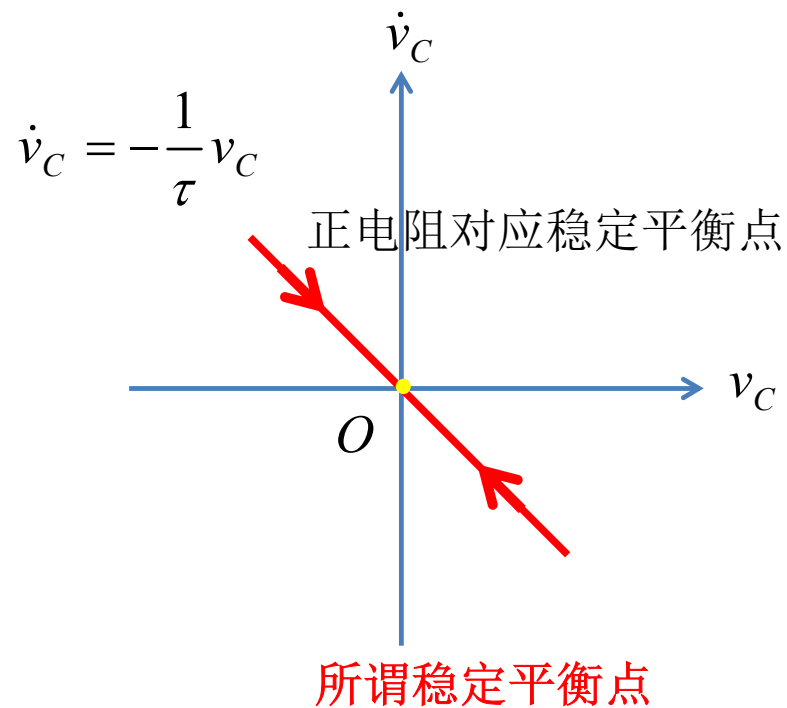
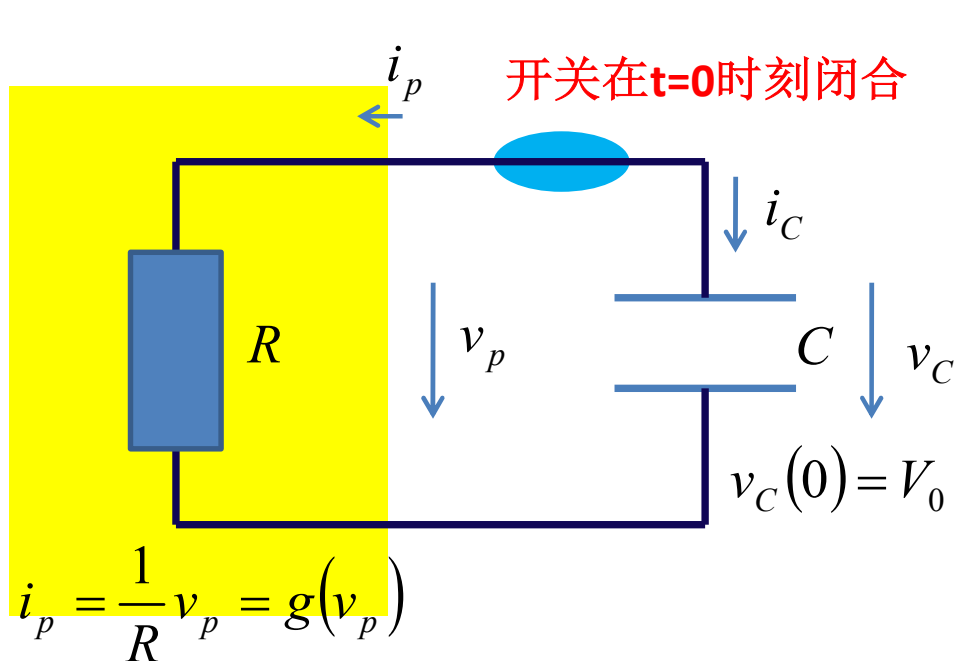
$$C \frac{dv_C}{dt} = i_C = -i_p = -g(v_p) = -g(v_C)$$

$$\frac{dv_C(t)}{dt} = -\frac{1}{C} g(v_C(t)) \quad \text{状态方程}$$

$$y = -\frac{1}{C} g(x) \quad \text{相轨迹}$$

$$x = v_C(t)$$
$$y = \frac{dv_C(t)}{dt}$$

(1) 电阻网络为线性电阻



$$\frac{dv_C(t)}{dt} = -\frac{1}{C}g(v_C(t)) = -\frac{1}{C}\frac{v_C(t)}{R} = -\frac{1}{RC}v_C(t) = -\frac{1}{\tau}v_C(t)$$

$$y = -\frac{1}{\tau}x$$

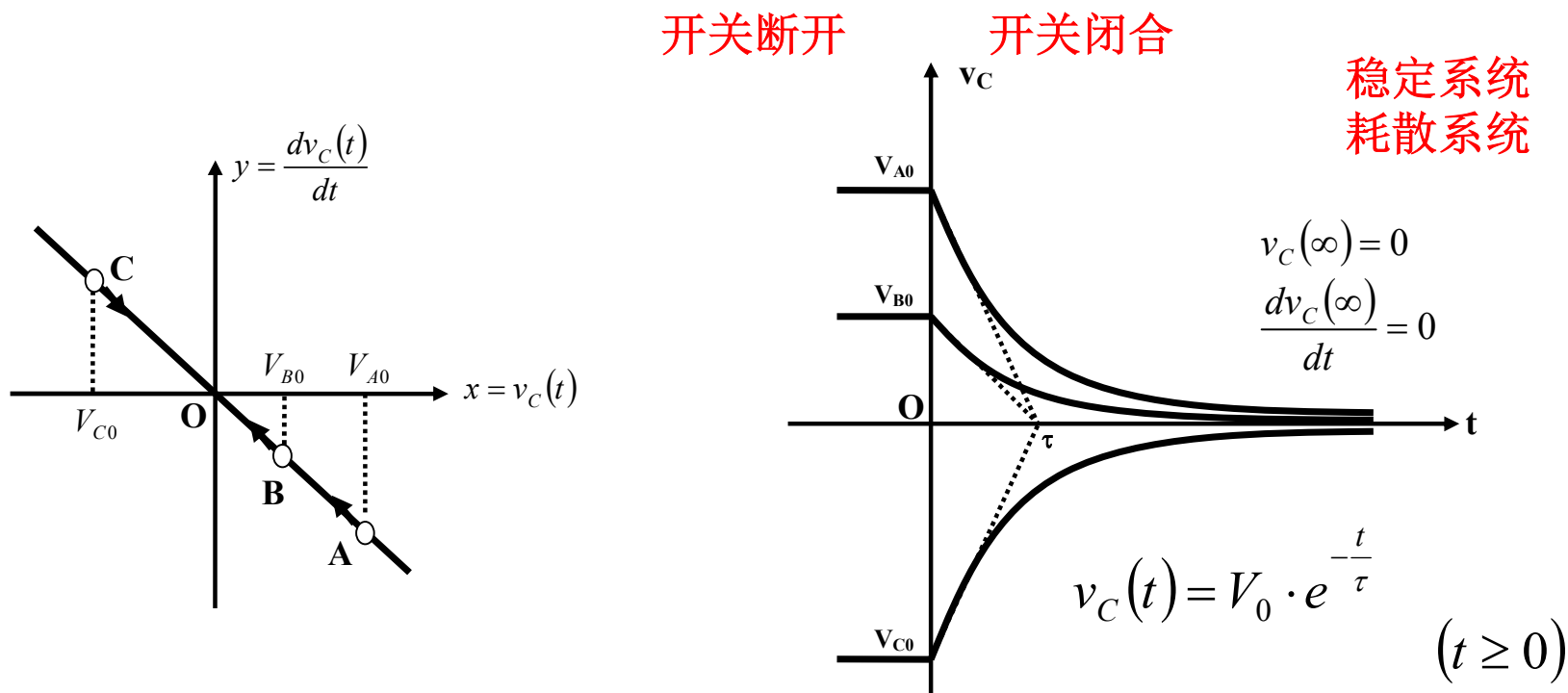
时间常数 $\tau = RC$

$t \rightarrow \infty$

$$v_C(t) \rightarrow 0$$

$$\frac{dv_C(t)}{dt} \rightarrow 0$$

不同初值，放电曲线形态一致

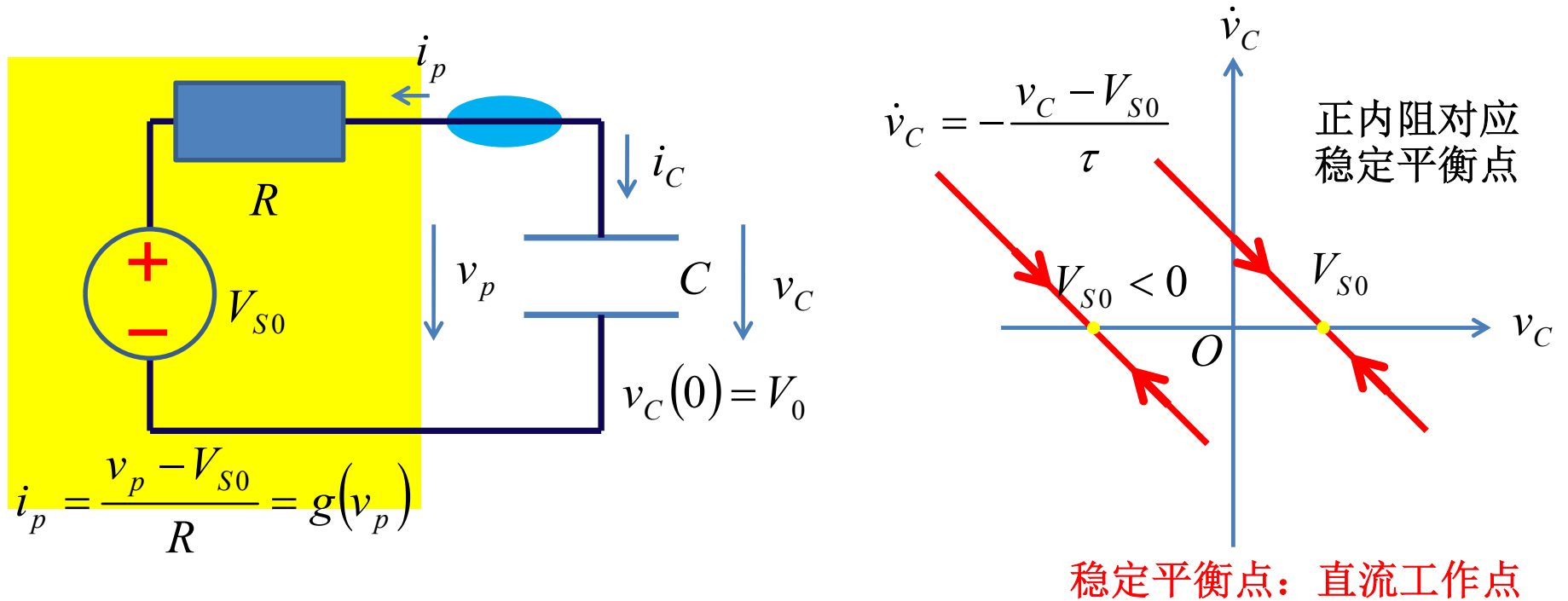


相轨迹的斜率 $-1/\tau$ ，代表了状态转移速度

时间常数越小，相轨迹越陡，状态转移速度越快，从一个状态转移到下一个状态用的时间就越短

$R=0, \tau=0$ ，瞬间完成放电（冲激电流）

(2) 电阻网络为直流戴维南源



$$\frac{dv_C(t)}{dt} = -\frac{1}{C} g(v_C(t)) = -\frac{1}{C} \frac{v_C(t) - V_{S0}}{R} = -\frac{1}{\tau} v_C(t) + \frac{1}{\tau} V_{S0}$$

$$y = -\frac{x - V_{S0}}{\tau}$$

时间常数 $\tau = RC$

$$t \rightarrow \infty$$

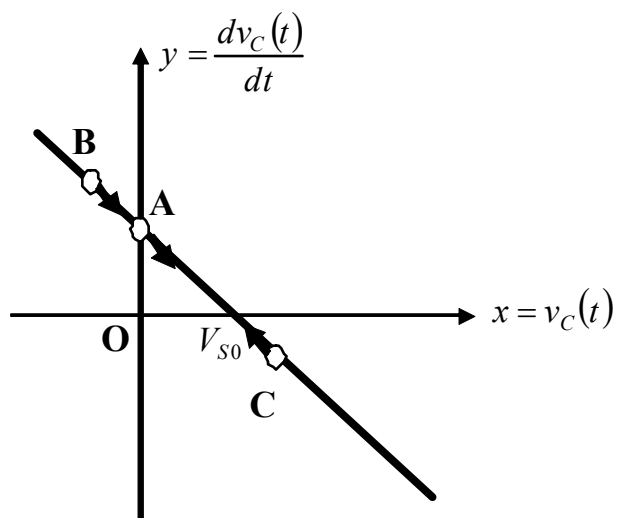
$$v_C(t) \rightarrow V_{S0}$$

$$\frac{dv_C(t)}{dt} \rightarrow 0$$

不同初值，形态一致

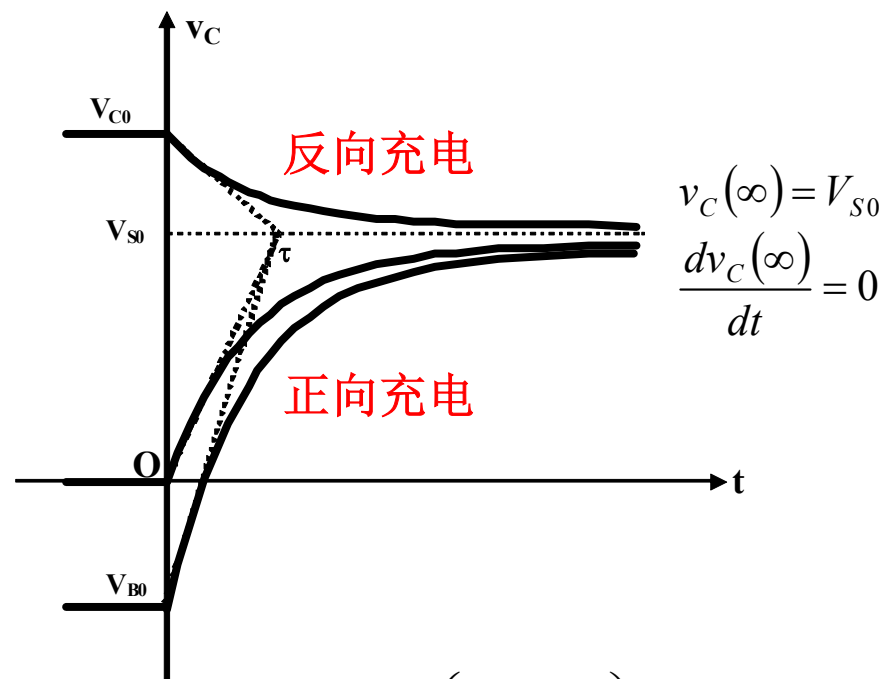
开关断开

开关闭合



$$\frac{dv_C(t)}{dt} = -\frac{1}{\tau} v_C(t) + \frac{1}{\tau} V_{S0}$$

$$y = -\frac{x - V_{S0}}{\tau}$$



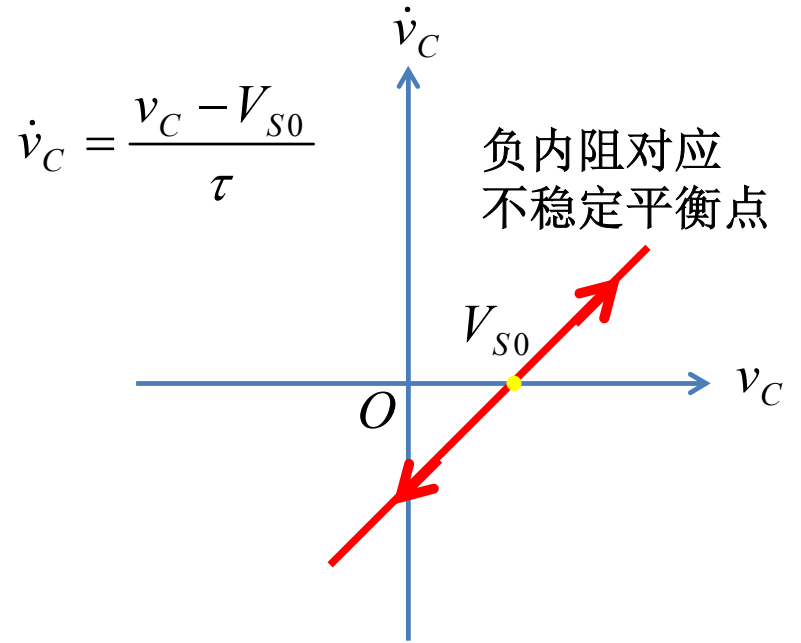
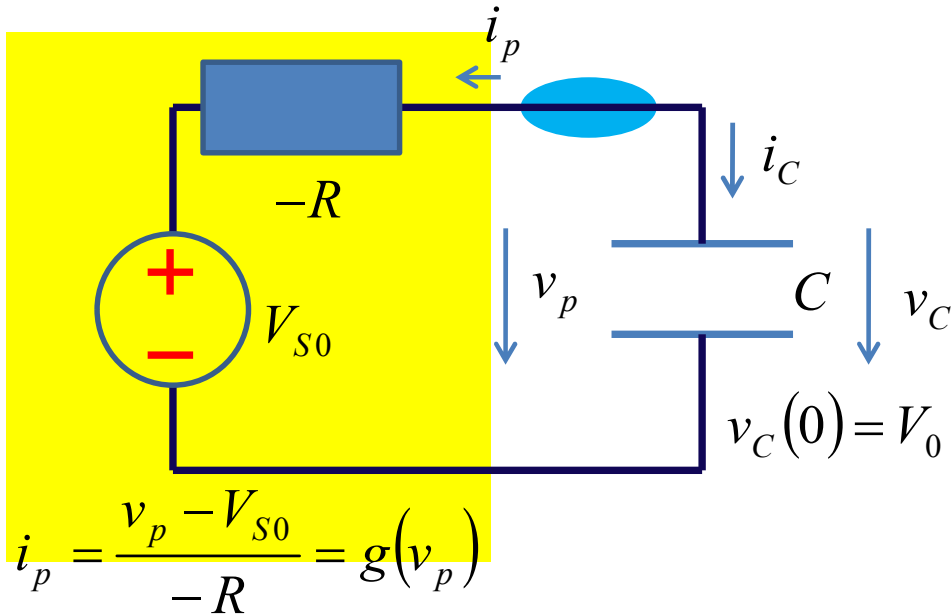
$$v_C(\infty) = V_{S0}$$

$$\frac{dv_C(\infty)}{dt} = 0$$

$$v_C(t) = V_0 + (V_{S0} - V_0) \left(1 - e^{-\frac{t}{\tau}}\right) \cdot U(t)$$

$$= \begin{cases} V_0 & t < 0 \\ V_{S0} + (V_0 - V_{S0}) e^{-\frac{t}{\tau}} & t \geq 0 \end{cases}$$

(3) 戴维南源内阻为负阻



不稳定平衡点：直流工作点

$$\frac{dv_C(t)}{dt} = -\frac{1}{C} g(v_C(t)) = -\frac{1}{C} \frac{v_C(t) - V_{S0}}{-R} = \frac{1}{\tau} v_C(t) - \frac{1}{\tau} V_{S0}$$

$$y = \frac{x - V_{S0}}{\tau}$$

时间常数 $\tau = RC$

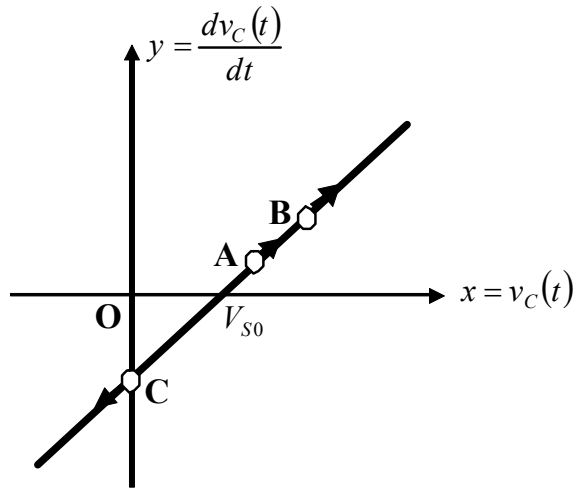
假设时间可以倒流

$$t \rightarrow -\infty$$

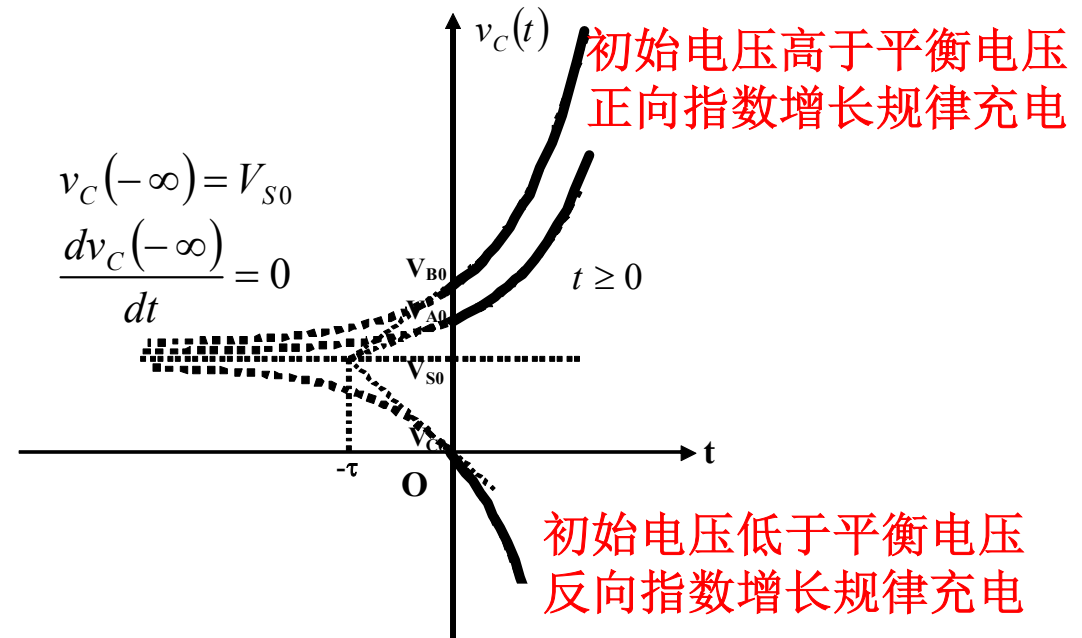
$$v_C(t) \rightarrow V_{S0}$$

$$\frac{dv_C(t)}{dt} \rightarrow 0$$

不同初值，形态一致



$$\begin{aligned} \frac{dv_C(t)}{dt} &= \frac{v_C(t) - V_{S0}}{\tau} \\ &= \frac{V_0 - V_{S0}}{\tau} e^{\frac{t}{\tau}} \end{aligned}$$



$$\begin{aligned} v_C(t) &= v_{C,\infty}(t) + (v_C(0^+) - v_{C,\infty}(0^+)) e^{\frac{t}{\tau}} \\ &= V_{S0} + (V_0 - V_{S0}) e^{\frac{t}{\tau}} \quad (t \geq 0) \end{aligned}$$

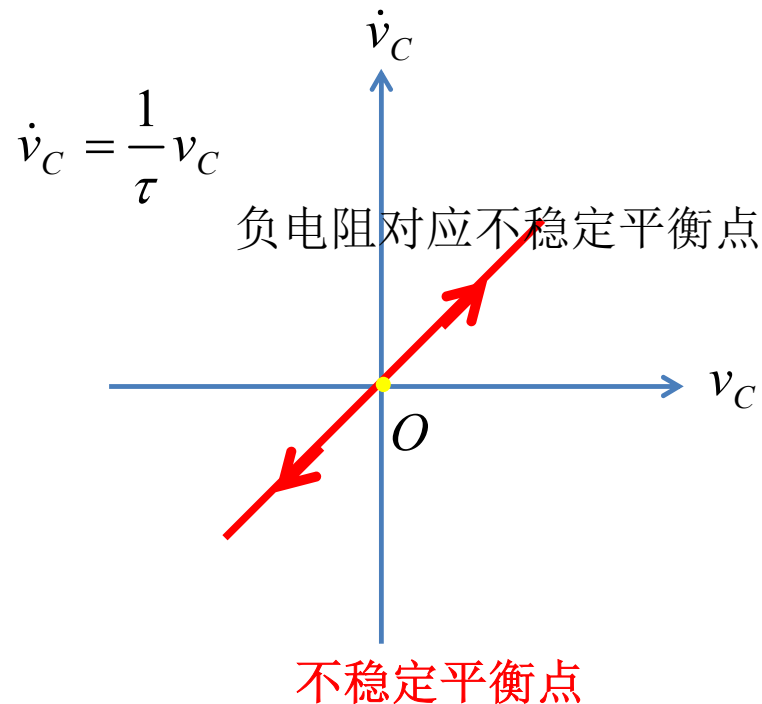
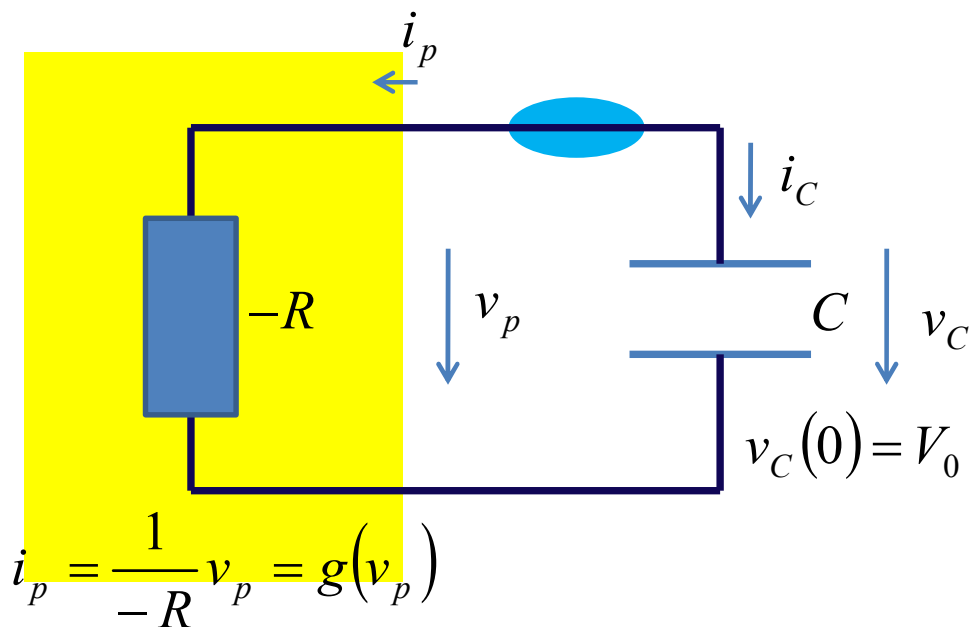
- 1、代入方程，成立，确实为解
- 2、代入 $t=0$ ，确实为初值 $v_C(0)=V_0$

三要素形式没有任何本质区别

- 1、指数增长规律
- 2、稳态值为 $t \rightarrow -\infty$ 时的不稳定平衡状态

(3.2) 电阻网络为线性负阻

戴维南源电压为零



$$\frac{dv_C(t)}{dt} = -\frac{1}{C} g(v_C(t)) = -\frac{1}{C} \frac{v_C(t)}{-R} = \frac{1}{RC} v_C(t) = \frac{1}{\tau} v_C(t)$$

$$y = \frac{1}{\tau} x$$

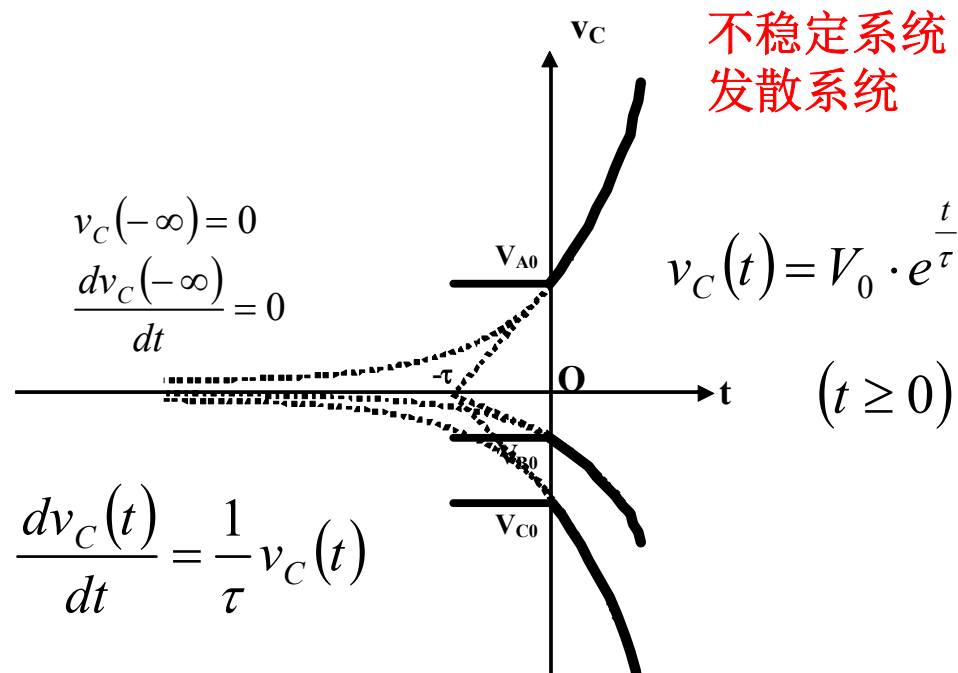
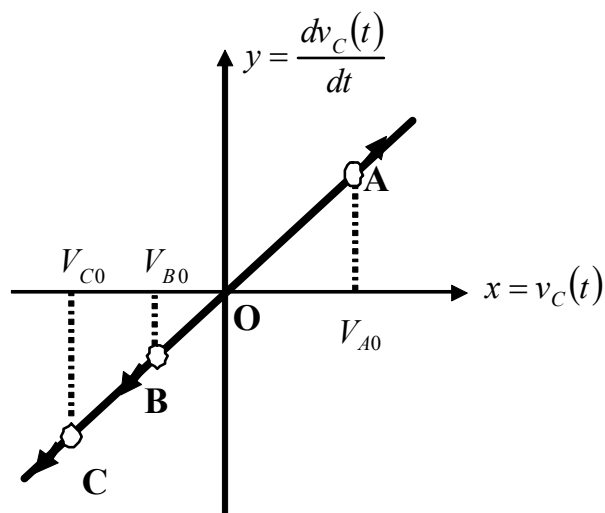
时间常数 $\tau = RC$

$$t \rightarrow -\infty$$

$$v_C(t) \rightarrow 0$$

$$\frac{dv_C(t)}{dt} \rightarrow 0$$

负阻为电容充电：越充越快



不稳定系统
发散系统

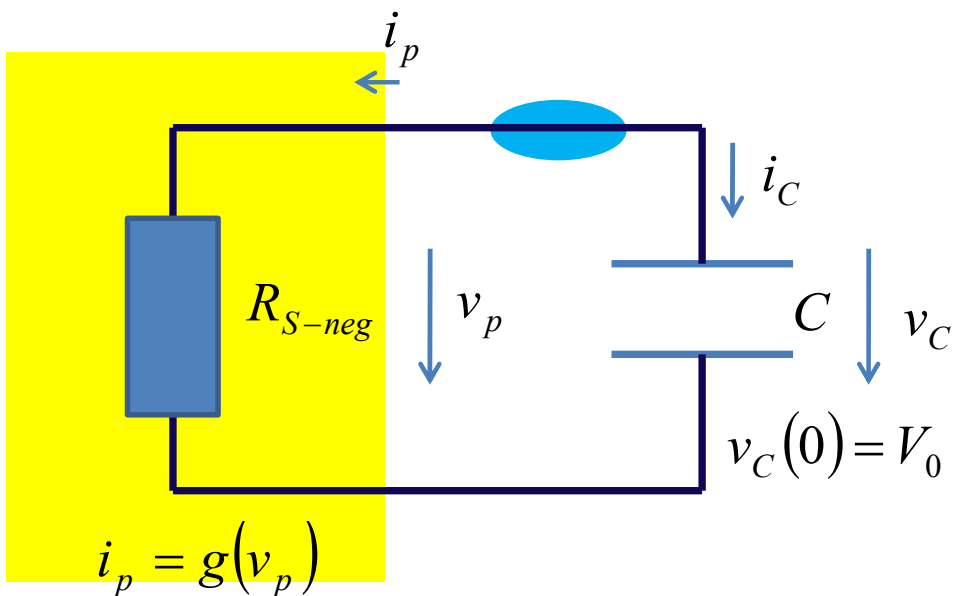
指数增长规律

$$\frac{dv_C(t)}{dt} = \frac{v_C(t) - V_{S0}}{\tau} \stackrel{V_{S0}=0}{=} \frac{v_C(t)}{\tau}$$

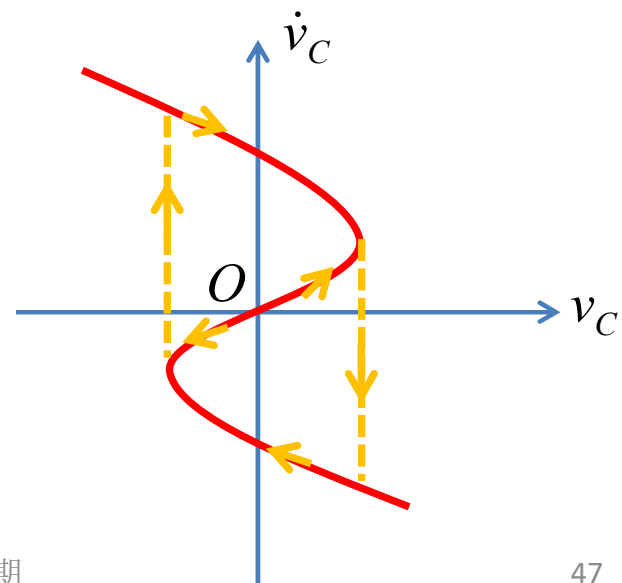
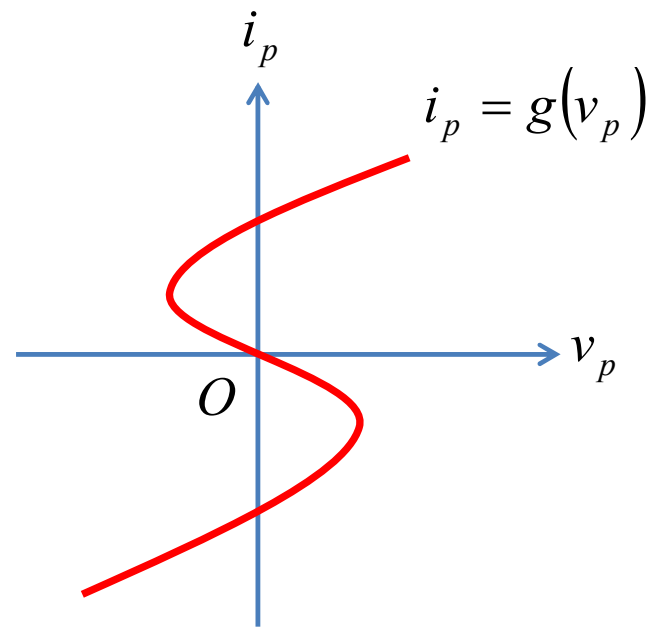
直流偏置清零
以 V_{S0} 为参考0电位即可

$$(v_C(t) - V_{S0}) = (V_0 - V_{S0}) \cdot e^{\frac{t}{\tau}}$$

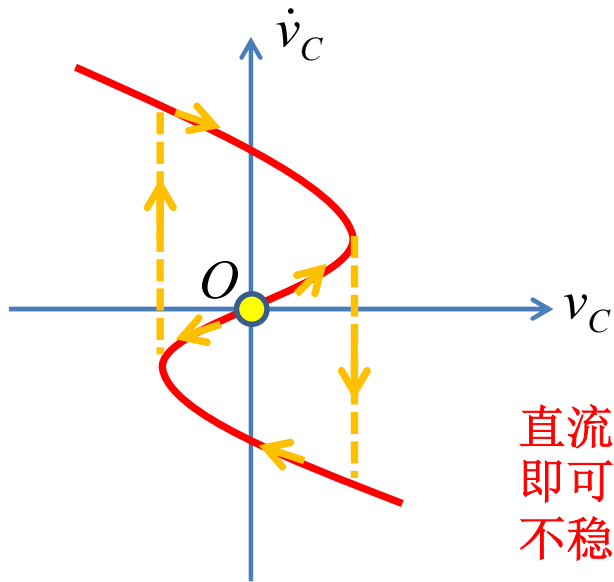
(4) S型负阻



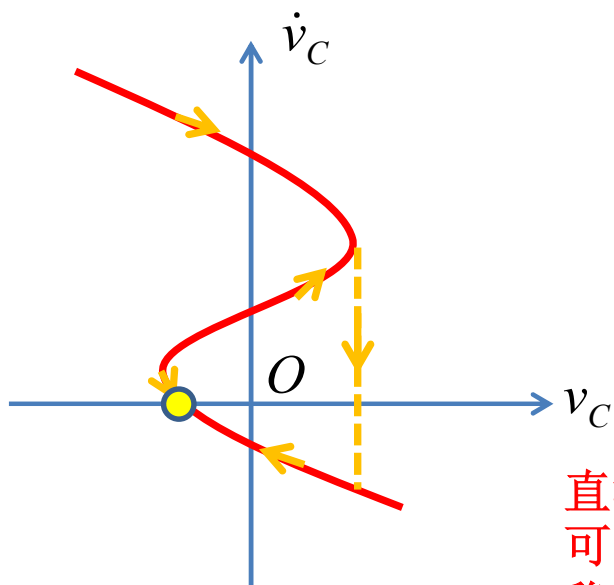
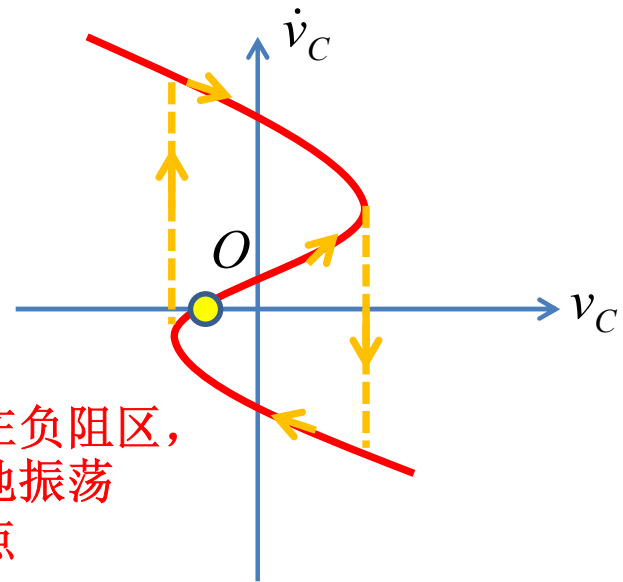
$$\frac{dv_C(t)}{dt} = -\frac{1}{C}g(v_C(t))$$



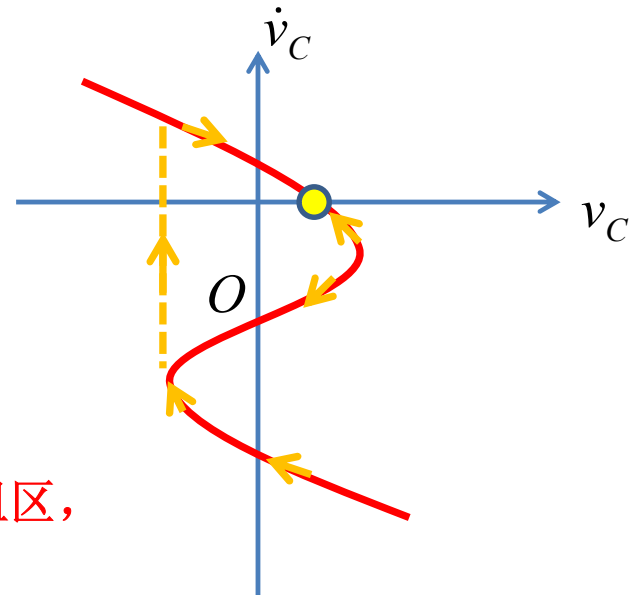
S型负阻的不同直流工作点



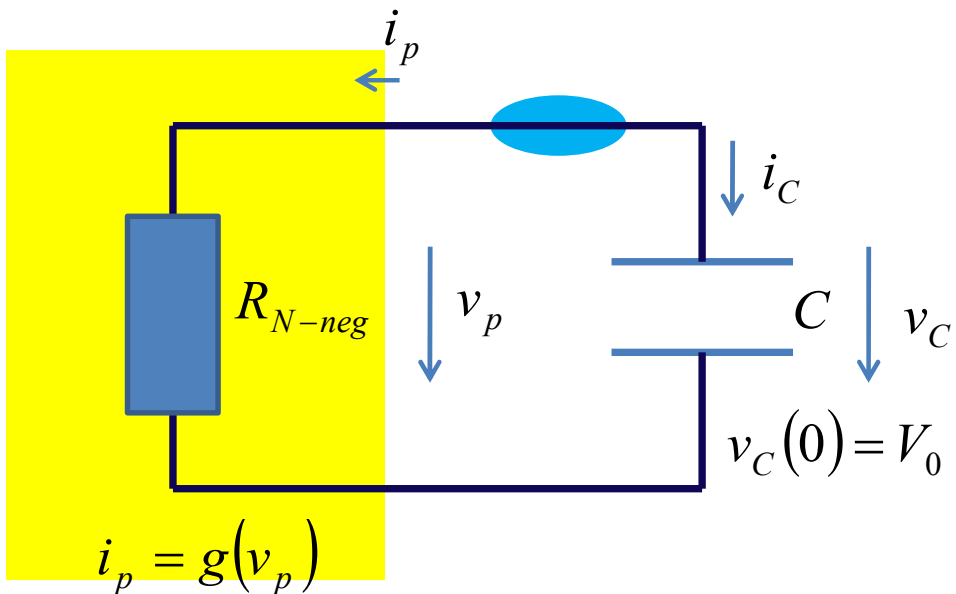
直流工作点在负阻区，
即可形成张弛振荡
不稳定平衡点



直流工作点在正阻区，
可能形成单脉冲
稳定平衡点

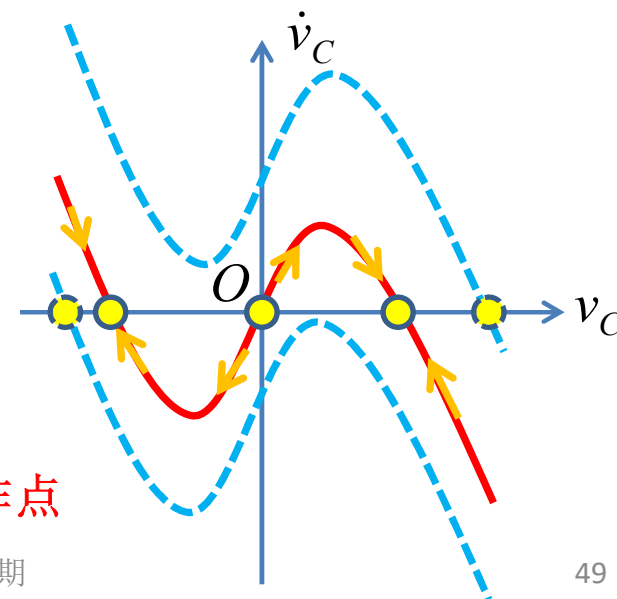
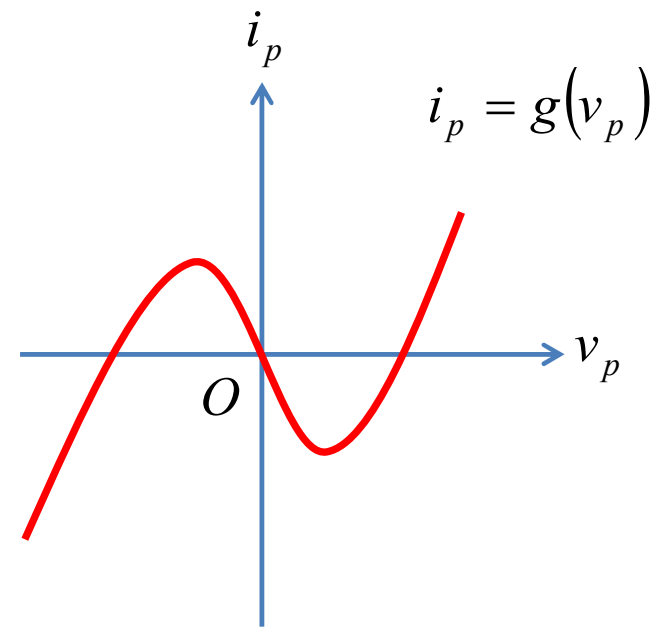


(5) N型负阻

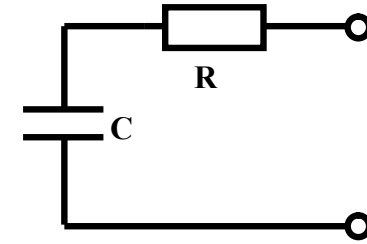


$$\frac{dv_C(t)}{dt} = -\frac{1}{C} g(v_C(t))$$

直流工作点在负阻区
可形成两个记忆状态
必然同时存在两个正阻工作点



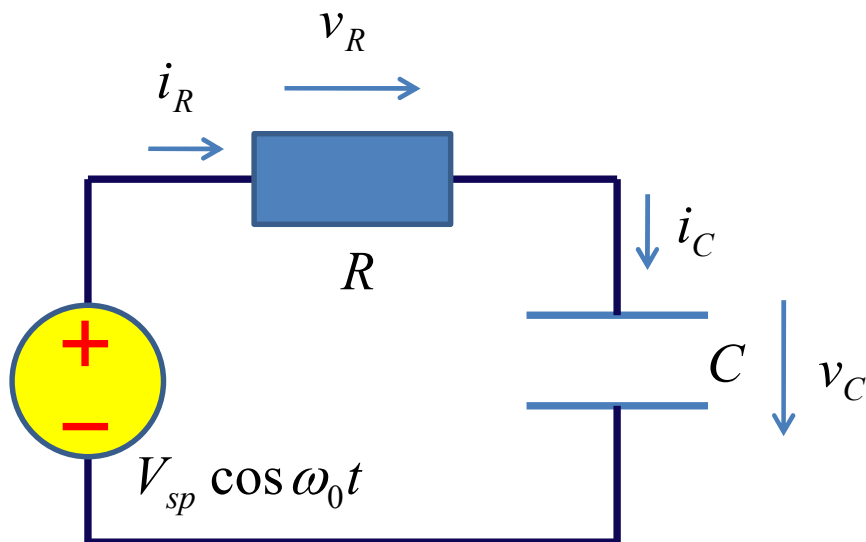
作业2 串联RC



- 对于图示RC串联电路

- (练习8.3.8) 在单端口加载正弦波激励电压源，测得电阻上正弦波电压幅度为**3V**，电容上正弦波电压幅度为**4V**，问激励电压源正弦波电压幅度为多少？保持正弦激励电压源幅度不变，但频率增加为原来频率的**2**倍，此时测得电阻上电压幅度为多少？电容上的电压幅度为多少？
- (练习8.3.9) 在单端口加载正弦波电压 $v_s(t) = V_{sp} \cos \omega t$ ，电容上分压为多少？电阻上分压为多少？是否满足两个分压之和等于总电压（**KVL**方程）？在频域分析中如何理解两个分压之和等于总电压（**KVL**方程）？

RC串联



在单端口加载正弦波激励电压源，测得电阻上正弦波电压幅度为**3V**，电容上正弦波电压幅度为**4V**，问激励电压源正弦波电压幅度为多少？保持正弦激励电压源幅度不变，但频率增加为原来频率的**2**倍，此时测得电阻上电压幅度为多少？电容上的电压幅度为多少？

$$v_S = V_{sp} \cos(\omega_0 t)$$

$$v_R = 3 \cos(\omega_0 t + \varphi_R)$$

$$V_{sp} = ?$$

$$v_C = 4 \cos(\omega_0 t + \varphi_C)$$

$$\dot{I} = I_p \angle \varphi_I$$

$$i_C = i_R = I_p \cos(\omega_0 t + \varphi_I)$$

$$\dot{V}_R = R \dot{I}$$

$$V_{Rp} = 3 = I_p R$$

$$\varphi_R = \varphi_I$$

$$\dot{V}_C = \frac{\dot{I}}{j\omega C}$$

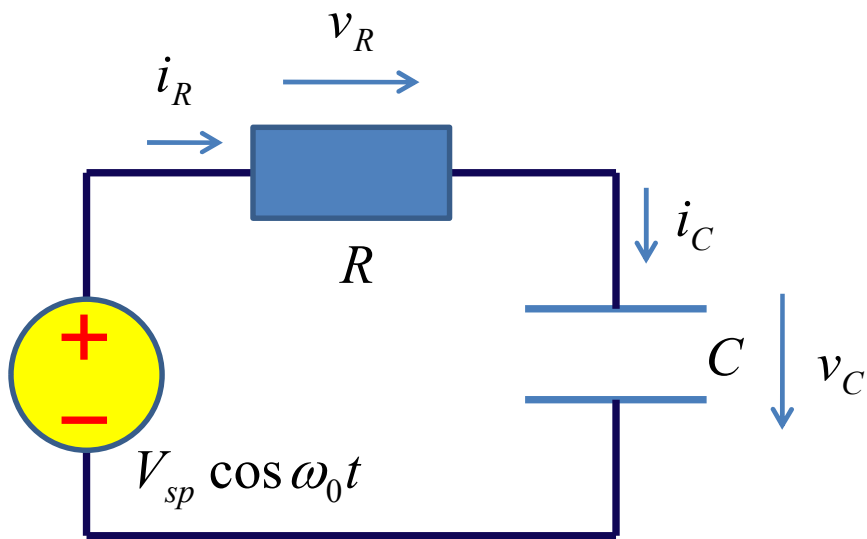
$$V_{Cp} = 4 = \frac{I_p}{\omega_0 C}$$

$$= \frac{I_p}{\omega C} \angle (\varphi_I - 90^\circ)$$

$$\varphi_C = \varphi_I - 90^\circ$$

电阻压流同频同相

电容压流同频滞后90°



$$\dot{I} = I_p \angle \varphi_I$$

$$i_C = i_R = I_p \cos(\omega_0 t + \varphi_I)$$

$$\dot{V}_R = R\dot{I}$$

$$V_{Rp} = 3 = I_p R$$

$$\varphi_R = \varphi_I$$

$$\dot{V}_C = \frac{\dot{I}}{j\omega C}$$

$$V_{Cp} = 4 = \frac{I_p}{\omega_0 C}$$

$$= \frac{I_p}{\omega C} \angle (\varphi_I - 90^\circ)$$

$$\varphi_C = \varphi_I - 90^\circ$$

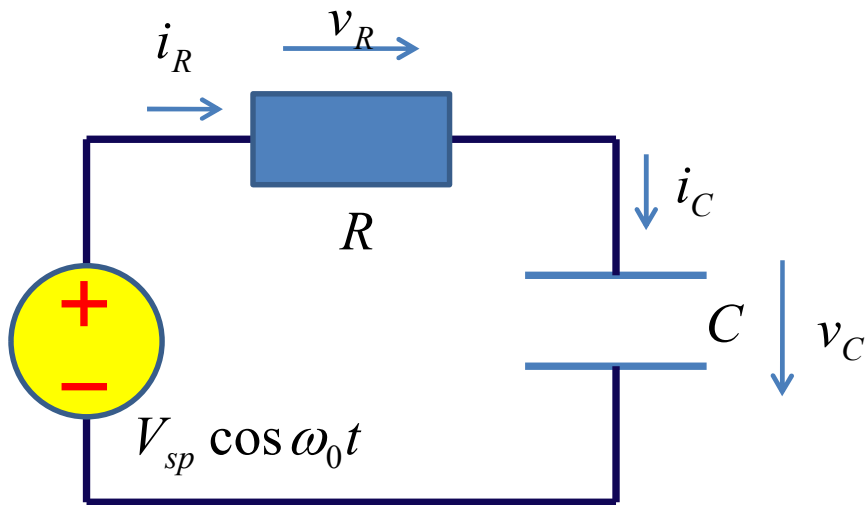
$$\dot{V}_S = \dot{V}_R + \dot{V}_C = \dot{I} \left(R + \frac{1}{j\omega_0 C} \right) = \dot{I} \sqrt{R^2 + \left(\frac{1}{\omega_0 C} \right)^2} \angle -\arctan \frac{1}{\omega_0 RC}$$

$$= I_p \sqrt{R^2 + \left(\frac{1}{\omega_0 C} \right)^2} \angle \left(\varphi_I - \arctan \frac{1}{\omega_0 RC} \right) = \sqrt{(I_p R)^2 + \left(\frac{I_p}{\omega_0 C} \right)^2} \angle \left(\varphi_I - \arctan \frac{1}{\omega_0 RC} \right)$$

$$= \sqrt{3^2 + 4^2} \angle \left(\varphi_I - \arctan \frac{1}{\omega_0 RC} \right) = 5 \angle \left(\varphi_I - \arctan \frac{1}{\omega_0 RC} \right)$$

$$V_{sp} = 5 = \sqrt{V_{Rp}^2 + V_{Cp}^2} = \sqrt{3^2 + 4^2}$$

相位差 90° ，组成直角三角形



在单端口加载正弦波激励电压源，测得电阻上正弦波电压幅度为**3V**，电容上正弦波电压幅度为**4V**，问激励电压源正弦波电压幅度为多少？保持正弦激励电压源幅度不变，但**频率增加为原来频率的2倍**，此时测得电阻上电压幅度为多少？电容上的电压幅度为多少？

$$\dot{V}_S = \dot{V}_R + \dot{V}_C = \dot{I} \left(R + \frac{1}{j\omega_0 C} \right)$$

$$= \sqrt{3^2 + 4^2} \angle \dots = 5 \angle \dots$$

$$\dot{V}_S = \dot{V}_R + \dot{V}_C = \dot{I}_2 \left(R + \frac{1}{j2\omega_0 C} \right)$$

$$= 5 \angle \dots = \sqrt{V_{Rp2}^2 + V_{Cp2}^2} \angle \dots$$

$$\frac{V_{Rp1}}{V_{Cp1}} = \frac{3}{4} = \frac{I_{p1} R}{I_{p1} / \omega_0 C} = \omega_0 RC$$

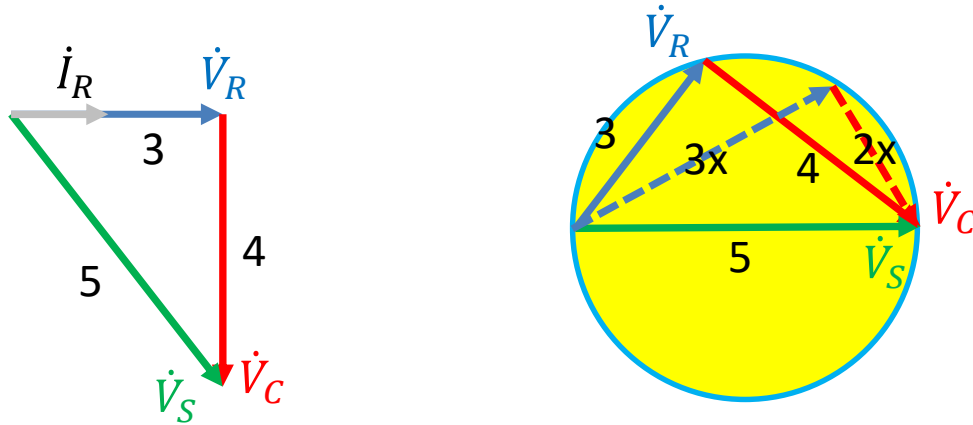
$$\frac{V_{Rp2}}{V_{Cp2}} = \frac{I_{p2} R}{I_{p2} / 2\omega_0 C} = 2\omega_0 RC = 1.5$$

$$5 = \sqrt{V_{Rp2}^2 + V_{Cp2}^2} = V_{Cp2} \sqrt{1.5^2 + 1^2} = 1.8 V_{Cp2}$$

$$V_{Cp2} = 5 / 1.8 = 2.77(V) \quad \leftarrow 4V$$

$$V_{Rp2} = 1.5 \times V_{Cp2} = 4.16(V) \quad \leftarrow 3V$$

相量图解法



$$\frac{|\dot{V}_R|}{|\dot{V}_C|} = \frac{R}{\frac{1}{2\omega_0 C}} = \frac{3}{2} = \frac{3x}{2x}$$

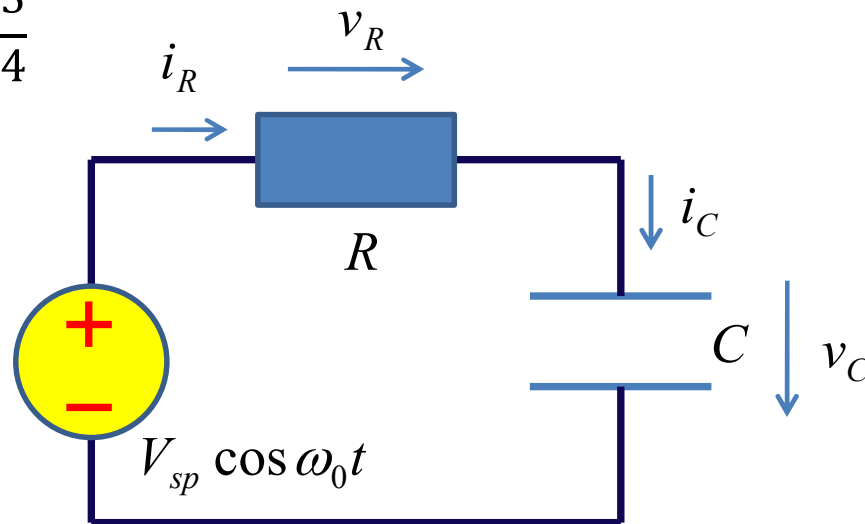
$$5 = |\dot{V}_S| = \sqrt{|\dot{V}_R|^2 + |\dot{V}_C|^2} \\ = \sqrt{(3x)^2 + (2x)^2} = \sqrt{13}x$$

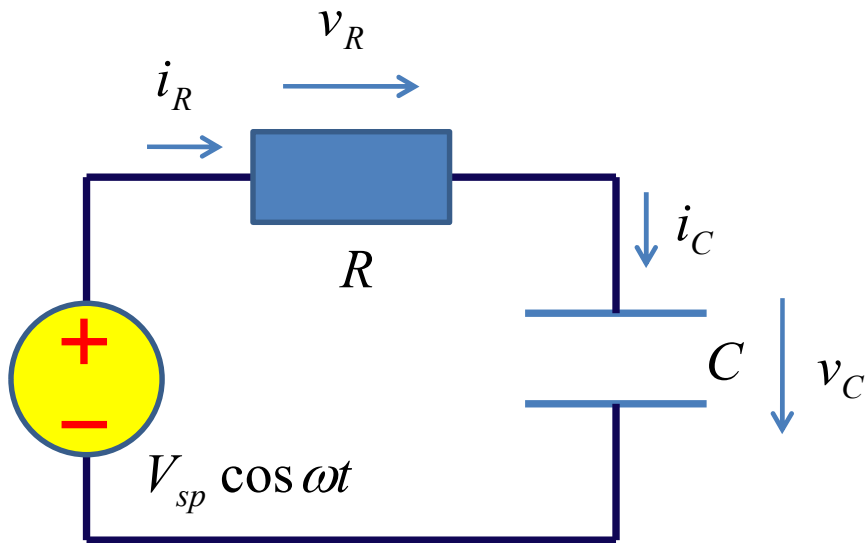
$$x = \frac{5}{\sqrt{13}}$$

$$|\dot{V}_R| = 3x = \frac{15}{\sqrt{13}} = 4.16V$$

$$|\dot{V}_C| = 2x = \frac{10}{\sqrt{13}} = 2.77V$$

$$\frac{|\dot{V}_R|}{|\dot{V}_C|} = \frac{R}{\frac{1}{\omega_0 C}} = \frac{3}{4}$$





在单端口加载正弦波电压 $v_s(t) = V_{sp} \cos \omega t$, 电容上分压为多少? 电阻上分压为多少? 是否满足两个分压之和等于总电压 (KVL 方程)? 在频域分析中如何理解两个分压之和等于总电压 (KVL 方程)?

$$\dot{I} = \frac{\dot{V}_S}{R + \frac{1}{j\omega C}}$$

$$\dot{V}_R = \dot{I}R = \frac{R}{R + \frac{1}{j\omega C}} \dot{V}_S = \frac{j\omega RC}{1 + j\omega RC} \dot{V}_S$$

$$= \frac{\omega RC}{\sqrt{1 + (\omega RC)^2}} \angle \left(\frac{\pi}{2} - \arctan \omega RC \right) \dot{V}_S$$

$$v_R(t) = V_{sp} \frac{\omega RC}{\sqrt{1 + (\omega RC)^2}} \cos \left(\omega t + \frac{\pi}{2} - \arctan \omega RC \right)$$

$$v_C(t) = V_{sp} \frac{1}{\sqrt{1 + (\omega RC)^2}} \cos(\omega t - \arctan \omega RC)$$

KVL方程在时域和频域均满足

频域表述更简单一些

$$\dot{V}_R = iR = \frac{R}{R + \frac{1}{j\omega C}} \dot{V}_S = \frac{j\omega RC}{1 + j\omega RC} \dot{V}_S \quad v_R(t) = V_{sp} \frac{\omega RC}{\sqrt{1 + (\omega RC)^2}} \cos\left(\omega t + \frac{\pi}{2} - \arctan \omega RC\right)$$

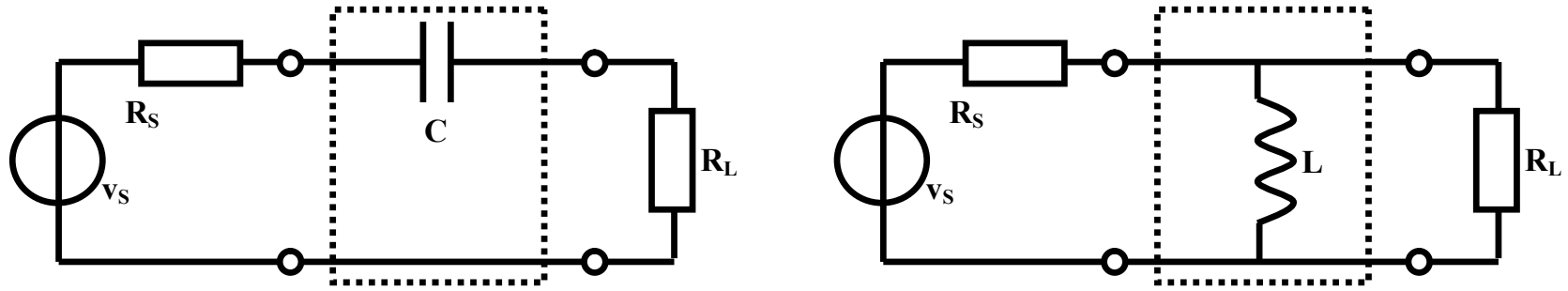
$$\dot{V}_C = i \frac{1}{j\omega C} = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} \dot{V}_S = \frac{1}{1 + j\omega RC} \dot{V}_S \quad v_C(t) = V_{sp} \frac{1}{\sqrt{1 + (\omega RC)^2}} \cos(\omega t - \arctan \omega RC)$$

$$\dot{V}_R + \dot{V}_C = \dot{V}_S$$

记住：相量域电量是复数，不能只考察幅度，还必须考虑相位影响
 $\mathbf{V}_{sp} \neq \mathbf{V}_{Rp} + \mathbf{V}_{Cp}$ ：矢量叠加，平行四边形法则运算

$$\begin{aligned} v_R(t) + v_C(t) &= -V_{sp} \frac{\omega RC}{\sqrt{1 + (\omega RC)^2}} \sin(\omega t - \arctan \omega RC) + V_{sp} \frac{1}{\sqrt{1 + (\omega RC)^2}} \cos(\omega t - \arctan \omega RC) \\ &= -V_{sp} \sin \varphi \sin(\omega t - \arctan \omega RC) + V_{sp} \cos \varphi \cos(\omega t - \arctan \omega RC) \\ &= V_{sp} \cos(\omega t - \arctan \omega RC + \varphi) = V_{sp} \cos \omega t = v_S(t) \end{aligned}$$

作业3 耦合电容和 高频扼流圈

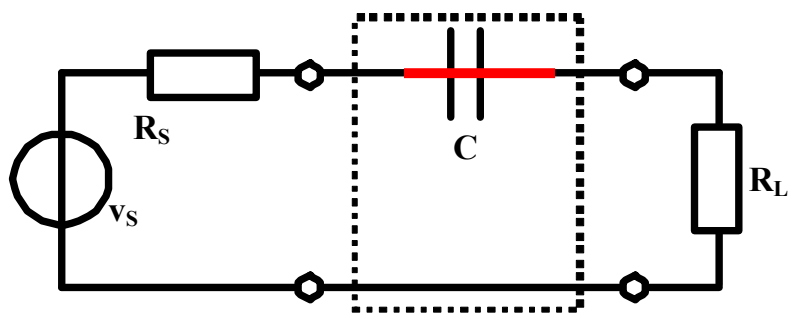


• (练习8.3.22)

- 如图**a**所示，这是一个用耦合电容耦合激励源和负载的简单电路模型。请分析确认：什么频率下可认为耦合电容是交流短路的？什么频率下可认为耦合电容是直流开路的？
- 如图**b**所示，这是一个高频扼流圈例子，一端接电源的高频扼流圈在此处被处理为接地。请分析确认：在什么频率下可认为高频扼流圈是直流短路的？什么频率下可认为高频扼流圈是交流开路的？

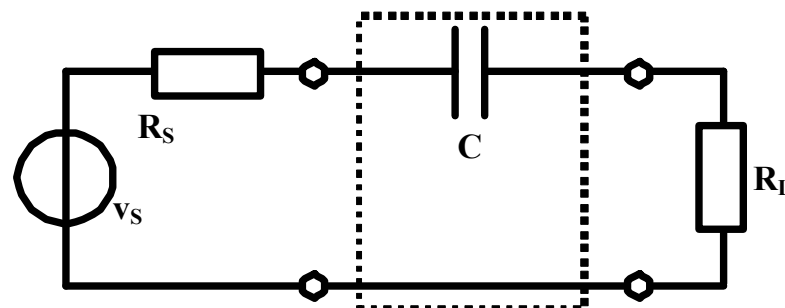
耦合电容

耦合电容高频短路，电路模型为



$$v_L = \frac{R_L}{R_S + R_L} v_S = \eta v_S$$

$$\omega_0 = \frac{1}{\tau} = \frac{1}{RC} = \frac{1}{(R_S + R_L)C}$$

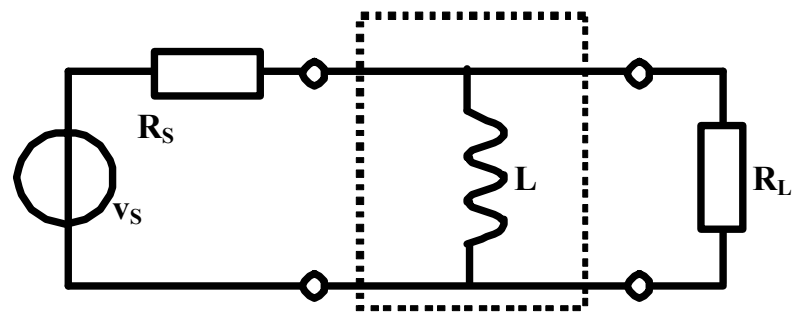


$$\begin{aligned} \dot{V}_L &= \frac{R_L}{R_S + \frac{1}{j\omega C} + R_L} \dot{V}_S \\ &= \frac{R_L}{R_S + R_L} \frac{1}{1 + \frac{1}{j\omega C(R_S + R_L)}} \dot{V}_S \\ &= \eta \frac{1}{1 + \frac{1}{j\omega\tau}} \dot{V}_S = \eta \frac{1}{1 + \frac{\omega_0}{j\omega}} \dot{V}_S \end{aligned}$$

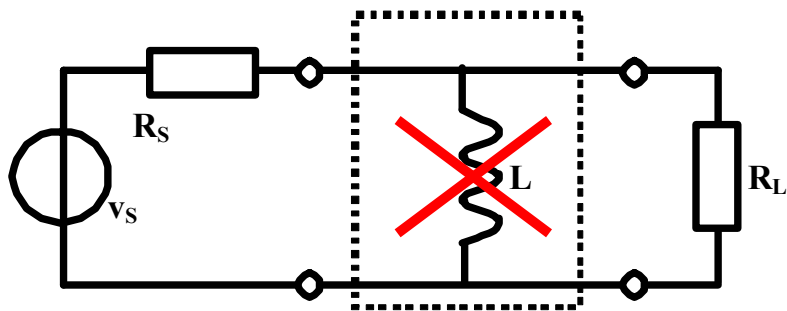
$$\begin{aligned} \omega \gg \omega_0 \\ \approx \eta \dot{V}_S \end{aligned}$$

负载电压是输入电压的高频分量
 $\omega \gg \omega_0$ 时，耦合电容视为高频短路 58

高频扼流圈



高频扼流圈高频开路，电路模型为



$$v_L = \frac{R_L}{R_S + R_L} v_S = \eta v_S$$

$$\omega_0 = \frac{1}{\tau} = \frac{1}{G_{SL}L} = \frac{R_S \parallel R_L}{L}$$

$$\begin{aligned} \dot{V}_L &= \frac{R_L \parallel j\omega L}{R_S + R_L \parallel j\omega L} \dot{V}_S = \frac{\frac{j\omega L R_L}{R_L + j\omega L}}{R_S + \frac{j\omega R_L L}{R_L + j\omega L}} \dot{V}_S \\ &= \frac{j\omega L R_L}{R_S(R_L + j\omega L) + j\omega L R_L} \dot{V}_S = \frac{j\omega L R_L}{R_S R_L + j\omega L(R_S + R_L)} \dot{V}_S \\ &= \frac{R_L}{R_S + R_L} \frac{j\omega L}{\frac{R_S R_L}{R_S + R_L} + j\omega L} \dot{V}_S = \frac{R_L}{R_S + R_L} \frac{j\omega L}{R_S \parallel R_L + j\omega L} \dot{V}_S \\ &= \frac{R_L}{R_S + R_L} \frac{j\omega G_{SL} L}{1 + j\omega G_{SL} L} \dot{V}_S = \eta \frac{1}{1 + \frac{\omega_0}{j\omega}} \dot{V}_S \stackrel{\omega \gg \omega_0}{\approx} \eta \dot{V}_S \end{aligned}$$

负载电压是输入电压的高频分量
 $\omega \gg \omega_0$ 时，高频扼流圈视为高频开路

高频? $\omega \gg \omega_0$

- $\omega > 10\omega_0$

$$\dot{V}_L = \eta \frac{1}{1 + \frac{\omega_0}{j\omega}} \dot{V}_S$$

$$\dot{V}_L = \eta \frac{1}{1 + \frac{\omega_0}{j10\omega_0}} \dot{V}_S = \eta \frac{1}{1 - j0.1} \dot{V}_S$$

$$= \eta \frac{e^{j5.7^\circ}}{1.005} \dot{V}_S = \eta \cdot 0.995 \cdot e^{j5.7^\circ} \cdot \dot{V}_S$$

$$v_S = V_{sp} \cos(\omega_0 t)$$

$$v_L = \eta V_{sp} \cos(\omega_0 t)$$

耦合电容**短路**，
高频扼流圈**开路**

0.5%误差

3.2%误差



$$v_L = 0.995\eta V_{sp} \cos(\omega_0 t + 5.7^\circ)$$

足够接近耦合电容**短路**，
高频扼流圈**开路**

低频? $\omega \ll \omega_0$

- $\omega < 0.1\omega_0$

$$\dot{V}_L = \eta \frac{1}{1 + \frac{\omega_0}{j\omega}} \dot{V}_S$$

$$\dot{V}_L = \eta \frac{1}{1 + \frac{\omega_0}{j0.1\omega_0}} \dot{V}_S = \eta \frac{1}{1 - j10} \dot{V}_S$$

$$= \eta \frac{e^{j84.3^\circ}}{10.05} \dot{V}_S = \eta \cdot 0.0995 \cdot e^{j84.3^\circ} \cdot \dot{V}_S$$

$$v_S = V_{sp} \cos(\omega_0 t)$$

$$v_L = 0$$

耦合电容**开路**，
高频扼流圈**短路**

1%的功率泄漏是否可忽略不计?



$$v_L = 0.1\eta V_{sp} \cos(\omega_0 t + 90^\circ - 5.7^\circ)$$

足够接近耦合电容直流开
路，高频扼流圈直流短路

如何直接写出 一阶系统系统传函表达式

- 先判断低通高通

如果不是简单的低通和高通，则老老实实地在相量域求解方程获得传递函数

$$H_{\text{LP}}(j\omega) = H_0 \frac{1}{1 + j\omega\tau}$$

$$H_{\text{HP}}(j\omega) = H_0 \frac{j\omega\tau}{1 + j\omega\tau}$$

- 求 H_0 : 中心频点的传递系数

$$H_0 = H_{\text{LP}}(j0)_{\text{电容开路, 电感短路}}$$

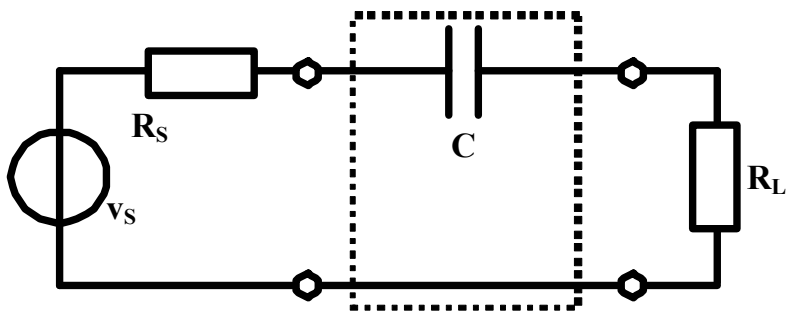
$$H_0 = H_{\text{HP}}(j\infty)_{\text{电容短路, 电感开路}}$$

- 求 τ : 一阶系统的时间常数

$$\tau = RC$$

$$\tau = GL = \frac{L}{R}$$

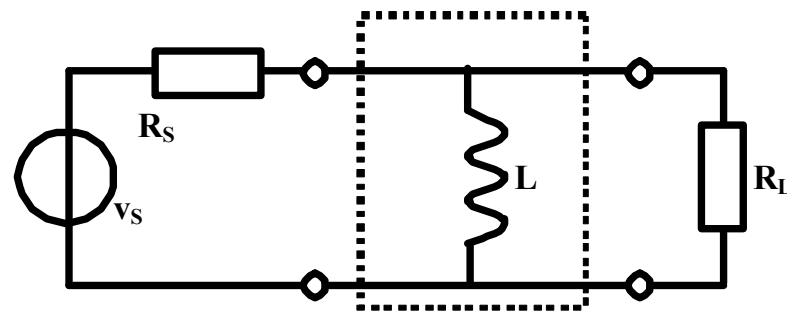
R 是 C 或 L 两端看入的等效电阻



$$H_{\text{HP}}(j\omega) = H_0 \frac{j\omega\tau}{1 + j\omega\tau}$$

$$H_0 = \frac{R_L}{R_S + R_L}$$

$$\tau = (R_S + R_L)C$$



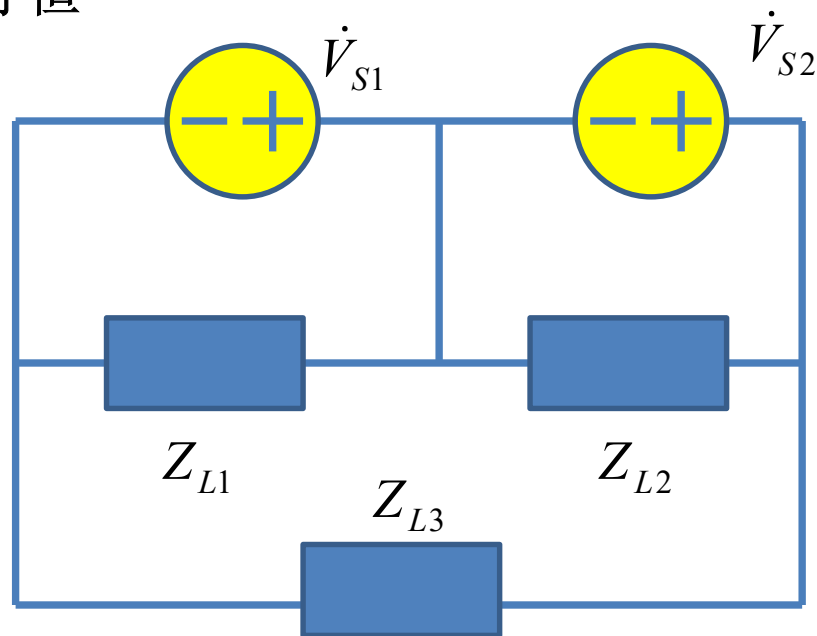
$$H_{\text{HP}}(j\omega) = H_0 \frac{j\omega\tau}{1 + j\omega\tau}$$

$$H_0 = \frac{R_L}{R_S + R_L}$$

$$\tau = (G_S + G_L)L$$

作业4：复功率

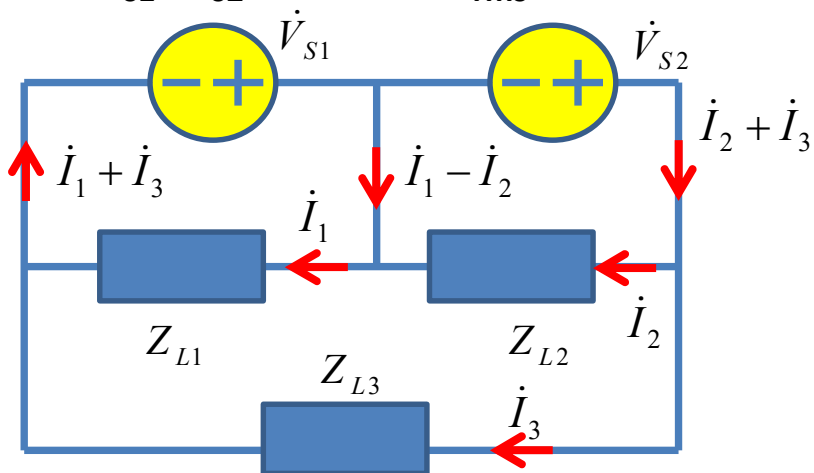
- **(练习8.3.5)** 如图所示电路中有两个电压源和三个负载，负载1吸收的功率为1.8kW和600var，负载2吸收功率为1.5kVA，功率因数0.8超前（电流超前电压），负载3为 $(12\Omega) \parallel (j48\Omega)$
 - 如果 $\dot{V}_{s1} = \dot{V}_{s2} = 120\angle 0^\circ \text{V}_{\text{rms}}$ ，求两个电源发送的平均功率和无功率
 - 确认复功率守恒



- 负载1吸收功率为1.8kW和600var，负载2吸收功率为1.5kVA，功率因数0.8超前（电流超前电压），负载3为 $(12\Omega) \parallel (j48\Omega)$ ，

$$V_{s1} = V_{s2} = 120 \angle 0^\circ V_{rms}$$

回路电流法



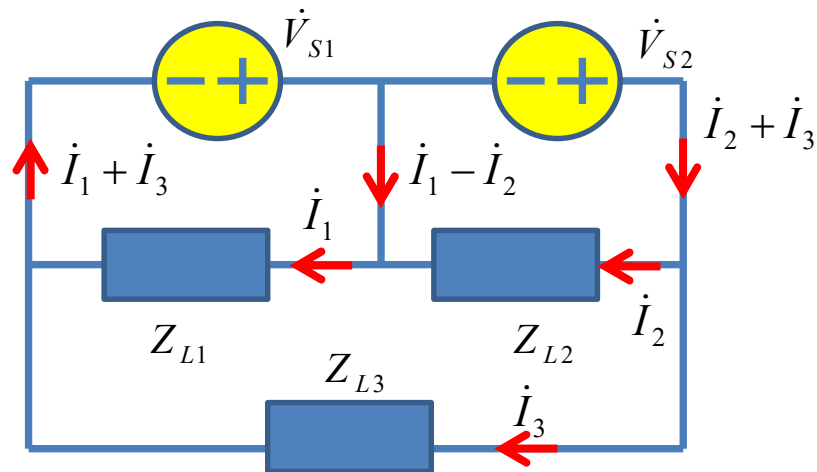
$$\dot{I}_{1,rms}^* = \frac{S_1}{\dot{V}_{1,rms}} = \frac{1800 + j600}{120} = 15 + j5 (A_{rms})$$

$$\begin{aligned} \dot{I}_{2,rms}^* &= \frac{S_2}{\dot{V}_{2,rms}} = \frac{|S_2| \angle (\varphi_{V2} - \varphi_{I2})}{|V_{2,rms}| \angle \varphi_2} = \frac{1500 \angle \arctan \frac{-0.6}{0.8}}{120 \angle 0} \\ &= \frac{1500 \times 0.8 - j1500 \times 0.6}{120} = \frac{1200 - j900}{120} = 10 - j7.5 (A_{rms}) \end{aligned}$$

$$\dot{I}_{3,rms} = \frac{\dot{V}_{1,rms} + \dot{V}_{2,rms}}{Z_{L3}} = \frac{240}{12 \parallel j48} = \frac{240}{\frac{12 \times j48}{12 + j48}} = \frac{240(12 + j48)}{12 \times j48} = \frac{5(1 + j4)}{j} = 20 - j5 (A_{rms})$$

$$S_3 = \dot{V}_{3,rms} \dot{I}_{3,rms}^* = (240) \times (20 + j5) = 4800 + j1200$$

$$\begin{aligned} S_L &= S_1 + S_2 + S_3 = (1800 + j600) + (1200 - j900) + (4800 + j1200) \\ &= 7800W + j900 \text{ var} \end{aligned}$$



$$\dot{I}_{1,rms} = 15 - j5(A_{rms}) \quad \dot{I}_{1,rms}^* = 15 + j5(A_{rms})$$

$$\dot{I}_{2,rms} = 10 + j7.5(A_{rms}) \quad \dot{I}_{2,rms}^* = 10 - j7.5(A_{rms})$$

$$\dot{I}_{3,rms} = 20 - j5(A_{rms})$$

$$S_{S1} = V_1(\dot{I}_{1,rms} + \dot{I}_{3,rms})^* = 120 \times (15 - j5 + 20 - j5)^* = 120 \times (35 + j10) = 4200 + j1200$$

$$S_{S2} = V_2(\dot{I}_{2,rms} + \dot{I}_{3,rms})^* = 120 \times (10 + j7.5 + 20 - j5)^* = 120 \times (30 - j2.5) = 3600 - j300$$

$$P_{S1} = 4200W$$

$$P_{S2} = 3600W$$

$$P_S = P_{S1} + P_{S2} = 7800W$$

$$Q_{S1} = 1200 \text{ var}$$

$$Q_{S1} = -300 \text{ var}$$

$$Q_S = Q_{S1} + Q_{S2} = 900 \text{ var}$$

复功 $S_{S1} + S_{S2} = S_S = S_L = S_1 + S_2 + S_3$

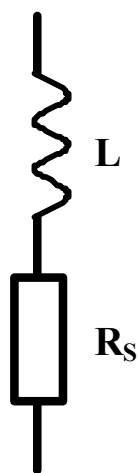
实功 $P_{S1} + P_{S2} = P_S = P_L = P_1 + P_2 + P_3$

能量守恒

虚功 $Q_{S1} + Q_{S2} = Q_S = Q_L = Q_1 + Q_2 + Q_3$

作业5、6：电桥

- 5、（习题8.4，8.5）用电桥测电感



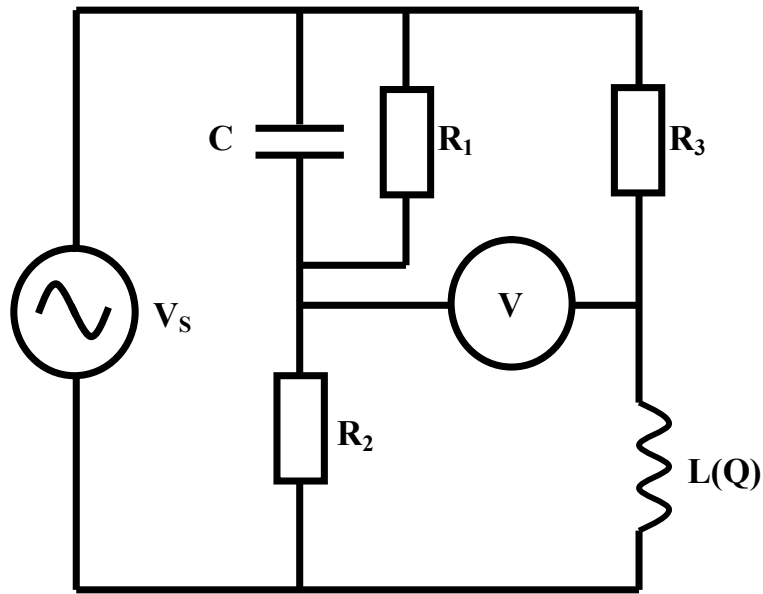
$$Q = \frac{\omega L}{R_s}$$

$$\text{品质因数} = \frac{|\text{虚功}|}{|\text{实功}|} = \begin{cases} \frac{|\text{串联电抗}|}{|\text{串联电阻}|} \\ \frac{|\text{并联电纳}|}{|\text{并联电导}|} \end{cases}$$

$$Z_L = R_s + j\omega L$$

真实电感存在寄生效应，这里假设频率较低，只考虑寄生电阻效应

Maxwell Bridge



$$Z_1 Z_4 = Z_2 Z_3$$

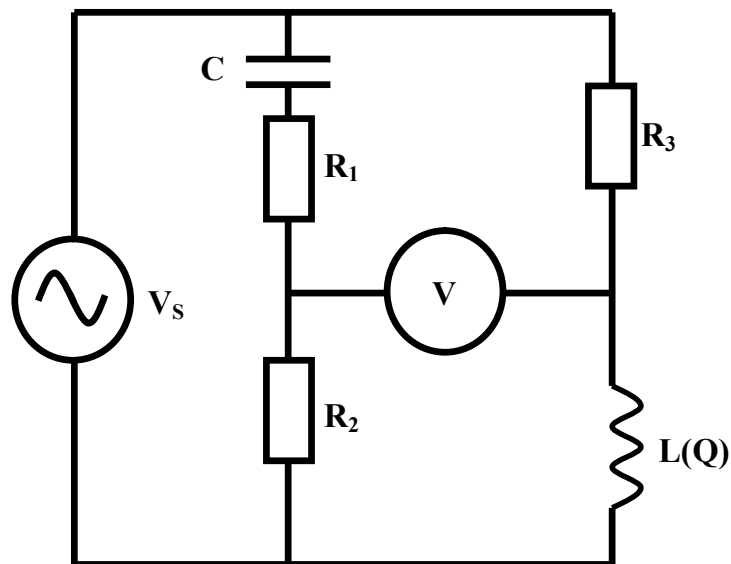
$$Z_4 = \frac{Z_2 Z_3}{Z_1} = \frac{R_2 R_3}{\frac{R_1}{1 + j\omega_0 R_1 C}} = \frac{R_2 R_3}{R_1} (1 + j\omega_0 R_1 C)$$

$$= \frac{R_2 R_3}{R_1} + j\omega_0 R_2 R_3 C = R_S + j\omega_0 L$$

$$L = R_2 R_3 C$$

$$Q = \frac{\omega_0 L}{R_S} = \frac{\omega_0 R_2 R_3 C}{\frac{R_2 R_3}{R_1}} = \omega_0 R_1 C = Q_1 = \frac{\omega_0 C}{G_1} = \frac{|\text{并联电纳}|}{\text{并联电导}}$$

Hay's Bridge



$$Z_1 Z_4 = Z_2 Z_3$$

$$Z_4 = \frac{Z_2 Z_3}{Z_1} = \frac{R_2 R_3}{R_1 + \frac{1}{j\omega_0 C}} = \frac{R_2 R_3}{R_1} \frac{j\omega_0 R_1 C}{1 + j\omega_0 R_1 C}$$

$$= \frac{R_2 R_3}{R_1} \frac{((\omega_0 R_1 C)^2 + j\omega_0 R_1 C)}{1 + (\omega_0 R_1 C)^2} = R_S + j\omega_0 L$$

$$Q = \frac{\omega_0 L}{R_S} = \frac{1}{\omega_0 R_1 C} = Q_1 = \frac{|\text{串联电抗}|}{\text{串联电阻}}$$

$$Q \gg 1$$

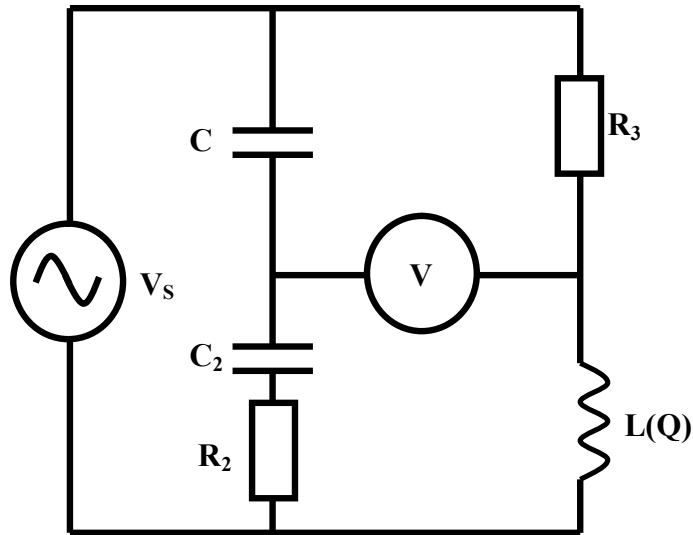
$$R_S = \frac{R_2 R_3}{R_1} \frac{(\omega_0 R_1 C)^2}{1 + (\omega_0 R_1 C)^2}$$

$$L = \frac{R_2 R_3}{R_1} \frac{R_1 C}{1 + (\omega_0 R_1 C)^2} = \frac{R_2 R_3 C}{1 + (\omega_0 R_1 C)^2}$$

$$L = \frac{R_2 R_3 C}{1 + (\omega_0 R_1 C)^2} \approx R_2 R_3 C$$

$$Z_1 Z_4 = Z_2 Z_3$$

Owen's Bridge



$$Z_4 = \frac{Z_2 Z_3}{Z_1} = \frac{\left(R_2 + \frac{1}{j\omega_0 C_2} \right) R_3}{\frac{1}{j\omega_0 C}} = \left(j\omega_0 R_2 C + \frac{C}{C_2} \right) R_3$$

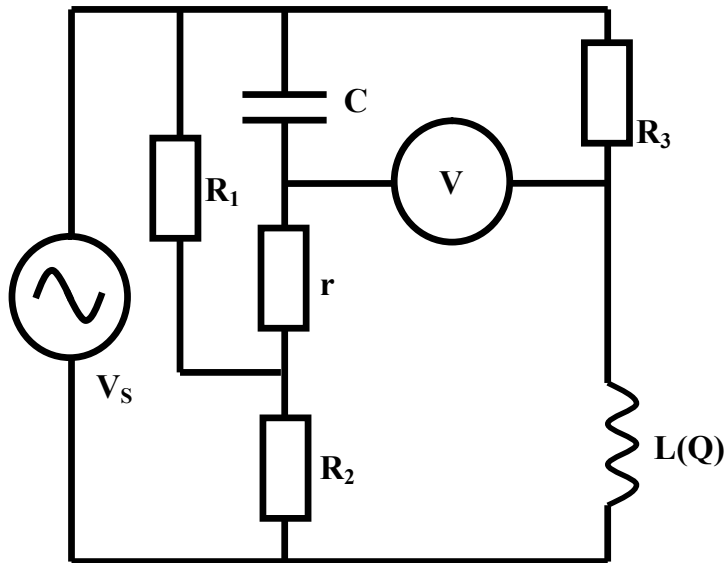
$$= \left(\frac{C}{C_2} R_3 + j\omega_0 R_3 R_2 C \right) = R_S + j\omega_0 L$$

$$R_S = \frac{C}{C_2} R_3$$

$$L = R_3 R_2 C$$

$$Q = \frac{\omega_0 L}{R_S} = \omega_0 R_2 C_2 = \frac{1}{Q_2} = \frac{1}{\frac{\text{串联电抗}}{\text{串联电阻}}}$$

Anderson's Bridge



$$\dot{V}_{d3} = \frac{R_3}{Z_4 + R_3} (-\dot{V}_s)$$

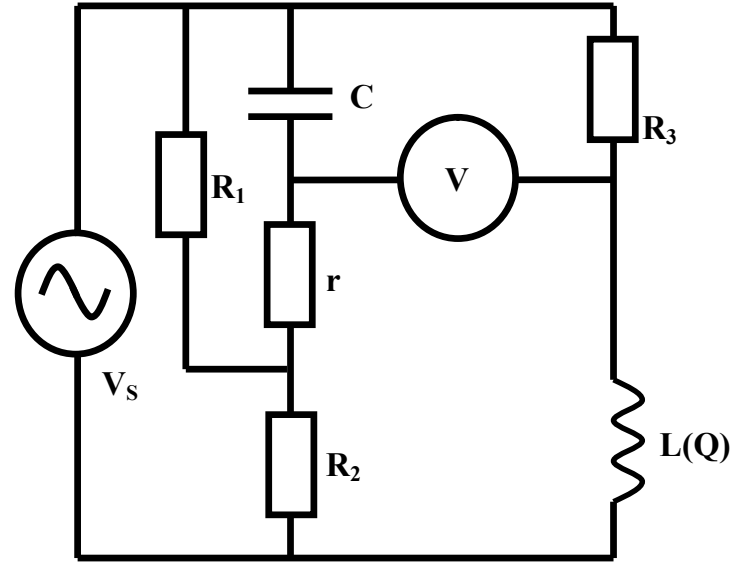
$$\dot{V}_{dC} = -\dot{V}_s \frac{R_1 \parallel \left(r + \frac{1}{j\omega_0 C} \right) \frac{1}{j\omega_0 C}}{R_2 + R_1 \parallel \left(r + \frac{1}{j\omega_0 C} \right) r + \frac{1}{j\omega_0 C}}$$

$$\dot{V}_{d3} = \dot{V}_{dC}$$

$$\frac{R_1 \parallel \left(r + \frac{1}{j\omega_0 C} \right) \frac{1}{j\omega_0 C}}{R_2 + R_1 \parallel \left(r + \frac{1}{j\omega_0 C} \right) r + \frac{1}{j\omega_0 C}} = \frac{R_3}{Z_4 + R_3}$$

$$\frac{R_1 \cdot \left(r + \frac{1}{j\omega_0 C} \right)}{R_1 + \left(r + \frac{1}{j\omega_0 C} \right)} \cdot \frac{1}{j\omega_0 C} = \frac{R_1}{R_2 R_1 + R_2 \left(r + \frac{1}{j\omega_0 C} \right)} \cdot \frac{1}{j\omega_0 C}$$

$$R_2 + \frac{R_1 \cdot \left(r + \frac{1}{j\omega_0 C} \right)}{R_1 + \left(r + \frac{1}{j\omega_0 C} \right)} \cdot \frac{1}{j\omega_0 C}$$



$$= \frac{R_1 \cdot \frac{1}{j\omega_0 C}}{\left(R_2 R_1 + R_2 r + R_1 r \right) + \left(R_2 + R_1 \right) \frac{1}{j\omega_0 C}} = \frac{R_3}{Z_4 + R_3}$$

$$= \frac{R_1}{\left(R_2 R_1 + R_2 r + R_1 r \right) j\omega_0 C + \left(R_2 + R_1 \right)} = \frac{R_3}{j\omega_0 L + R_S + R_3}$$

$$= \frac{1}{j\omega_0 \left(R_2 + \frac{R_2}{R_1} r + r \right) C + \frac{R_2}{R_1} + 1} = \frac{1}{j\omega_0 \frac{L}{R_3} + \frac{R_S}{R_3} + 1}$$

$$R_S = \frac{R_2}{R_1} R_3$$

$$L = R_3 \left(R_2 + \frac{R_2}{R_1} r + r \right) C$$

$$= R_3 R_2 C \left(1 + \frac{1}{R_1} r + \frac{1}{R_2} r \right)$$

$$= R_3 R_2 C \left(1 + \frac{r}{R_1 \parallel R_2} \right)$$