

电子电路与系统基础

习题课第十五讲

- 1、运算放大器复习
- 2、第十五讲作业讲解

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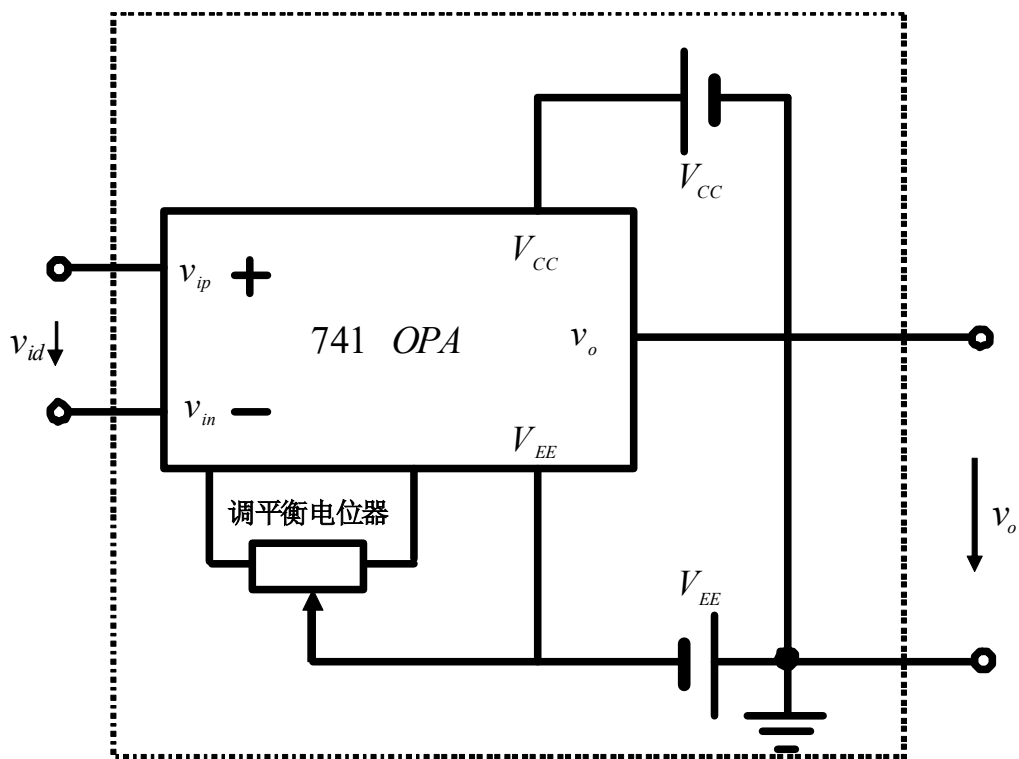
运算放大器复习

基本要求

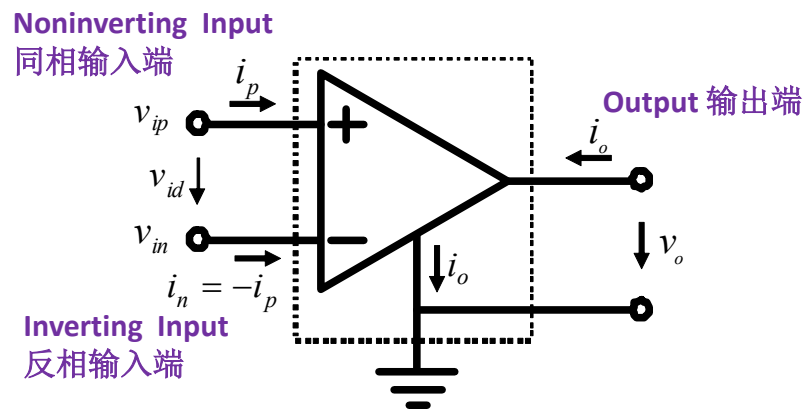
- 1、基本电路模型
- 2、虚短虚断应用
- 3、负反馈类型判定
- 4、正反馈分析

- 运放转移特性曲线
 - 具有明显的分区特性：三段折线等效电路模型
- 在运放转移特性曲线的放大区，运放等效为压控压源
 - 放大倍数抽象为无穷大
 - 虚短、虚断特性：熟练运用
 - 运放保持在放大区，绝大多数靠负反馈实现
 - 什么是负反馈，什么是正反馈？
- 运放转移特性曲线的饱和区，运放等效电路为恒压源
 - 负反馈运放电路
 - 如果输出幅度预算超过饱和电压则必进入饱和区
 - 正反馈运放电路
 - 大多进入饱和区，个别通过适当控制（形成负反馈效应）则可工作在线性区（等效为负阻）

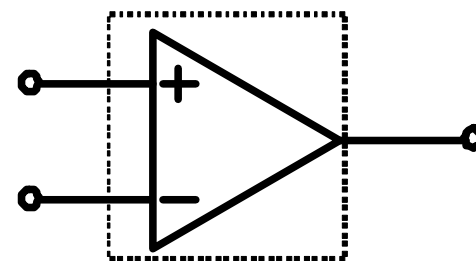
运放是高度抽象的二端口网络



(a) 实际运放外部连接关系



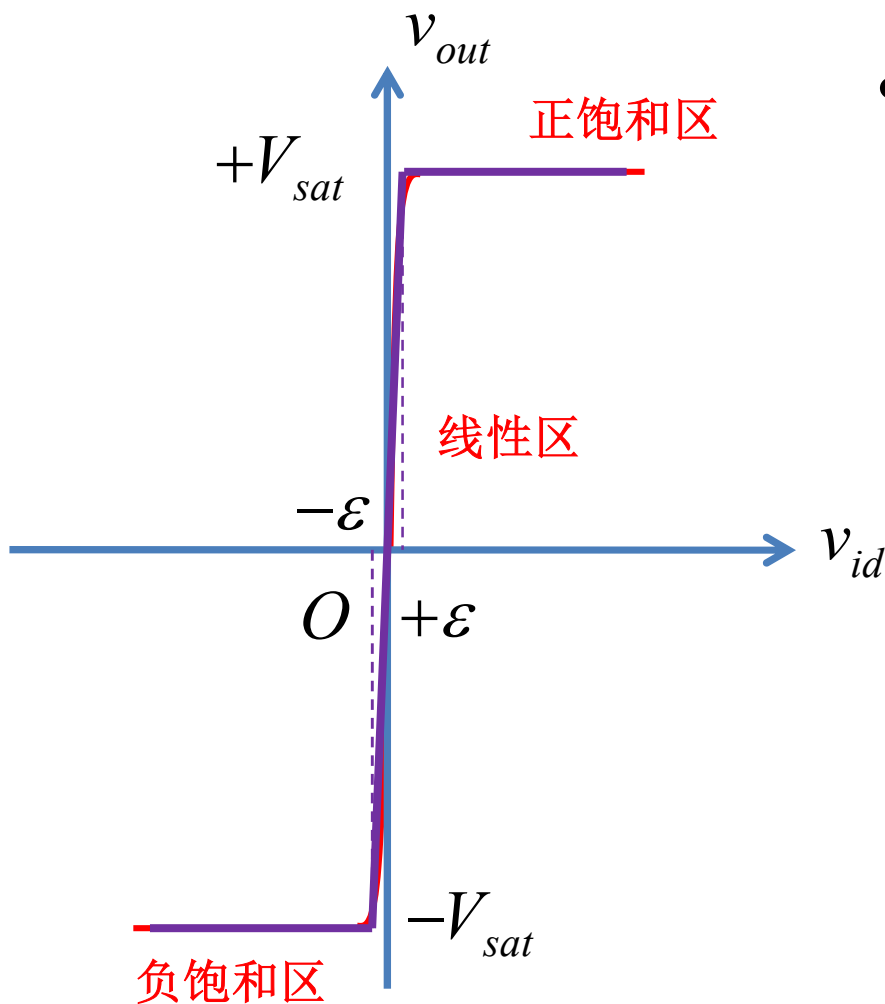
(b) 运放符号: (带地)



(c) 运放符号: (默认带地)

$$v_{out} = f(v_{id}) = f(v_{ip} - v_{in}) \stackrel{\text{线性放大区}}{\cong} A_{v0}(v_{ip} - v_{in})$$

三段折线模型

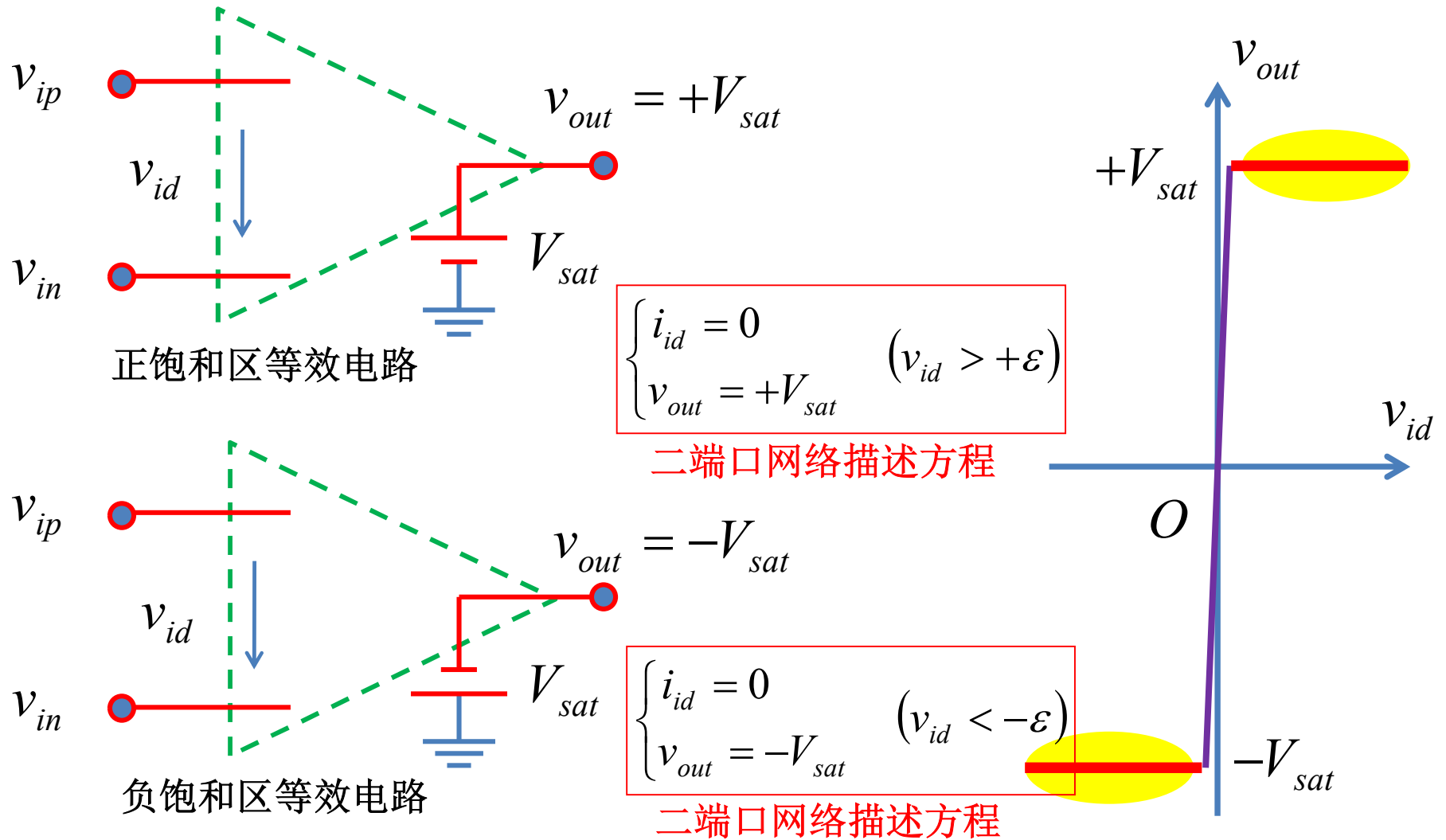


- 分段线性是对强非线性的常见处理手法
– 运放转移特性曲线

$$v_{out} = \begin{cases} -V_{sat} & v_{id} < -\epsilon \\ A_{v0}v_{id} & -\epsilon < v_{id} < +\epsilon \\ +V_{sat} & v_{id} > +\epsilon \end{cases}$$

$$\epsilon = \frac{V_{sat}}{A_{v0}} \quad \begin{matrix} A_{v0} \text{极大} \\ \epsilon \text{很小} \end{matrix}$$

饱和区恒压源模型

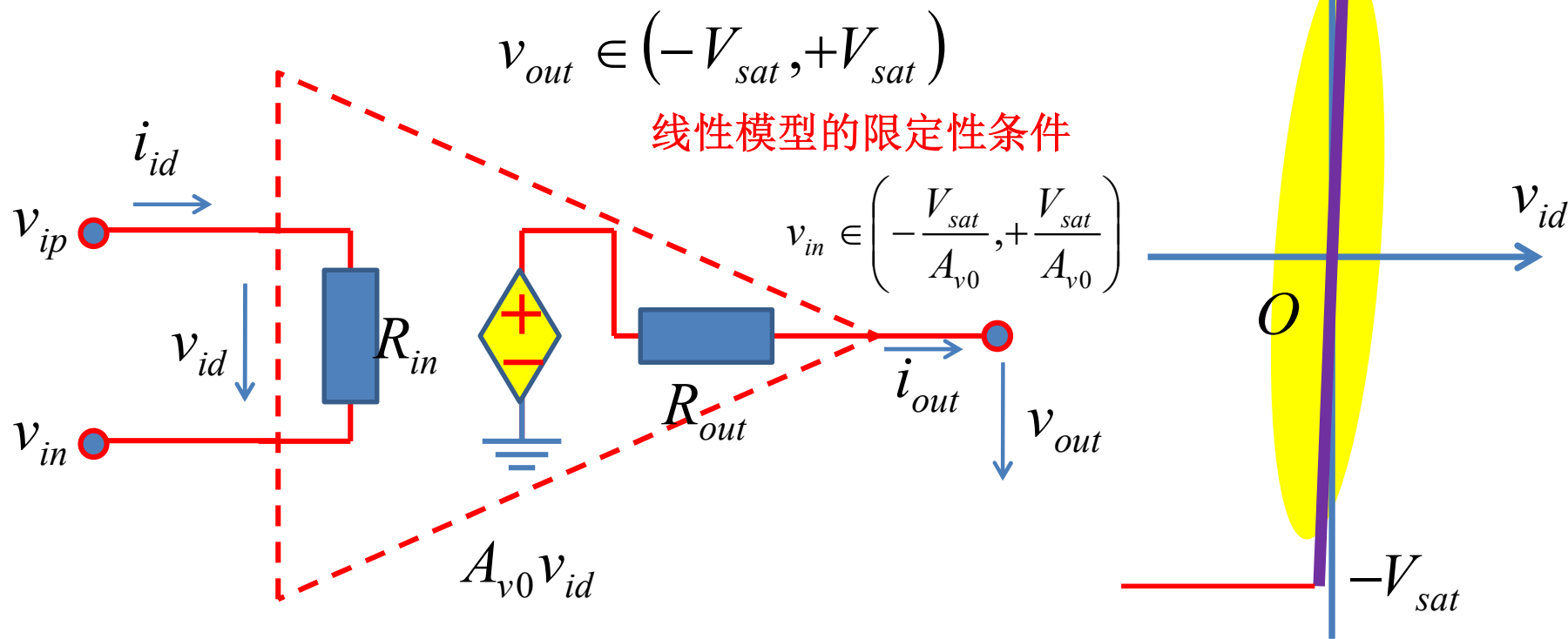


线性区 压控压源模型

$$\begin{cases} i_{id} = v_{id} / R_{in} \\ v_{out} = A_{v0} v_{id} - R_{out} i_{out} \end{cases}$$

二端口网络描述方程

- 既然是电压放大器，除了电压增益（传输特性）外，还有端口阻抗特性

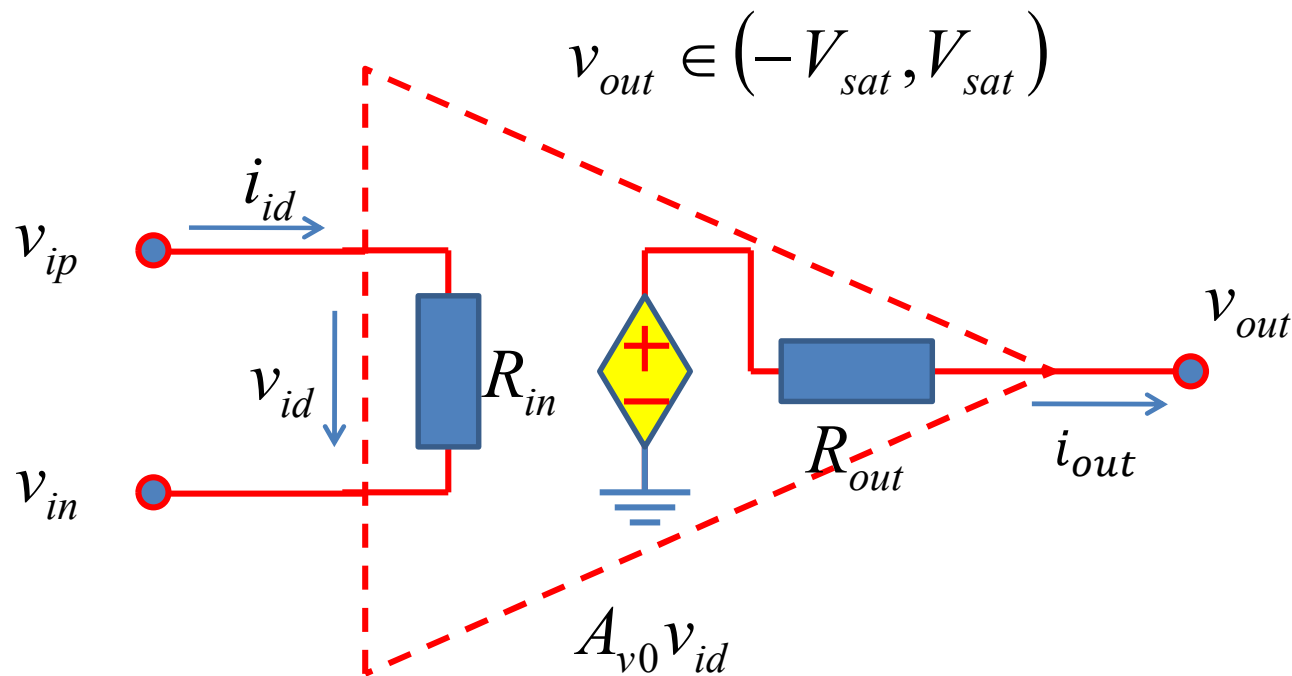


理想运放电路模型

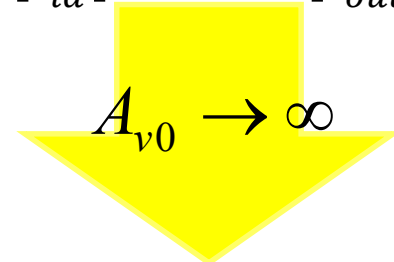
$$A_{v0} \rightarrow \infty$$

传输参量

$$ABCD = \begin{bmatrix} \frac{1}{A_{v0}} & \frac{R_{out}}{A_{v0}} \\ 1 & R_{out} \\ \frac{1}{A_{v0}R_{in}} & \frac{R_{out}}{A_{v0}R_{in}} \end{bmatrix}$$



$$\begin{bmatrix} v_{id} \\ i_{id} \end{bmatrix} = ABCD \begin{bmatrix} v_{out} \\ i_{out} \end{bmatrix}$$



$$A_{v0} \rightarrow \infty$$

$$\begin{cases} i_{id} = 0 \\ v_{id} = 0 \end{cases}$$

二端口网络描述方程
限定性条件:

$$\begin{cases} i_{out} \in (-I_{sc}, I_{sc}) \\ v_{out} \in (-V_{sat}, V_{sat}) \end{cases}$$

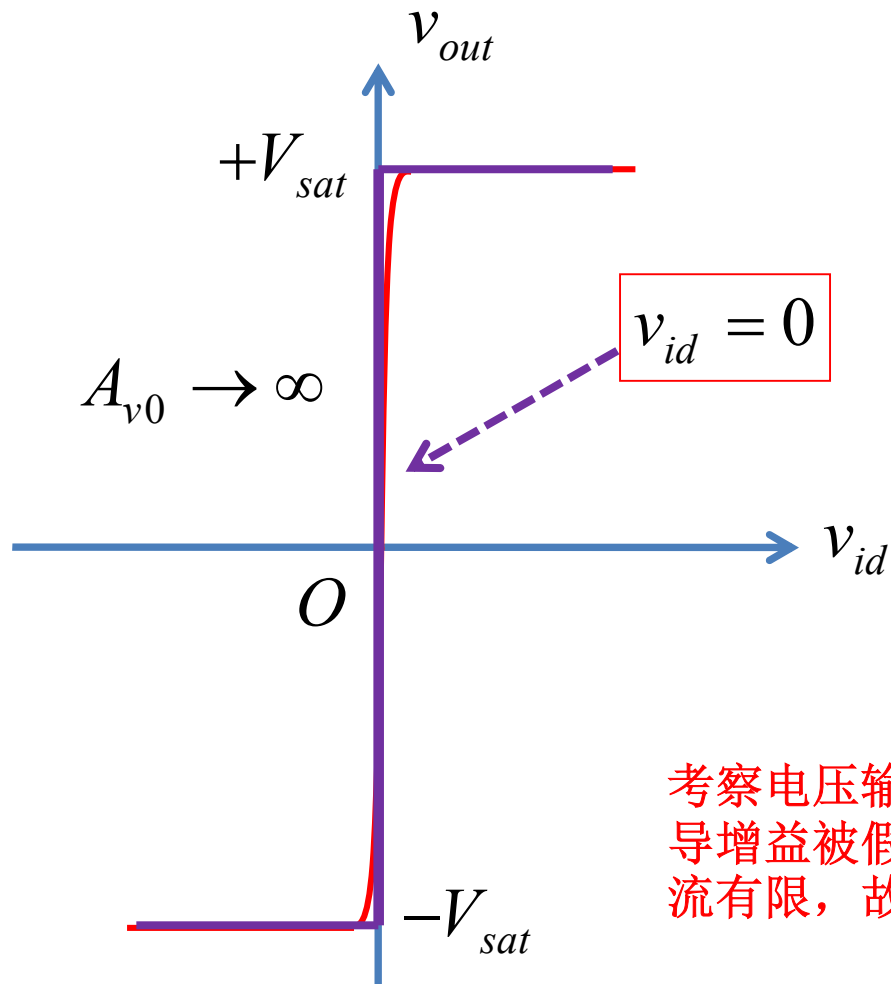
虚短 virtual short circuit

$$\begin{cases} i_{id} = 0 \\ v_{id} = 0 \end{cases}$$

理想运放二端口描述方程

$$-V_{sat} < v_{out} < +V_{sat}$$

$$v_{ip} = v_{in}$$



$$v_{out,open} = A_{v0}v_{id}$$

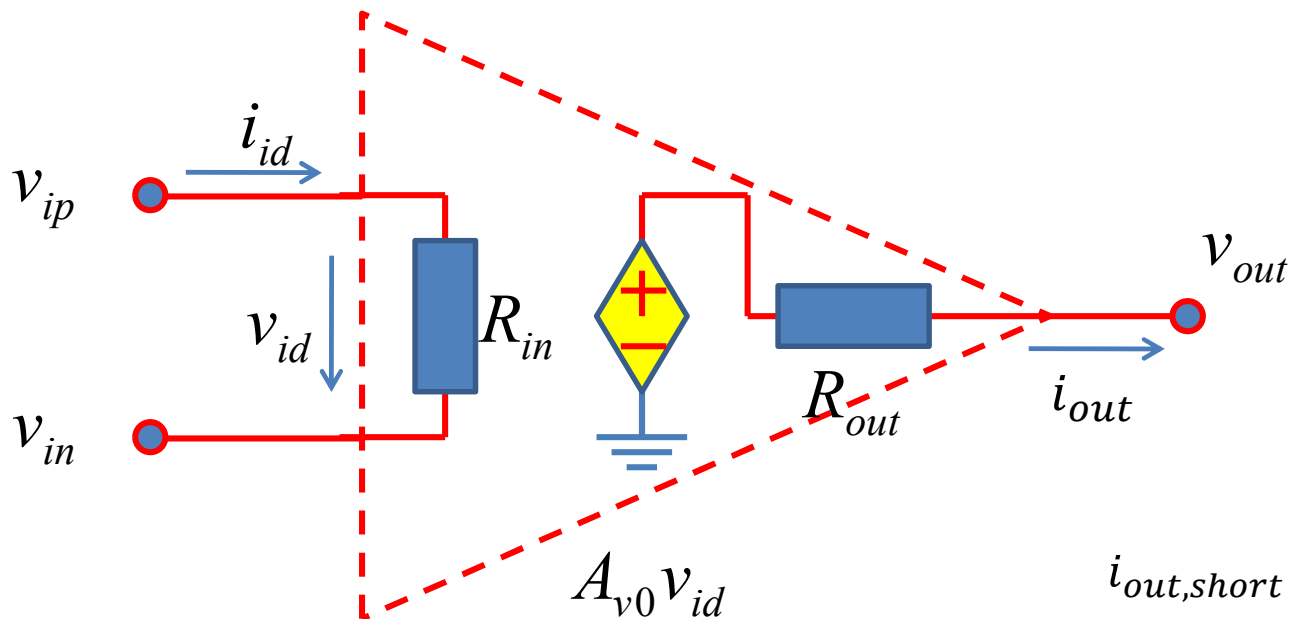
$$i_{out,short} = G_{m0}v_{id} = \frac{A_{v0}}{R_{out}}v_{id}$$

考察电压输入时，由于本征电压增益和本征跨导增益被假设为无穷大，而输出电压和输出电流有限，故而输入电压虚拟为0（虚短）

虚断 virtual open circuit

$$\begin{cases} i_{id} = 0 \\ v_{id} = 0 \end{cases}$$

理想运放二端口描述方程



$$\begin{cases} i_{out} \in (-I_{sc}, I_{sc}) \\ v_{out} \in (-V_{sat}, V_{sat}) \end{cases}$$

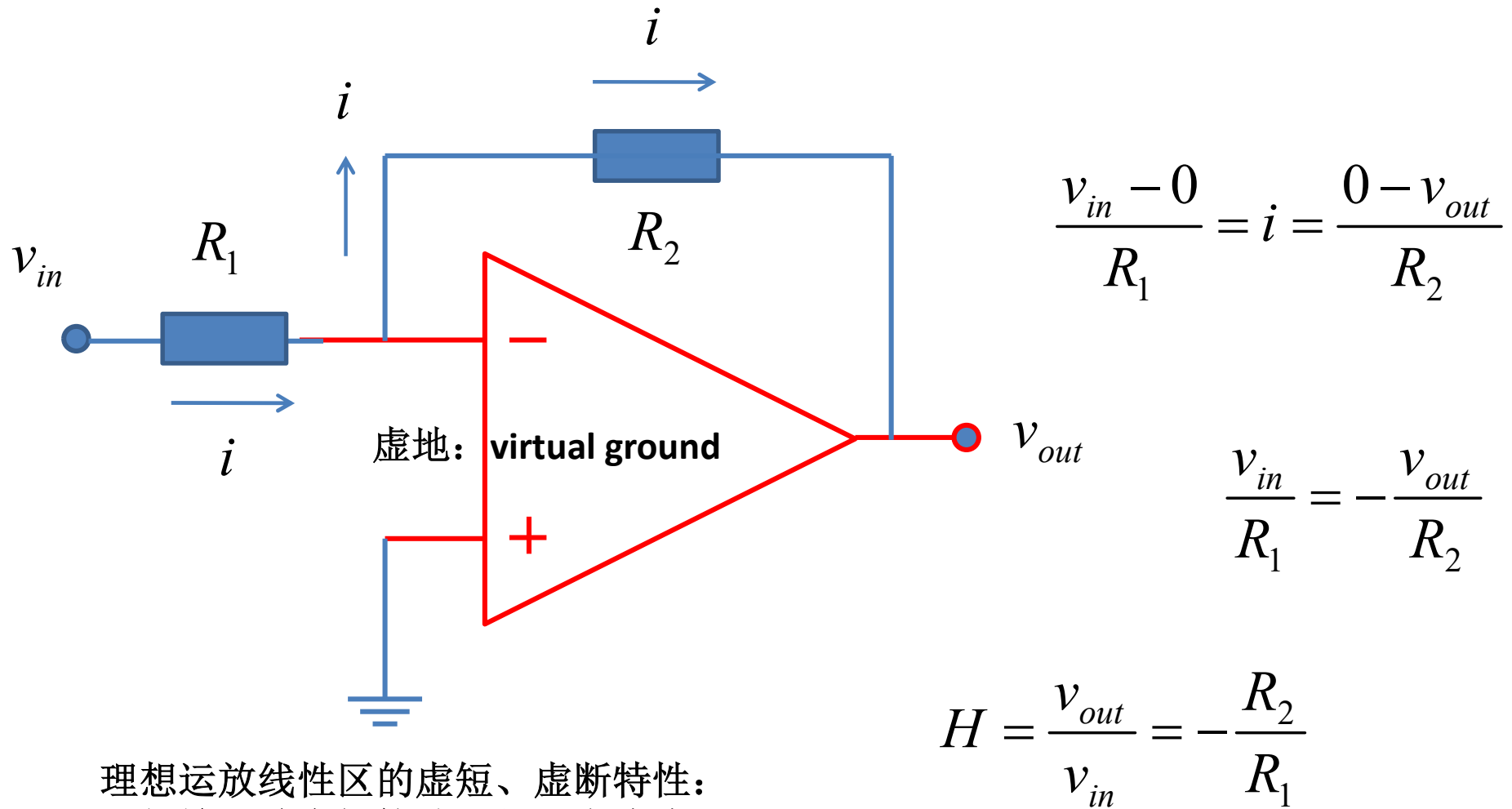
$$i_{out,short} = A_{i0} i_{id} = \frac{A_{v0} R_{in}}{R_{out}} i_{id}$$

$$v_{out,open} = R_{m0} i_{id} = A_{v0} R_{in} i_{id}$$

考察电流输入时，由于本征跨阻增益和本征电流增益假设无穷大，而输出电压和输出电流有限，故而输入电流虚拟为0（虚断）

虚短、虚断简化分析要求熟练掌握

大多数的负反馈运放电路分析流程：首先判断负反馈，之后假设虚短和虚断

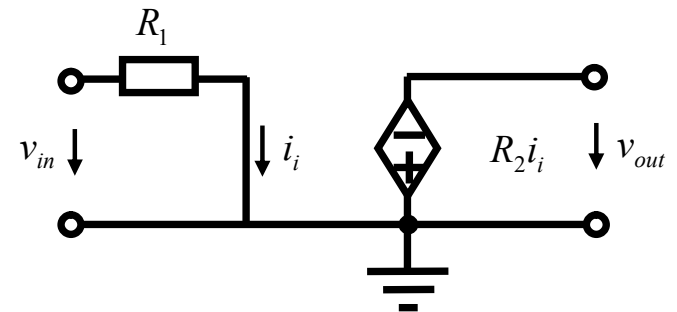
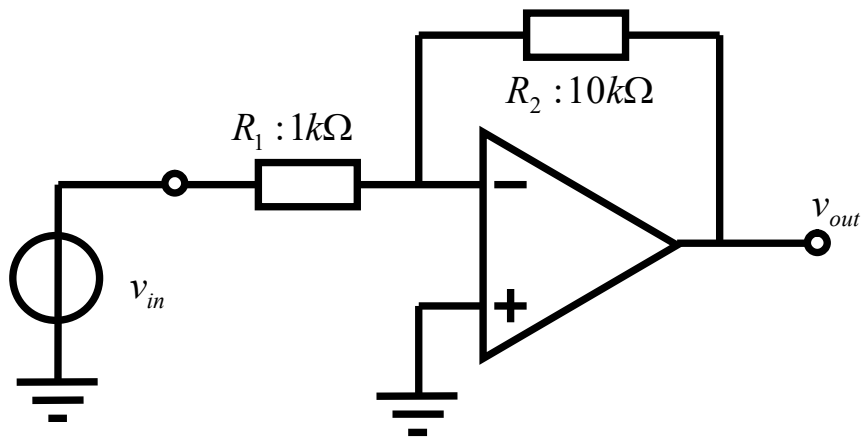
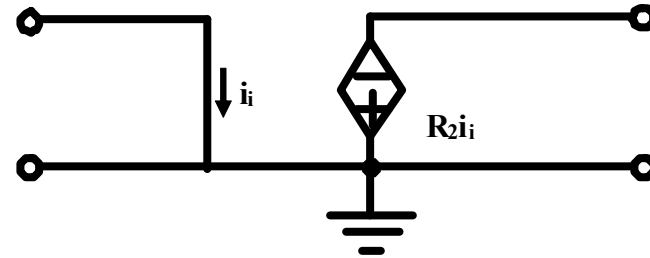
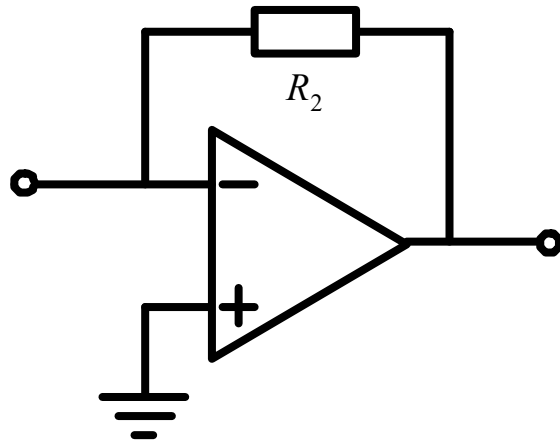


理想运放线性区的虚短、虚断特性：
反相输入端虚拟接地，但无电流流入

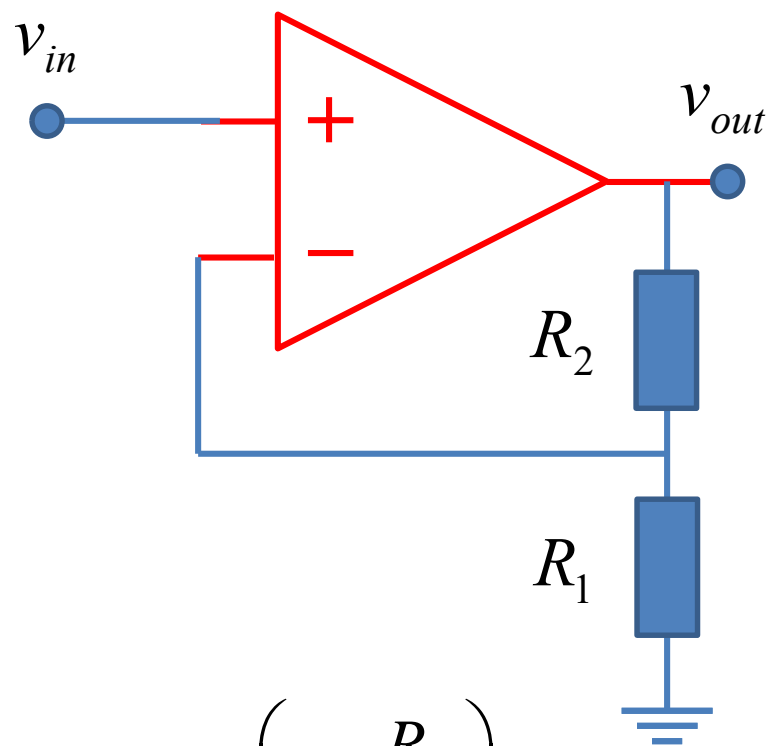
运放外围电路是正反馈还是负反馈？

- 只要从输出端连接到反相输入端，则是负反馈连接方式
 - 如果反馈网络是电阻网络，一阶阻容网络，则为负反馈
 - 如果反馈网络为二阶或二阶以上阻容网络，由于阻容网络或可形成 180° 移相，有可能将负反馈连接变成正反馈连接（下学期振荡器设计）
- 只要从输出端连接到同相输入端，则是正反馈连接方式
- 如果输出端同时有连接到同相输入端和反相输入端
 - 考察 $F_p = \Delta v_p / \Delta v_o$ ， $F_n = \Delta v_n / \Delta v_o$ 两个反馈系数
 - $F_p > F_n$ ，正反馈占优，则为正反馈
 - $F_p < F_n$ ，负反馈占优，则为负反馈
- 如果确定为负反馈，运放则可假定工作在线性区，用虚短、虚断分析，如果分析结果中的输出电压超过饱和电压，运放则工作在饱和区
- 如果确定为正反馈，运放则可假定工作在正负饱和区

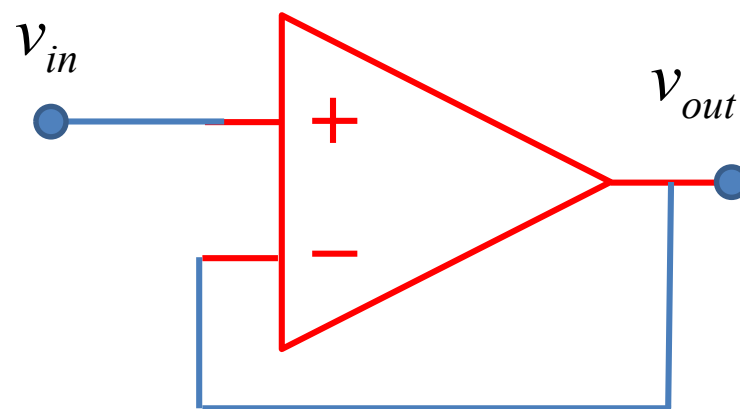
并并连接负反馈：应用最多



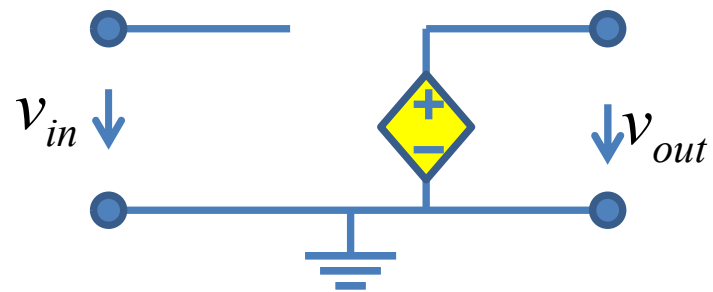
串并连接负反馈：电压缓冲器



$$v_{out} = \left(1 + \frac{R_2}{R_1}\right) v_{in}$$

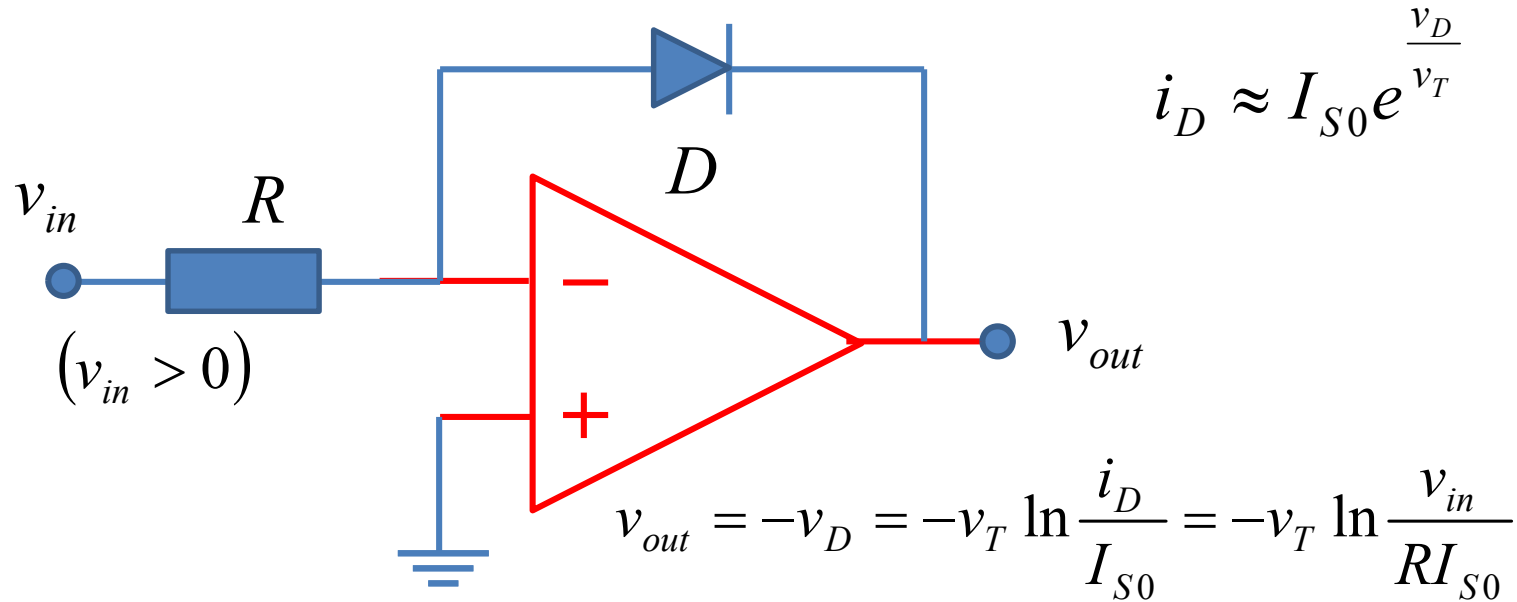


$$v_{out} = v_{in}$$

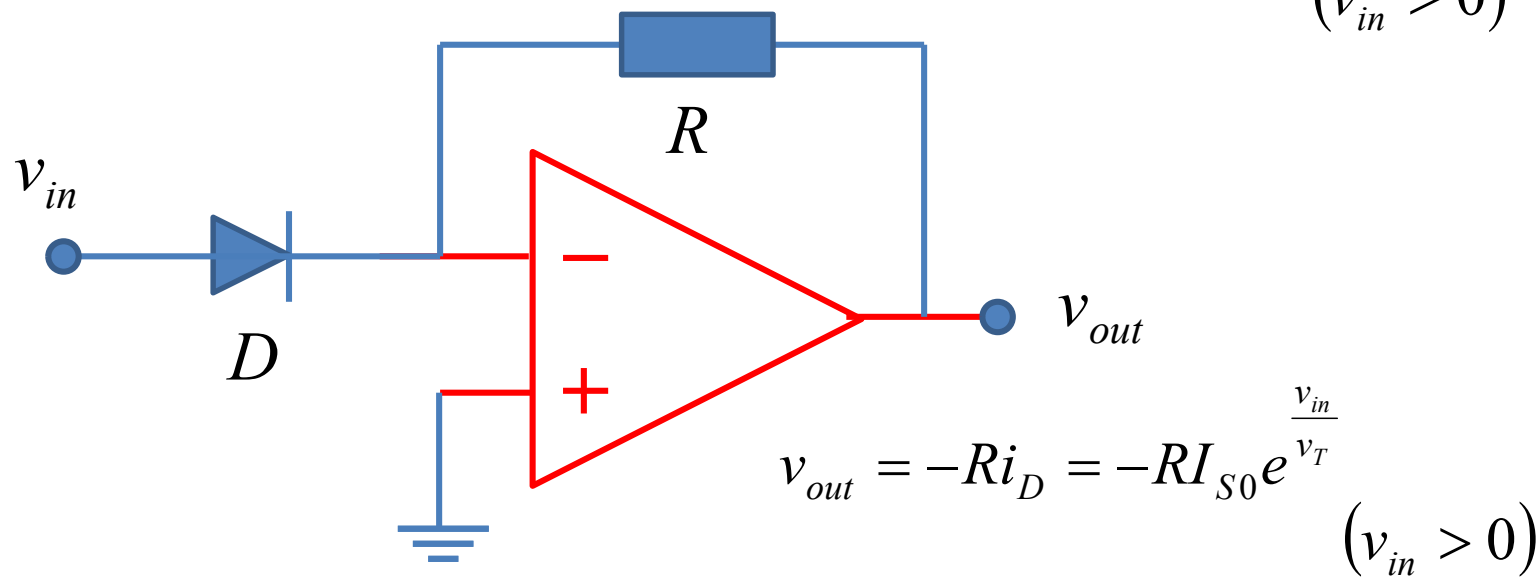


隔离，缓冲
单向传输，解除反向耦合

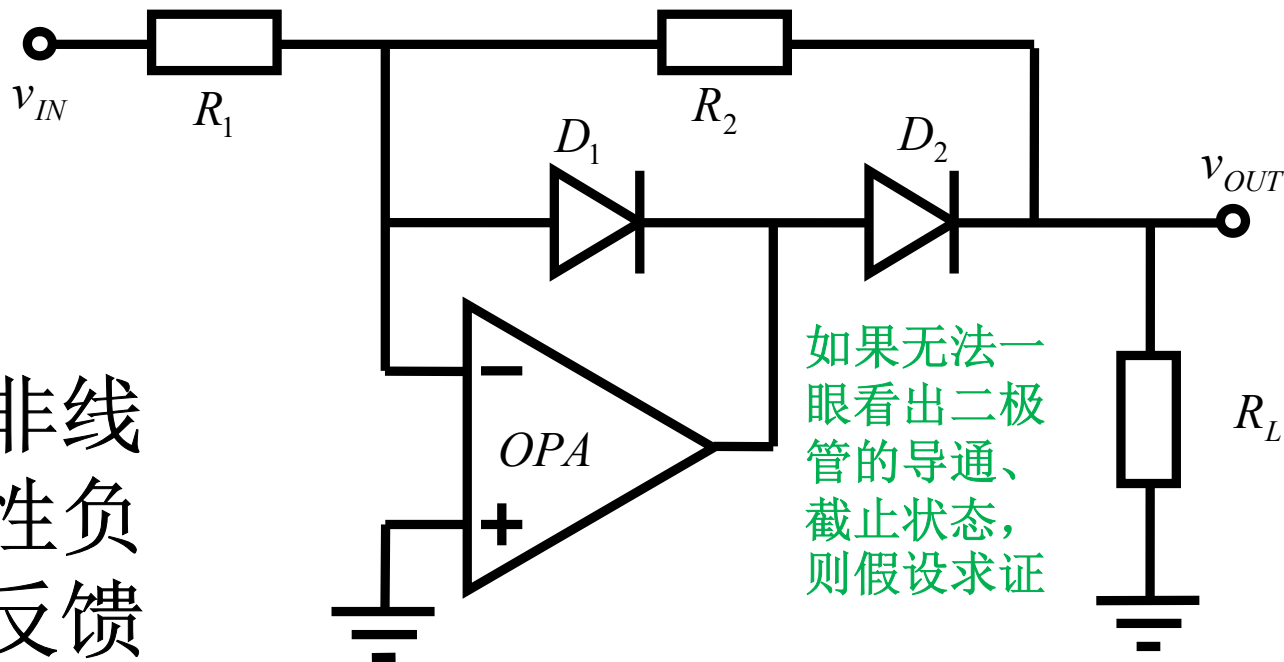
负反馈 非线性应用



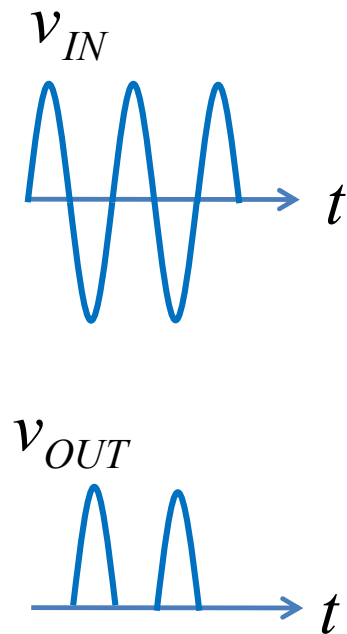
$(v_{in} > 0)$



非线性负反馈应用



如果无法一眼看出二极管的导通、截止状态，则假设求证



$$v_{IN} > 0$$

D_1 导通

$$v_{OUT} = 0$$

$$v_{OPA,O} = -0.7V$$

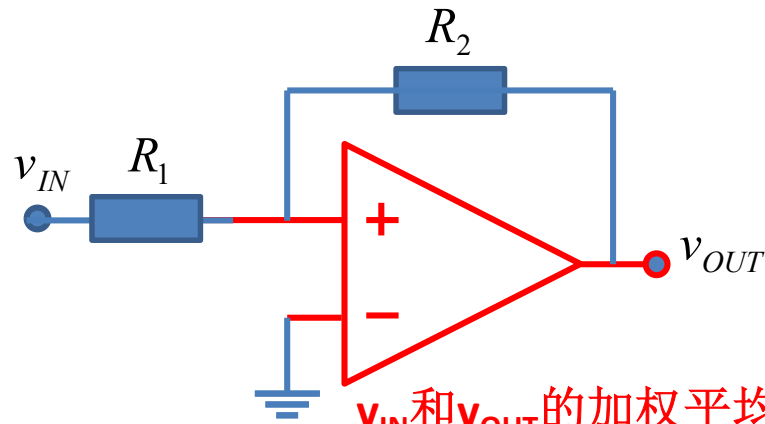
$$v_{IN} < 0$$

D_2 导通

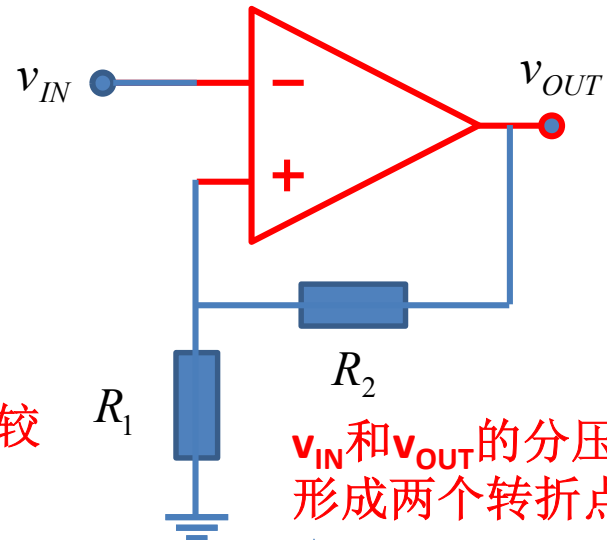
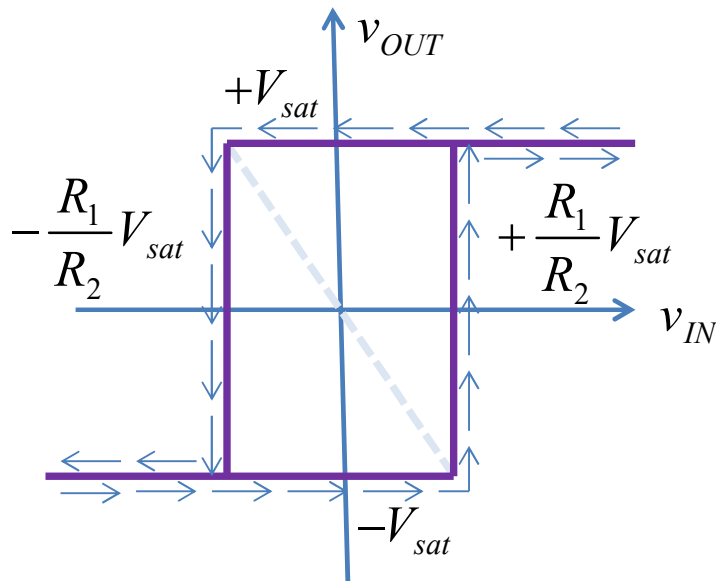
$$v_{OUT} = -\frac{R_2}{R_1} v_{IN}$$

$$v_{OPA,O} = v_{OUT} + 0.7V$$

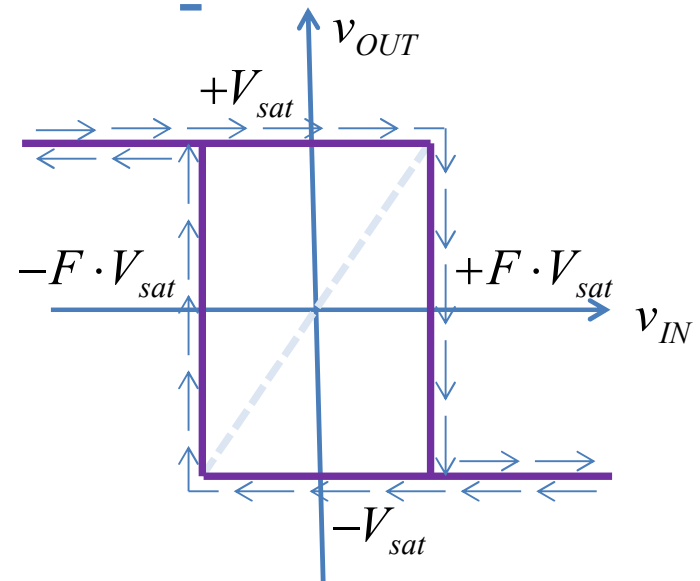
两个最基本的正反馈：施密特触发器



v_{IN} 和 v_{OUT} 的加权平均和0进行比较
形成两个转折点

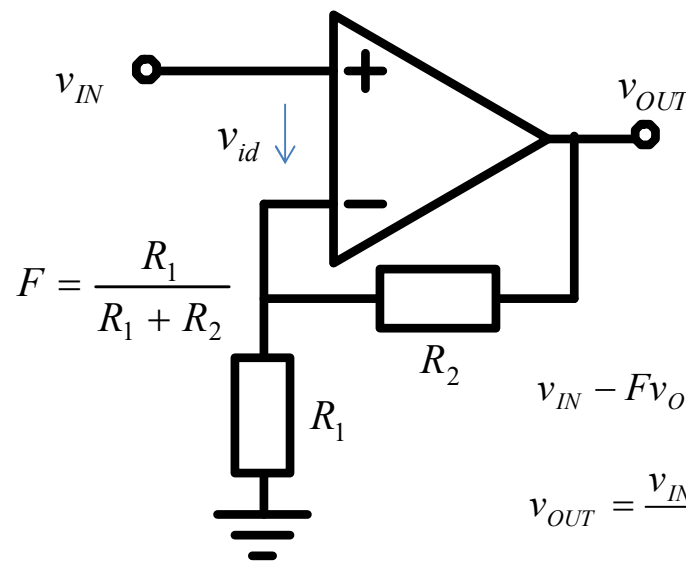


v_{IN} 和 v_{OUT} 的分压进行比较
形成两个转折点



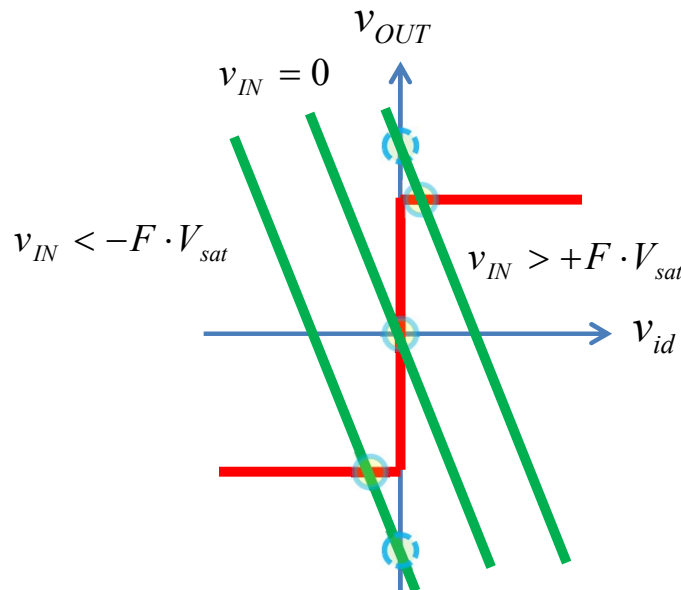
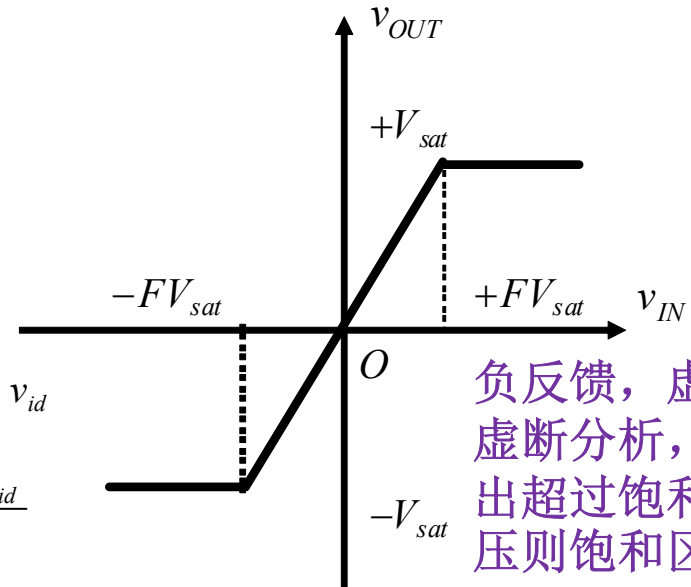
线性负反馈 唯一输出

线性正反馈与线性负反馈的区别



$$v_{IN} - Fv_{OUT} = v_{id}$$

$$v_{OUT} = \frac{v_{IN} - v_{id}}{F}$$

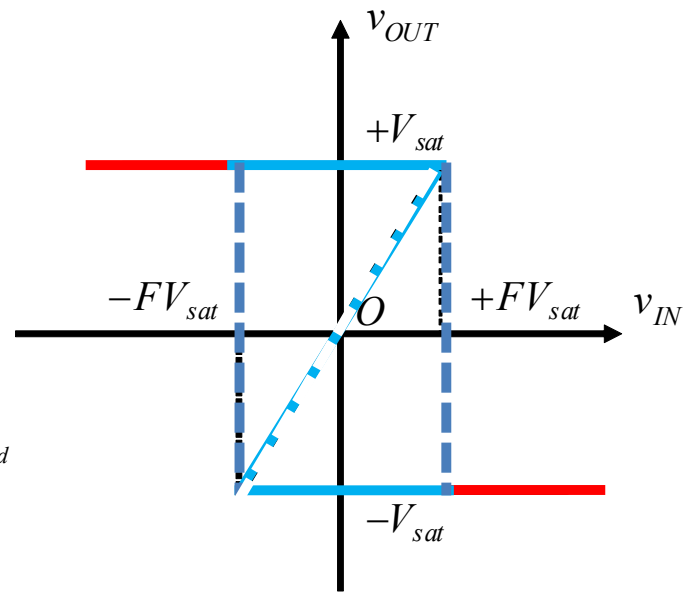
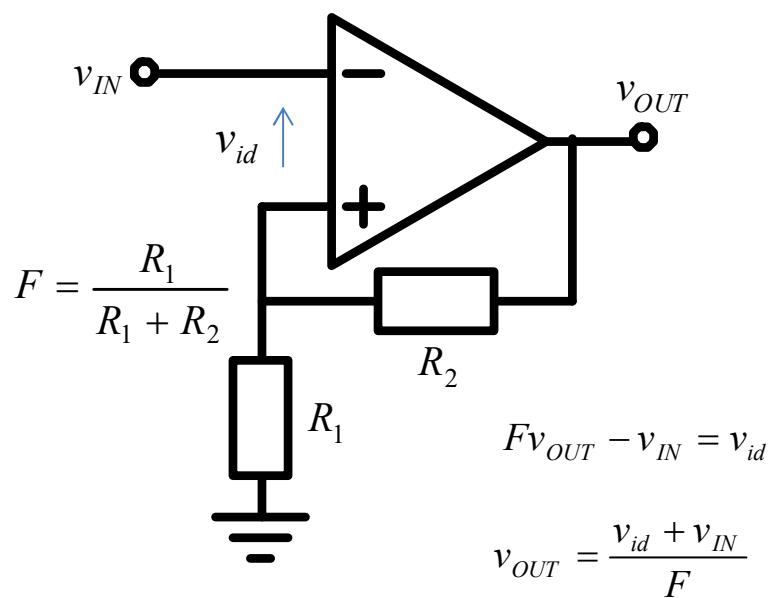


线性区

$$v_{IN} = F \cdot v_{OUT}$$

$$v_{OUT} = \frac{1}{F} v_{IN} = \left(1 + \frac{R_2}{R_1}\right) v_{IN}$$

线性正反馈



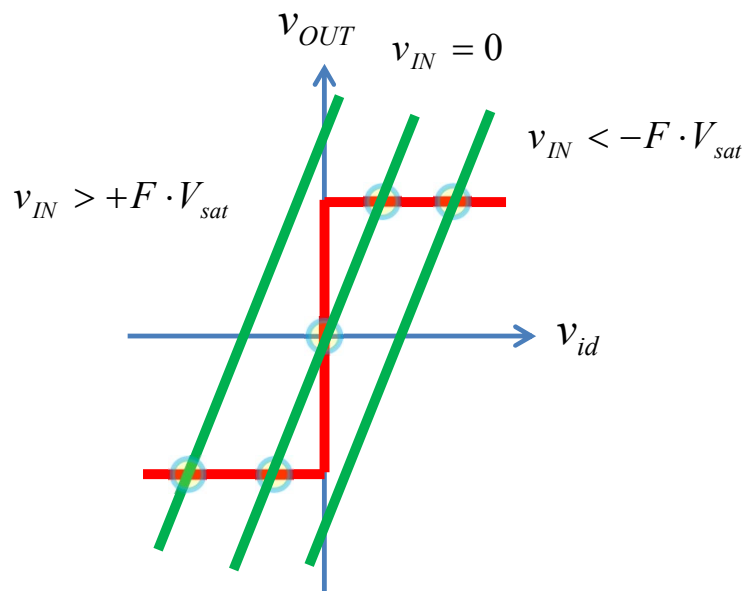
线性区 $v_{IN} = F \cdot v_{OUT}$

$$v_{OUT} = \frac{1}{F} v_{IN} = \left(1 + \frac{R_2}{R_1}\right) v_{IN}$$

不稳定区：待不住

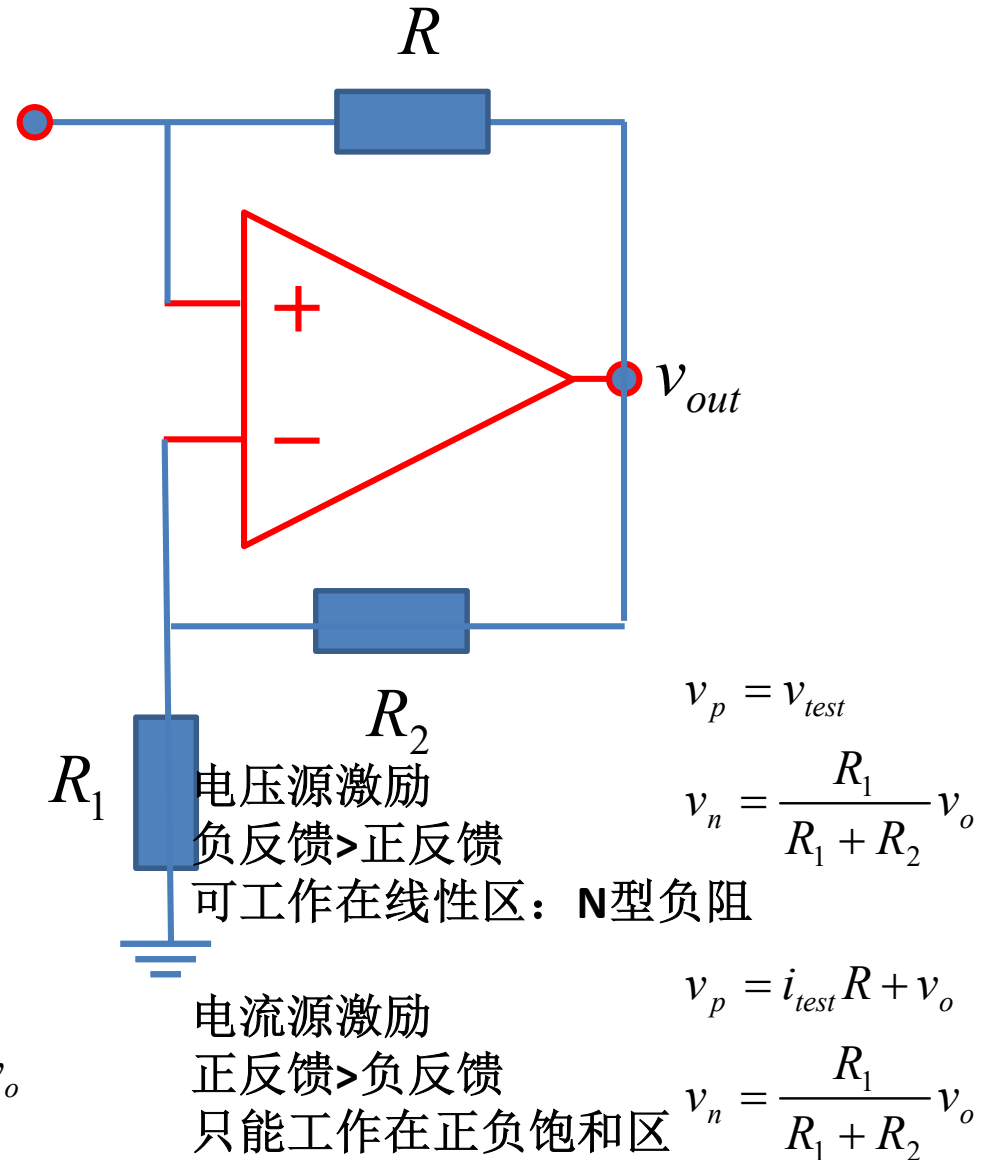
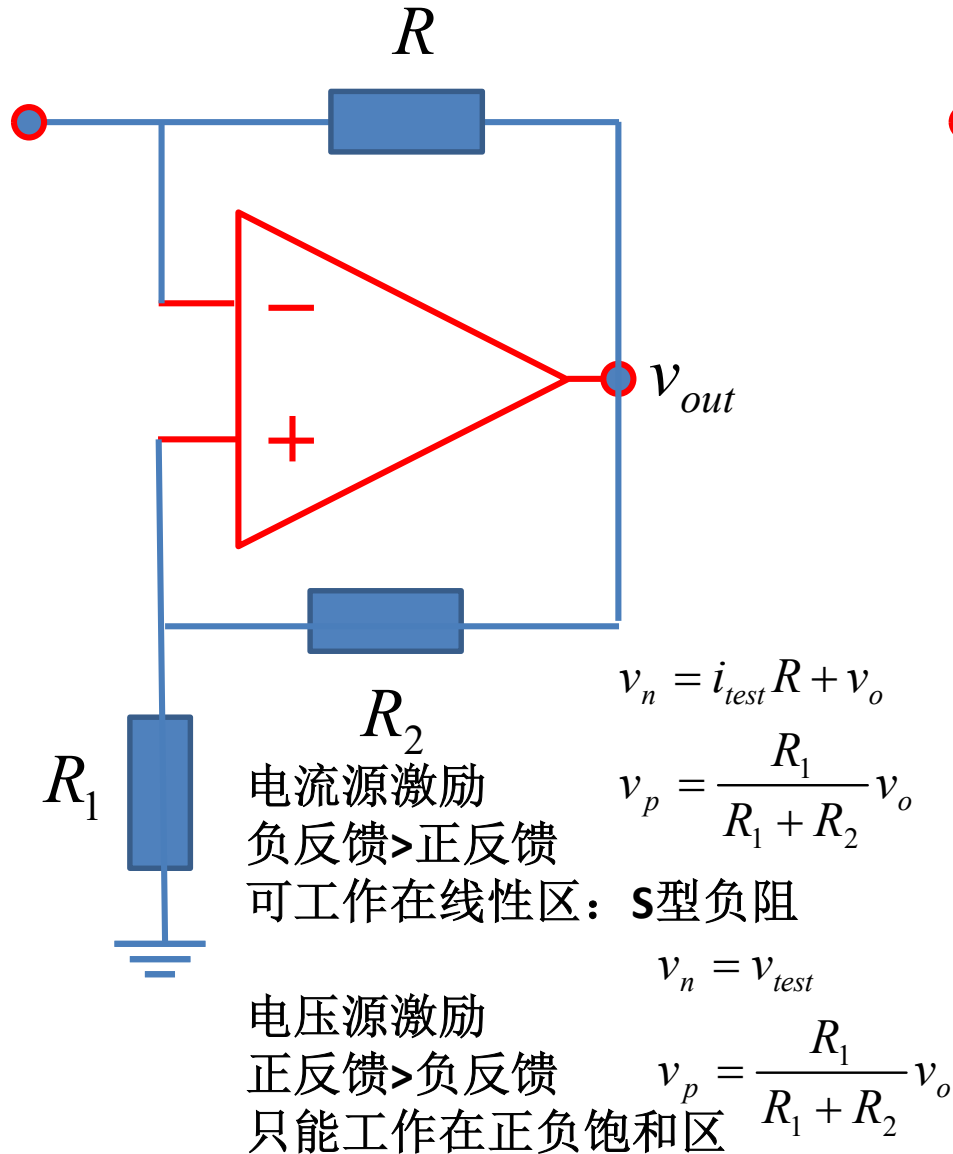
理论转移特性曲线
实际转移特性曲线：滞回曲线

非唯一输出

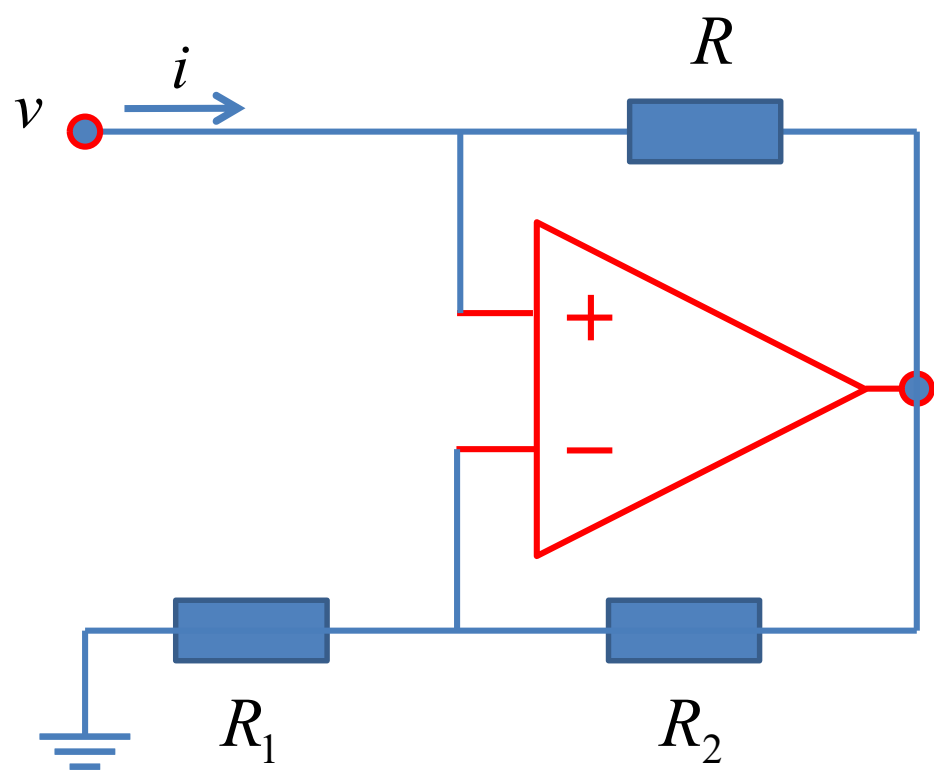


同时有正反馈和负反馈

不能再用连接关系判断受控源类型：不再是用负反馈稳定输出

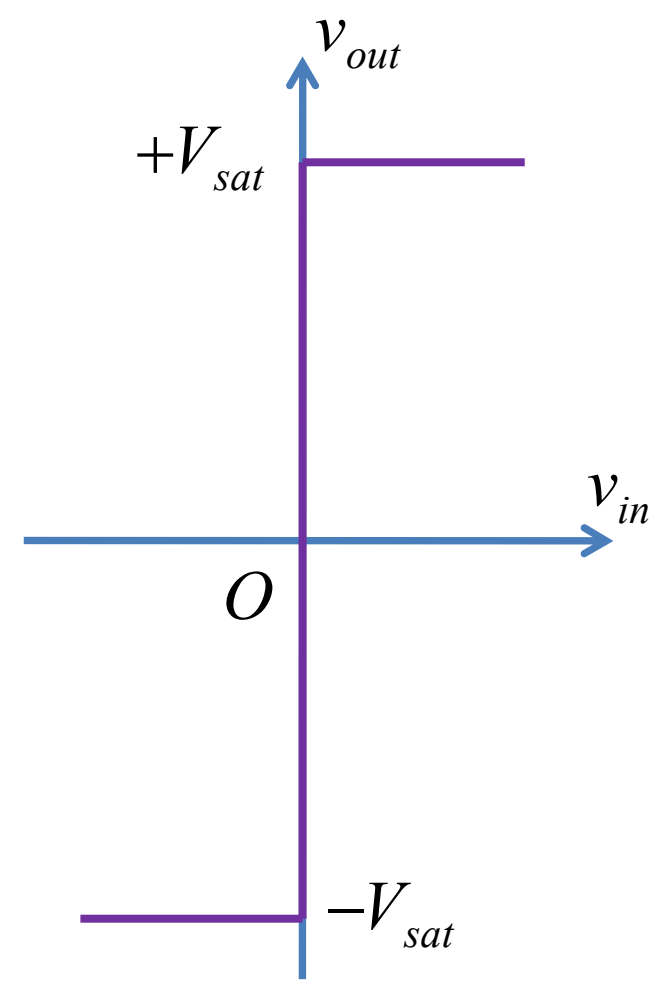


- 已知理想运放的转移特性，分析确认如图所示单端口网络的伏安特性为N型负阻
 - 提示1: 假设在线性区，假设在正饱和区，假设在负饱和区，分别考察
 - 提示2: 电压源驱动，N型具有唯一解
 - 电压源驱动，确保负反馈

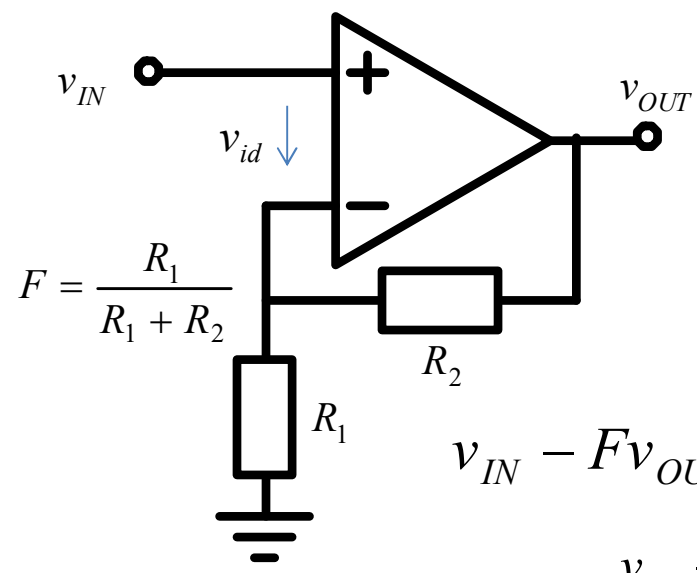


作业2

N型负阻



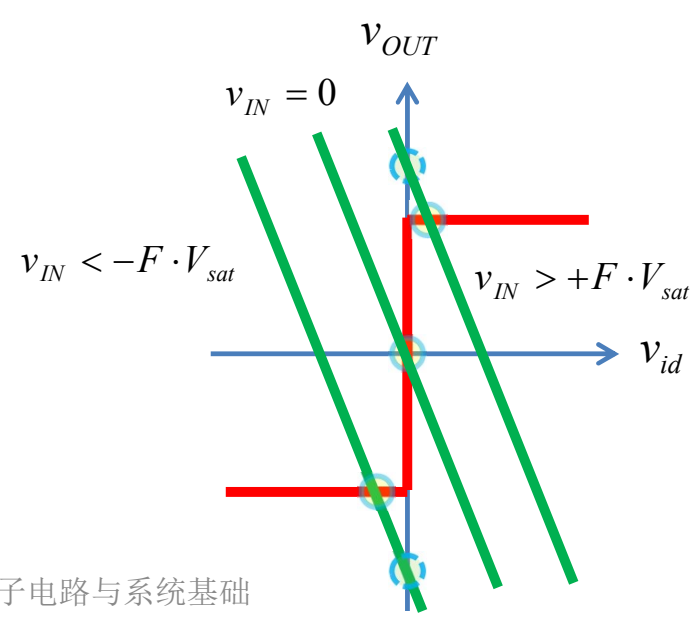
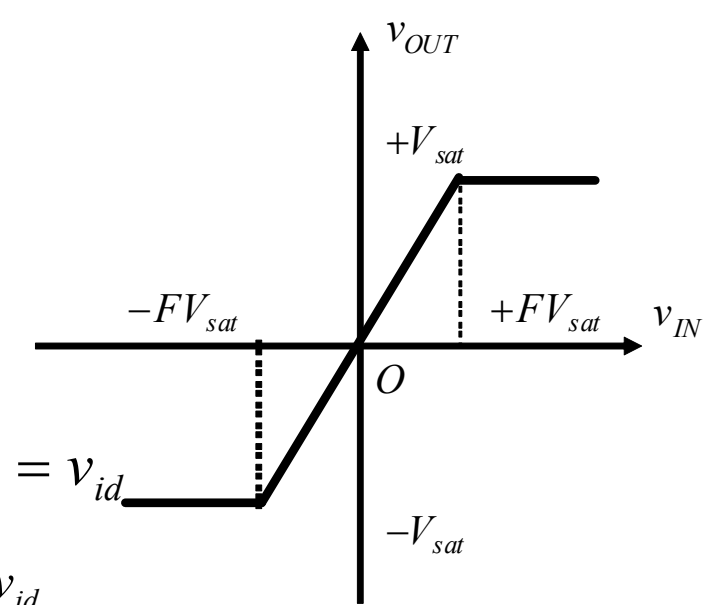
同相电压放大器



$$F = \frac{R_1}{R_1 + R_2}$$

$$v_{IN} - Fv_{OUT} = v_{id}$$

$$v_{OUT} = \frac{v_{IN} - v_{id}}{F}$$

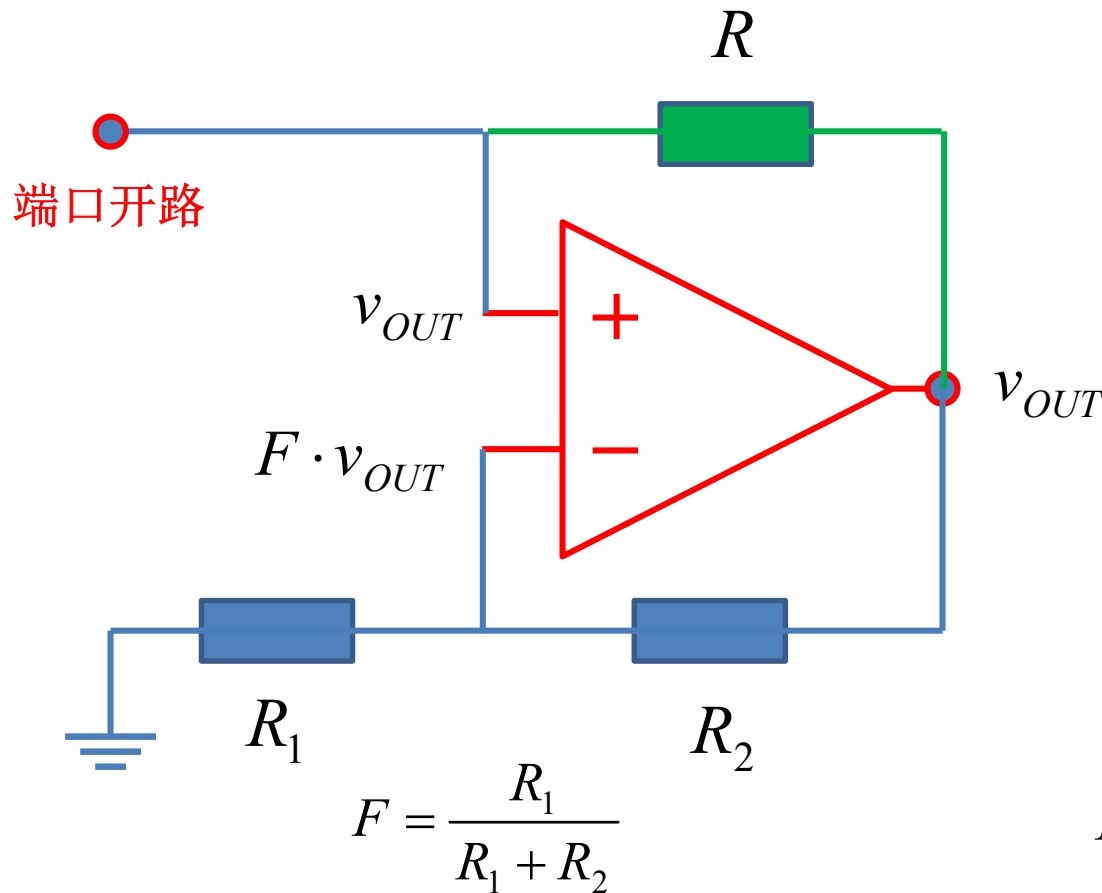


线性区

$$v_{IN} = F \cdot v_{OUT}$$

$$v_{OUT} = \frac{1}{F} v_{IN} = \left(1 + \frac{R_2}{R_1} \right) v_{IN}$$

正反馈则无法待在线性区



可能性1: 运放线性区

$$v_{OUT} = F \cdot v_{OUT}$$

$$v_{OUT} = 0$$



可能性2: 运放正饱和区

$$V_{sat} > F \cdot V_{sat}$$



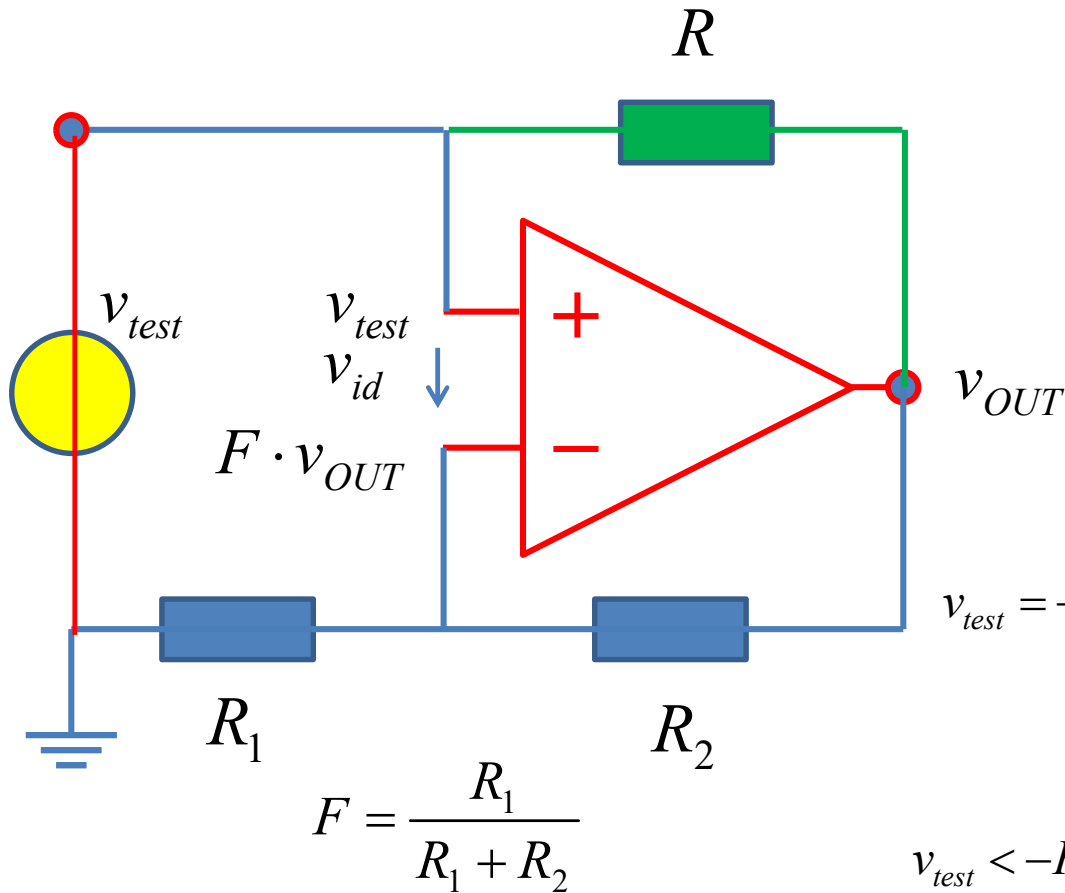
可能性3: 运放负饱和区

$$F \cdot (-V_{sat}) > -V_{sat}$$

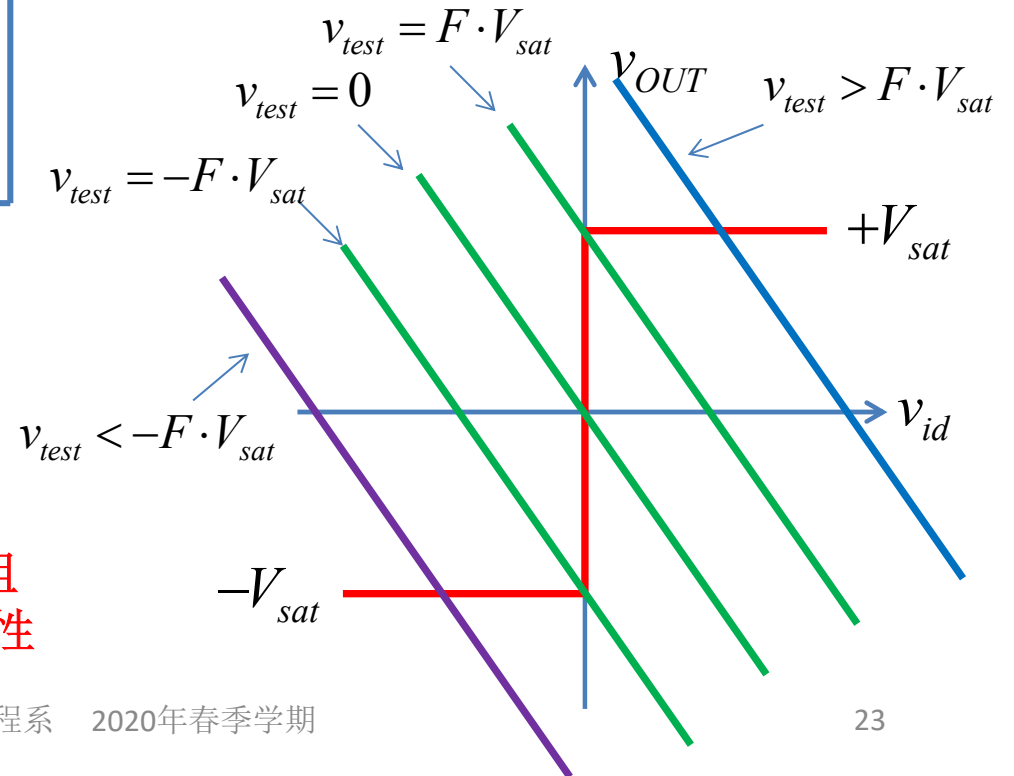


输入端口开路，正反馈高于负反馈，电路中的噪声，
将导致运放无法待在线性区

同相输入端恒压源取消正反馈



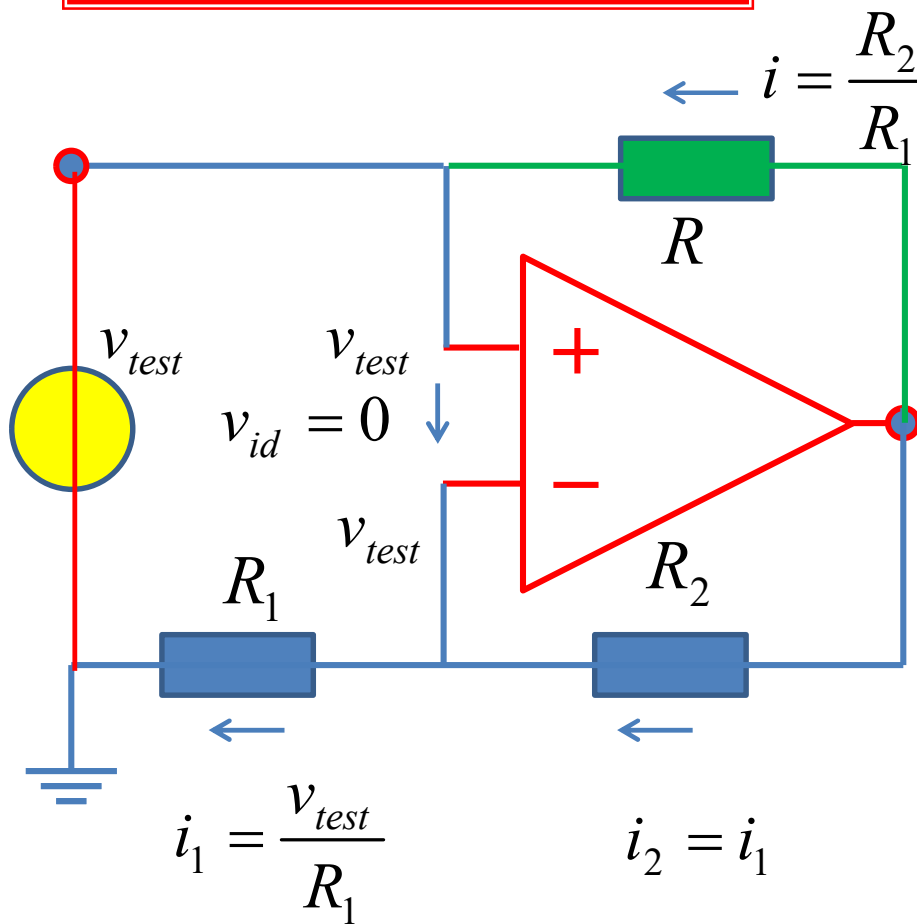
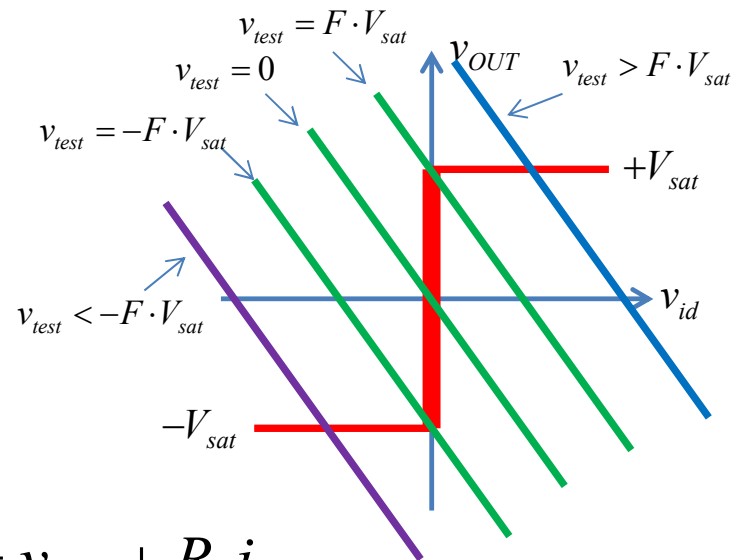
加压测试负反馈：N型负阻
 加流测试正反馈：滞回特性



运放线性区

$$-F \cdot V_{sat} < v_{test} < +F \cdot V_{sat}$$

$$F = \frac{R_1}{R_1 + R_2}$$



$$i = \frac{R_2}{R_1} \frac{v_{test}}{R}$$

$$v_{OUT} = v_{test} + R_2 i_2$$

$$= v_{test} + \frac{R_2}{R_1} v_{test}$$

$$= \frac{v_{test}}{F} \in (-V_{sat}, V_{sat})$$

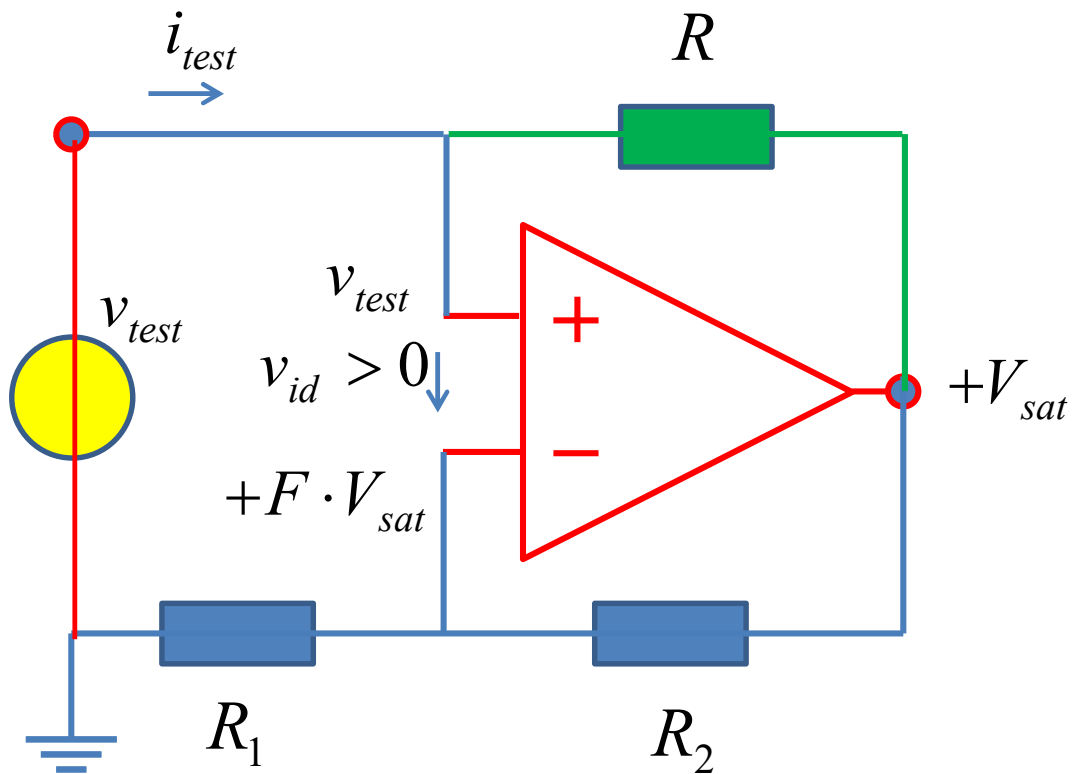
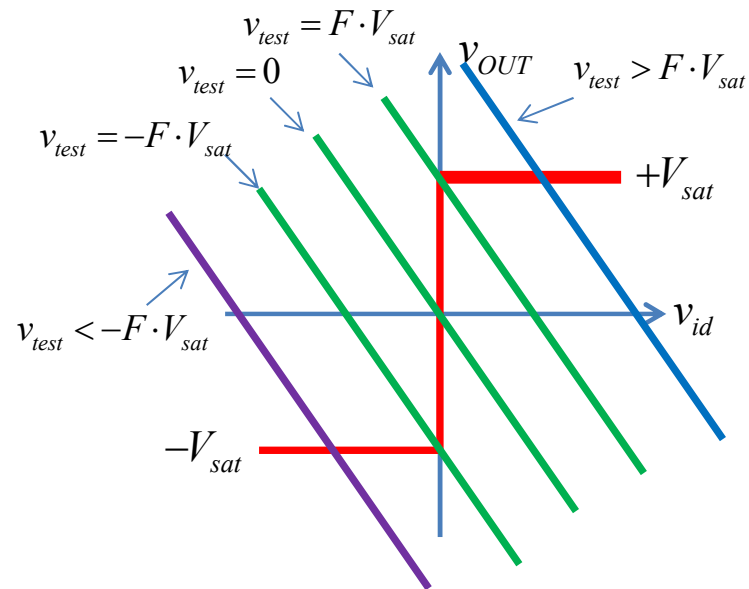
$$i = \frac{R_2}{R_1} \frac{v_{test}}{R} = -i_{test}$$

$$v_{test} = -i_{test} \frac{R_1}{R_2} R$$

运放正饱和区

$$v_{test} > +F \cdot V_{sat}$$

$$F = \frac{R_1}{R_1 + R_2}$$

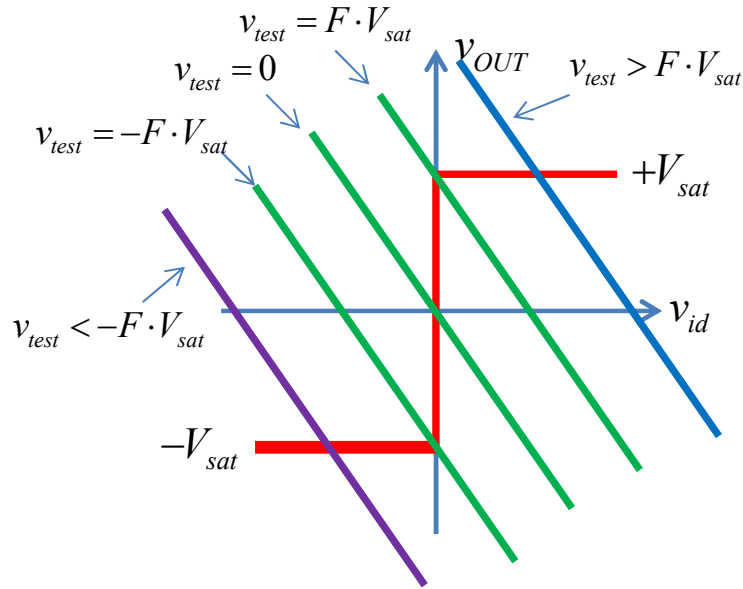
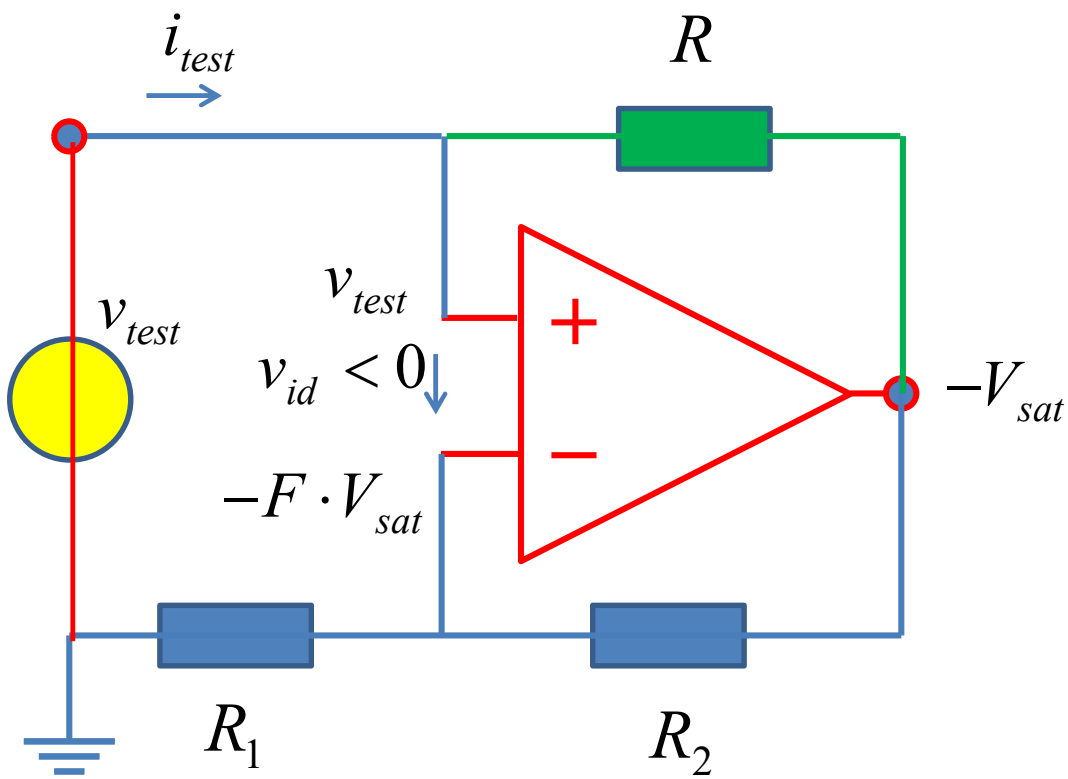


$$v_{test} = i_{test} R + V_{sat}$$

运放负饱和区

$$v_{test} < -F \cdot V_{sat}$$

$$F = \frac{R_1}{R_1 + R_2}$$



$$v_{test} = i_{test} R - V_{sat}$$

N型负阻 压控器件

运放线性区

$$-F \cdot V_{sat} < v_{test} < +F \cdot V_{sat}$$

$$v_{test} = -i_{test} \frac{R_1}{R_2} R$$

$$i_{test} = -\frac{R_2}{R_1} \frac{v_{test}}{R}$$

运放正饱和区

$$v_{test} > +F \cdot V_{sat}$$

$$v_{test} = i_{test} R + V_{sat}$$

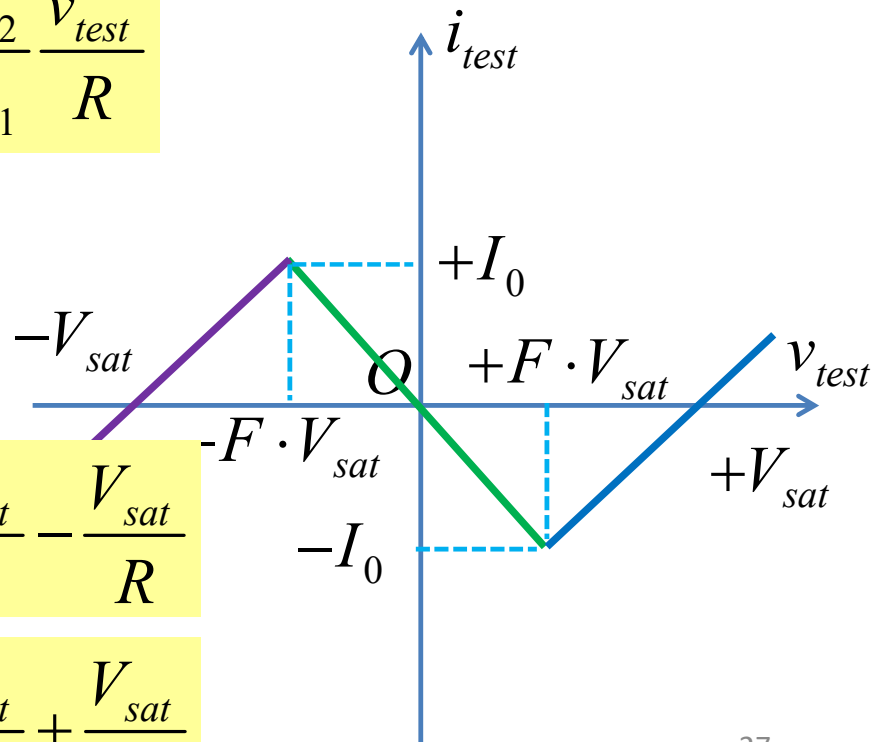
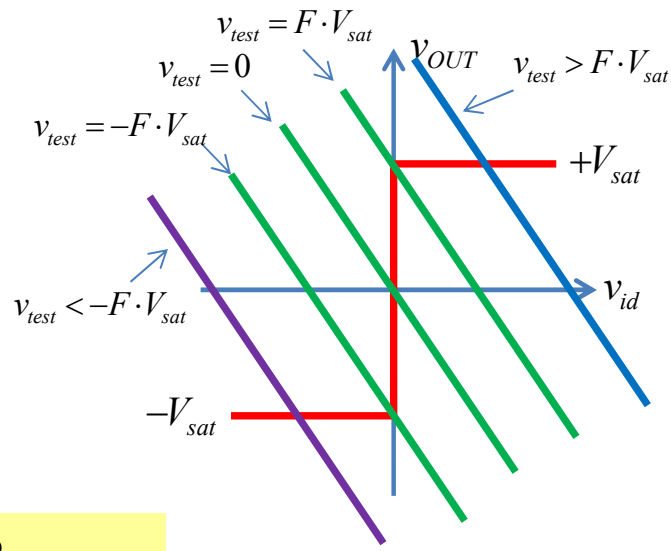
运放负饱和区

$$v_{test} < -F \cdot V_{sat}$$

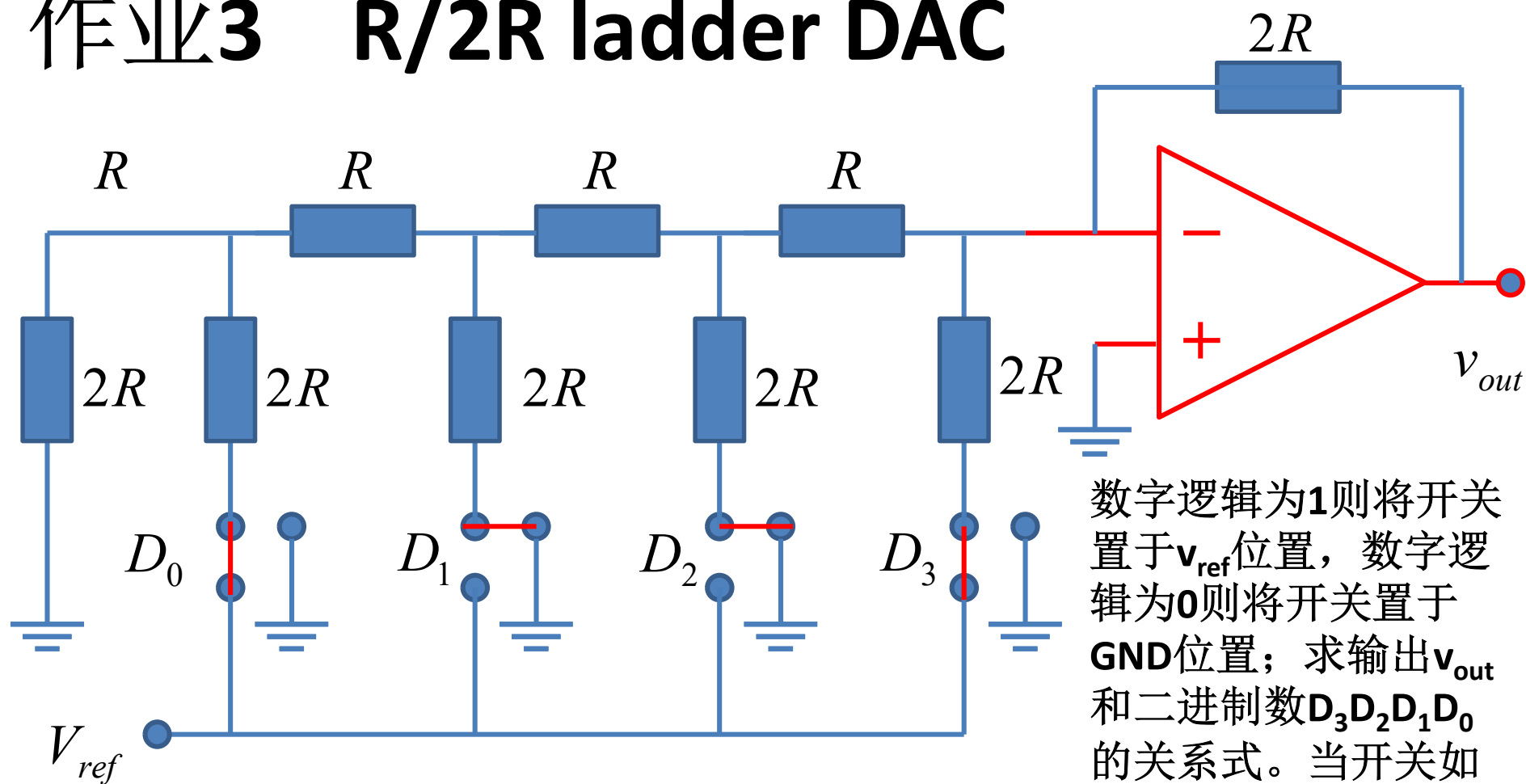
$$v_{test} = i_{test} R - V_{sat}$$

$$i_{test} = \frac{v_{test}}{R} - \frac{V_{sat}}{R}$$

$$i_{test} = \frac{v_{test}}{R} + \frac{V_{sat}}{R}$$

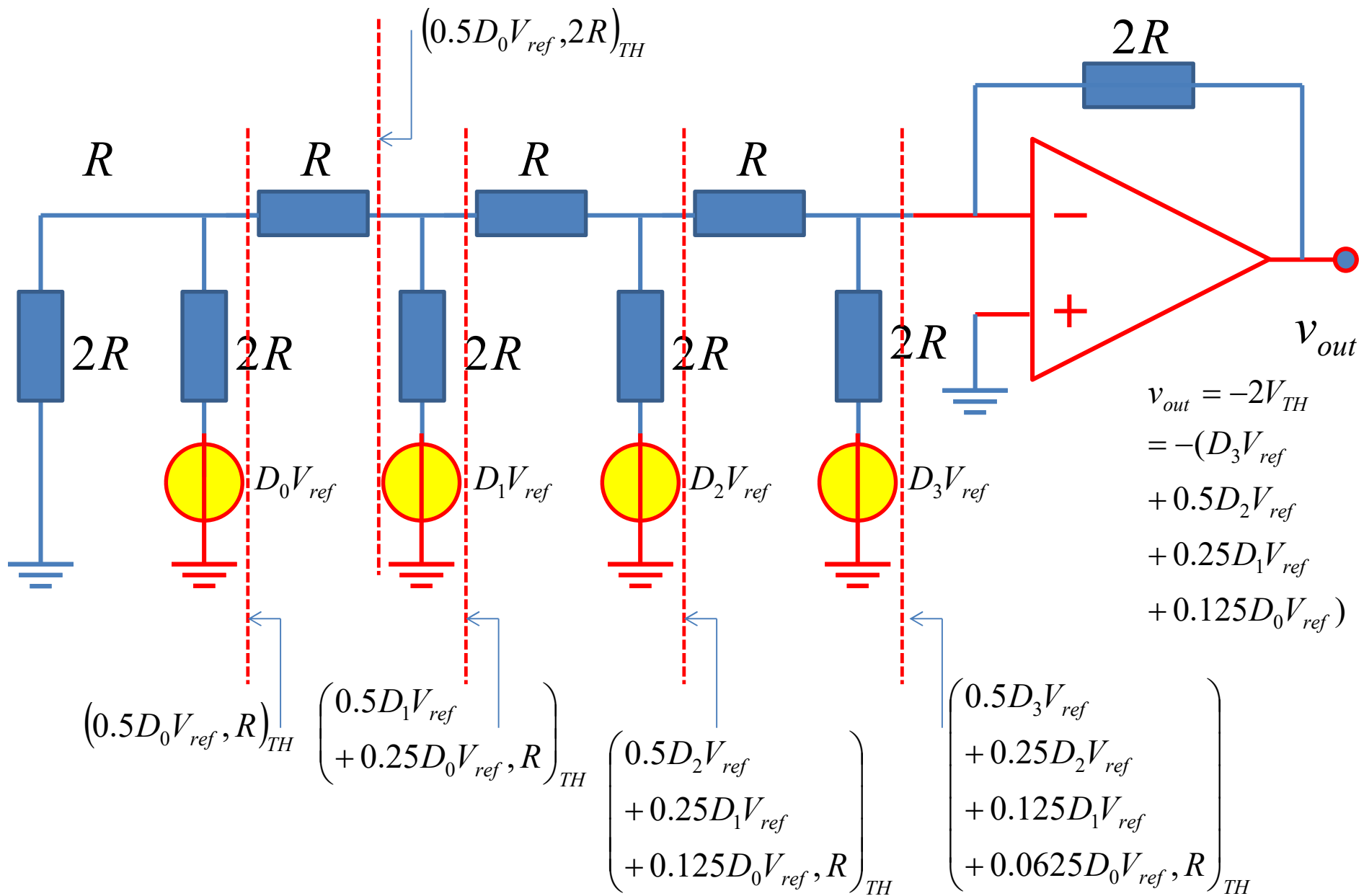


作业3 R/2R ladder DAC



提示：将D0-D3处理为电压源，...

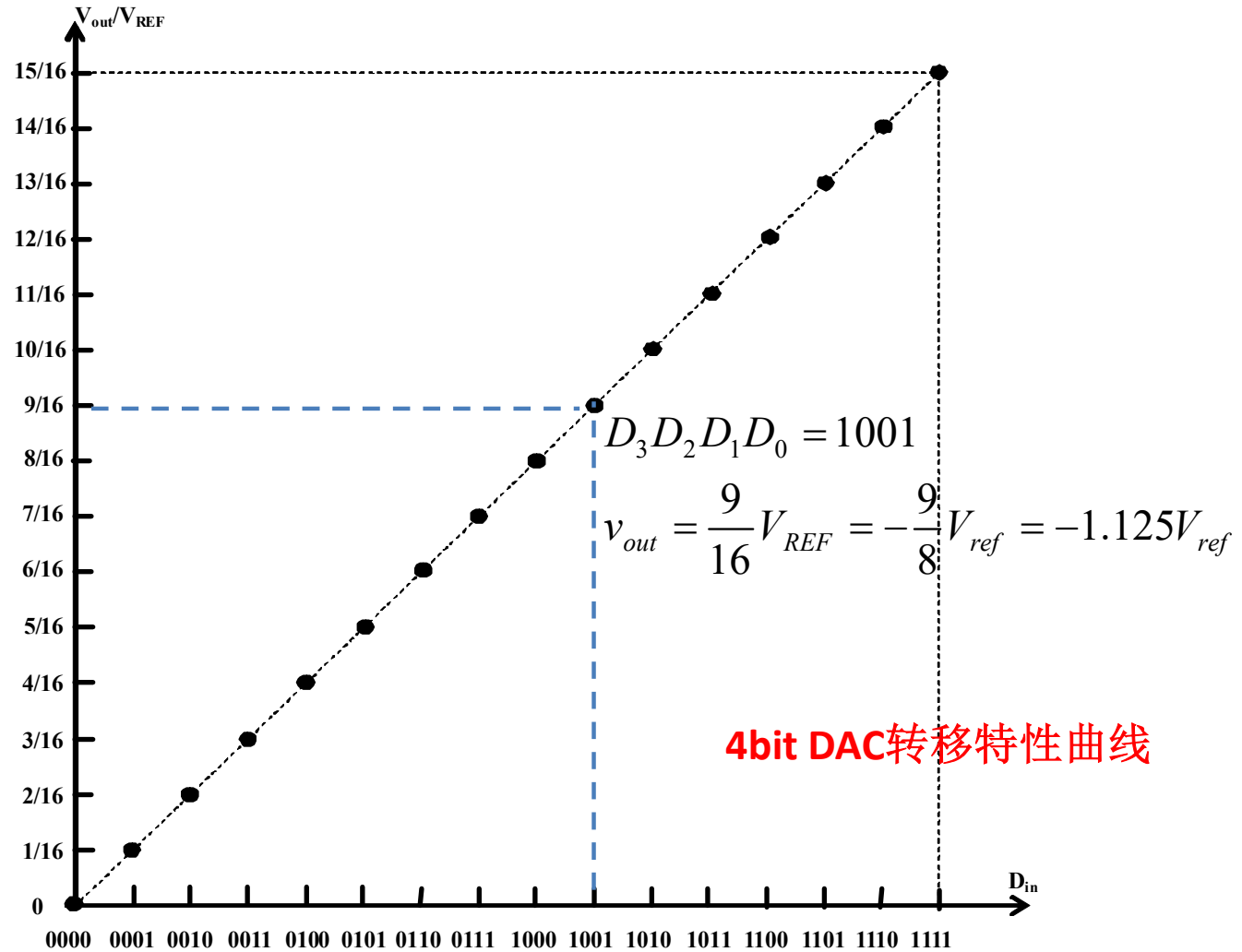
数字逻辑为1则将开关置于 v_{ref} 位置，数字逻辑为0则将开关置于GND位置；求输出 v_{out} 和二进制数 $D_3D_2D_1D_0$ 的关系式。当开关如图所示时，二进制数是多少？对应输出电压为多少？假设 $v_{ref}=5V$ 。



$$v_{out} = -(D_3V_{ref} + 0.5D_2V_{ref} + 0.25D_1V_{ref} + 0.125D_0V_{ref})$$

$$= -\frac{2}{16}V_{ref} (2^3 D_3 + 2^2 D_2 + 2^1 D_1 + 2^0 D_0)$$

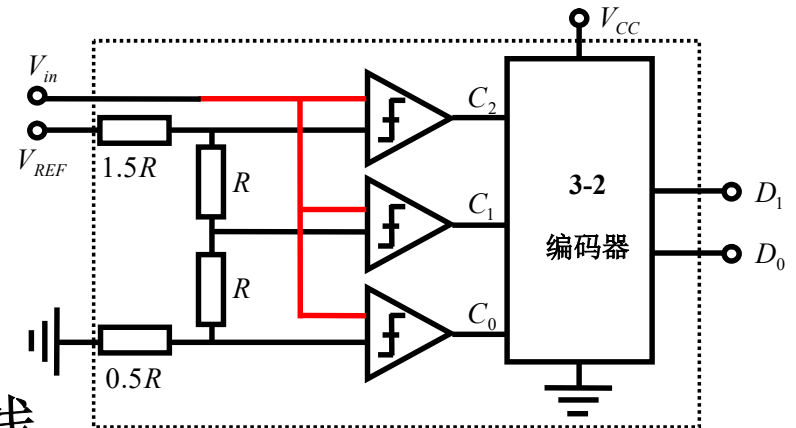
$$= \frac{V_{REF}}{2^4} \sum_{k=0}^3 2^k D_k$$



作业4

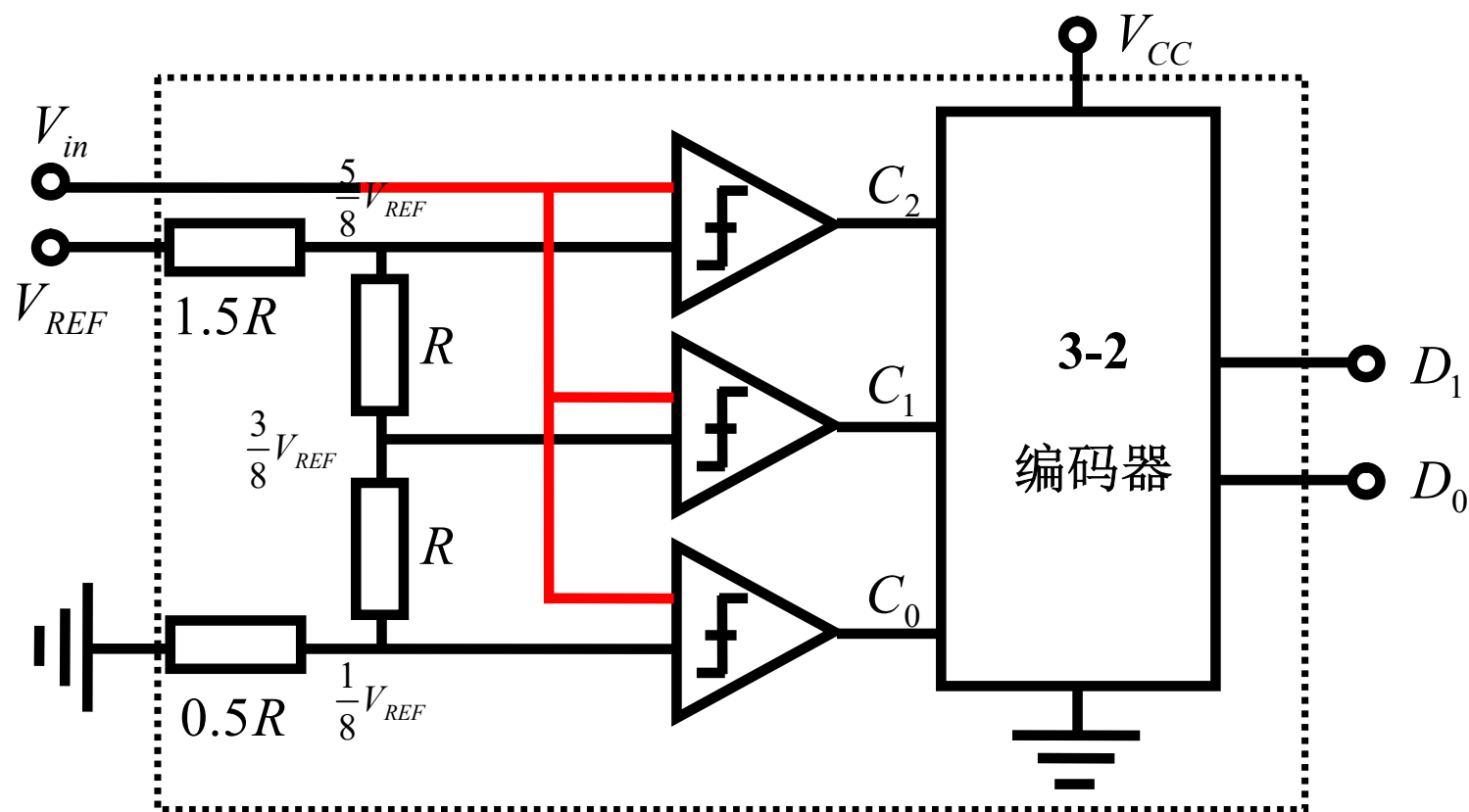
Flash-ADC编码表

- 填写flash-ADC编码的码表
- 画出输入 V_{in} 输出 D_{out} 转移特性曲线

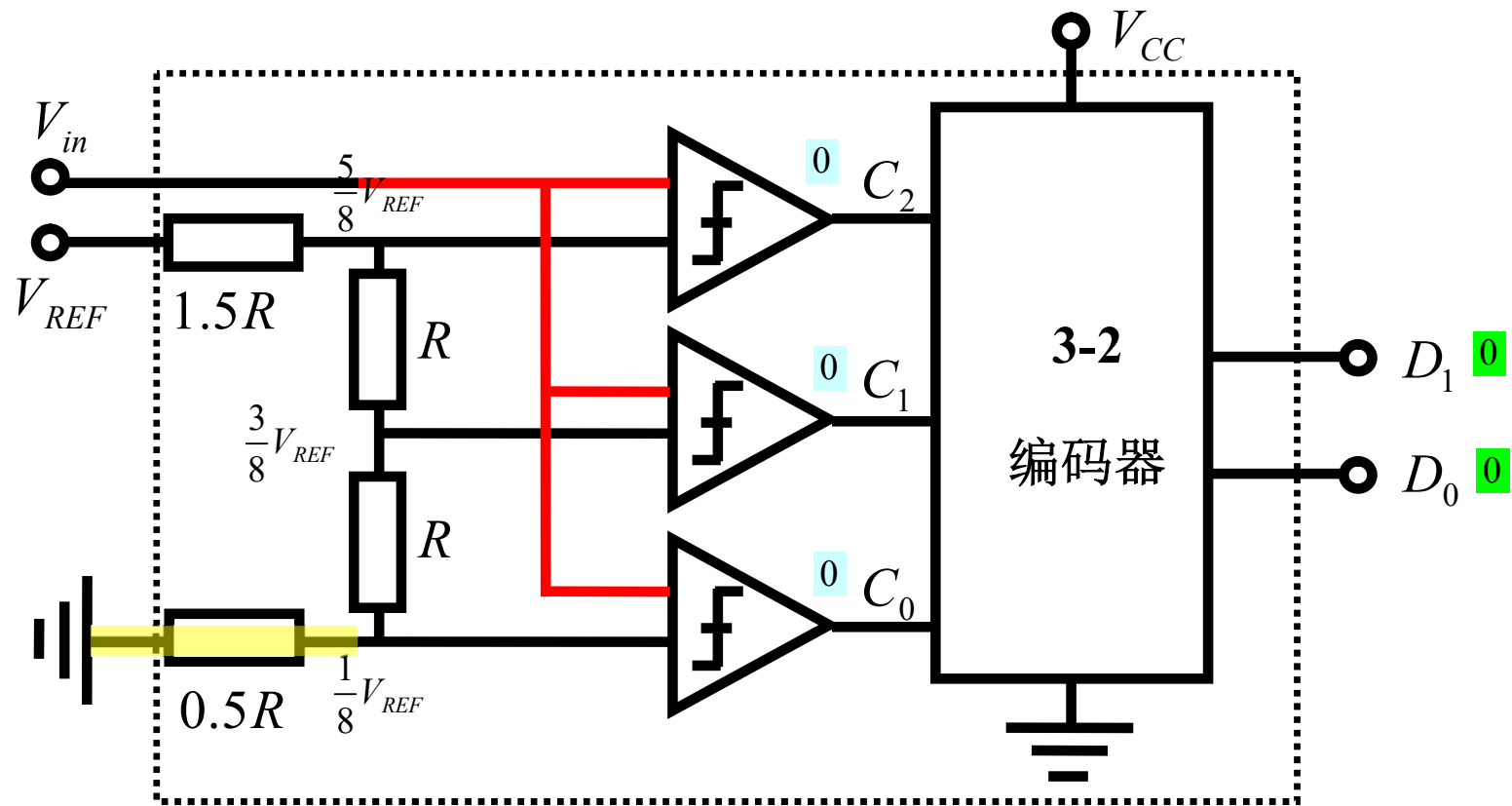


| 模拟输入电压 | $C_2C_1C_0$ | 数字输出码 D_1D_0 |
|--------|-------------|----------------|
| | 000 | 00 |
| | | 01 |
| | | 10 |
| | | 11 |

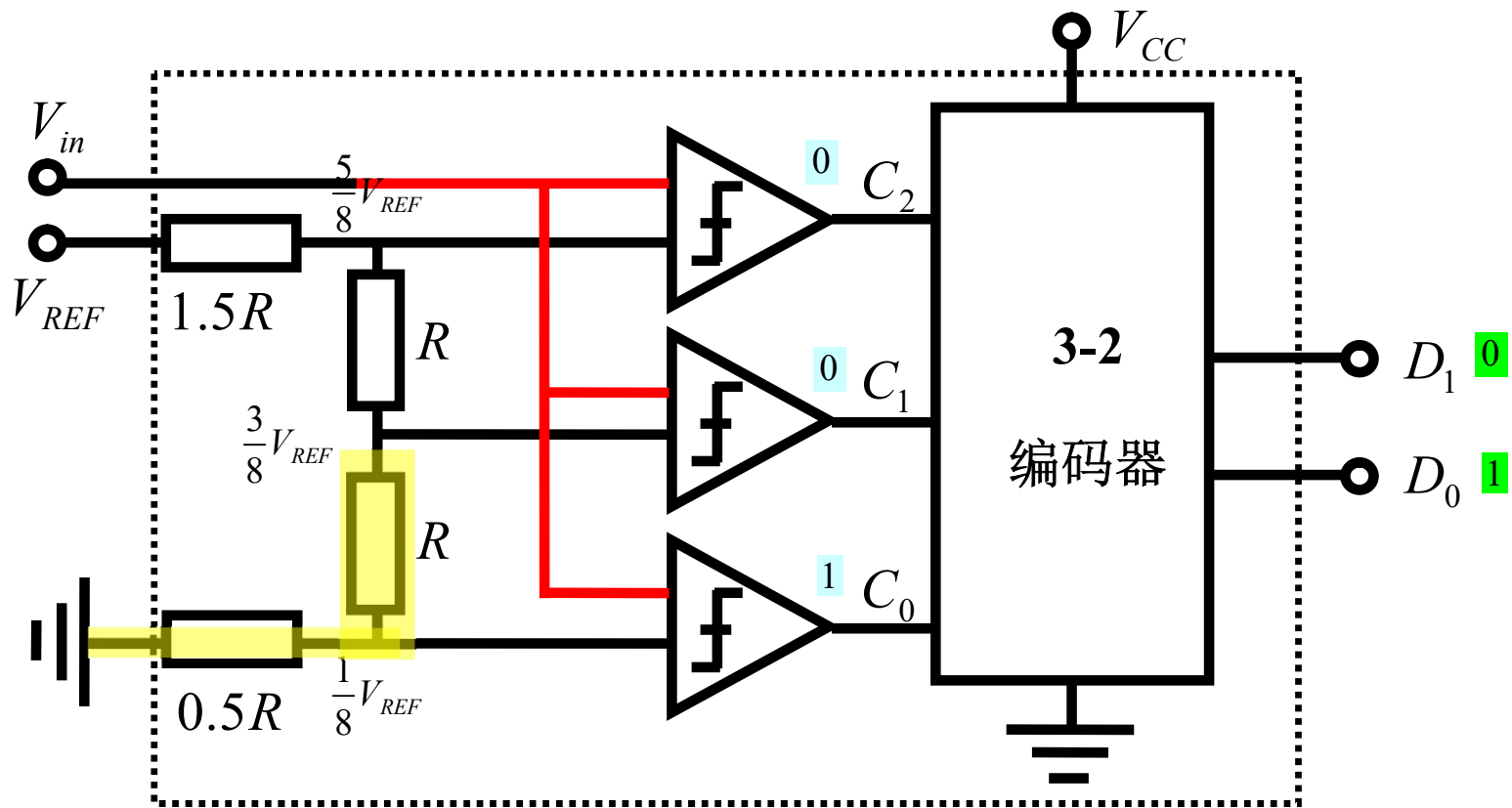
电阻分压网络提供比较电压基准



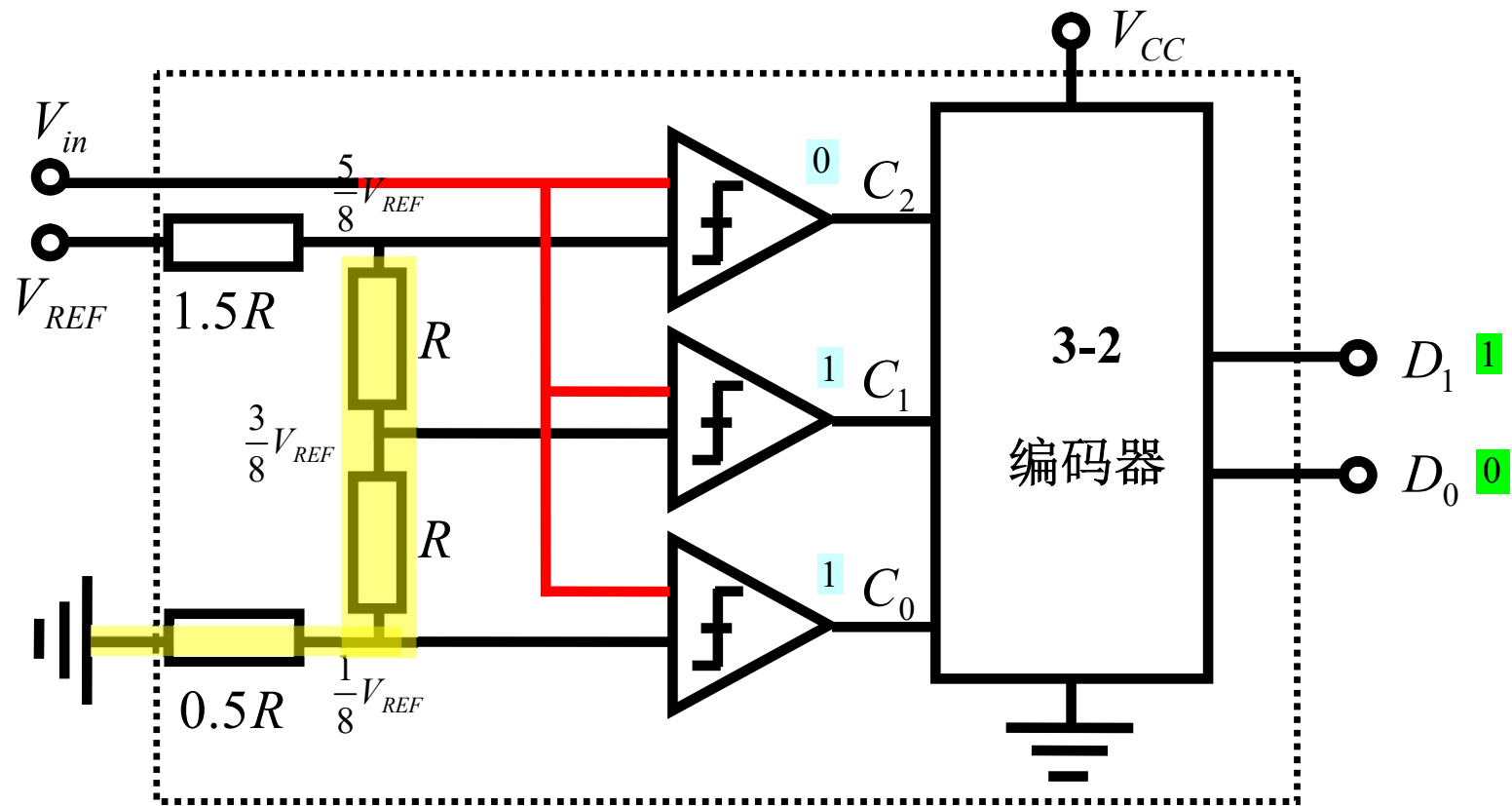
$$V_{in} < V_{REF}/8$$



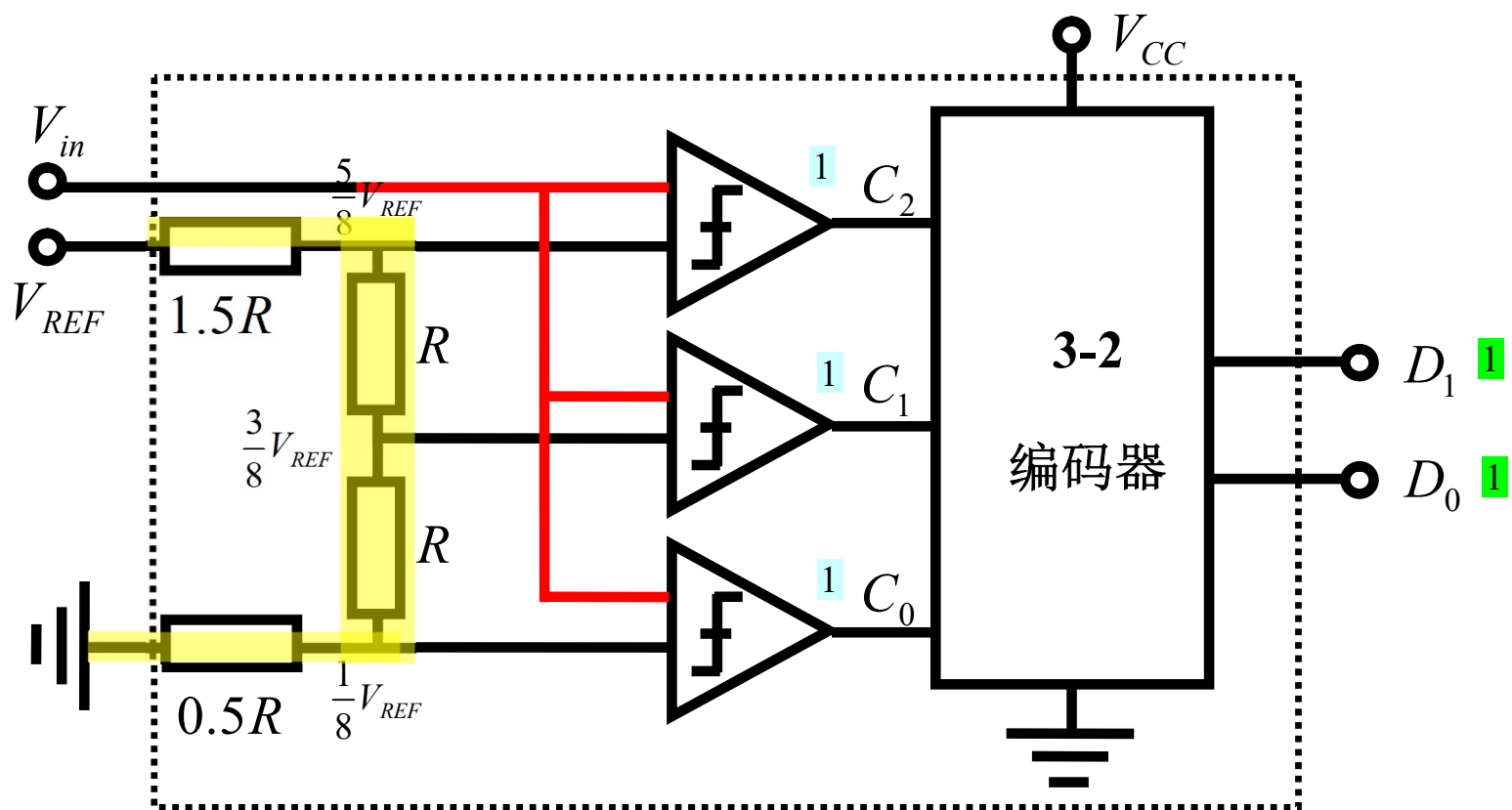
$$V_{REF}/8 < V_{in} < 3V_{REF}/8$$



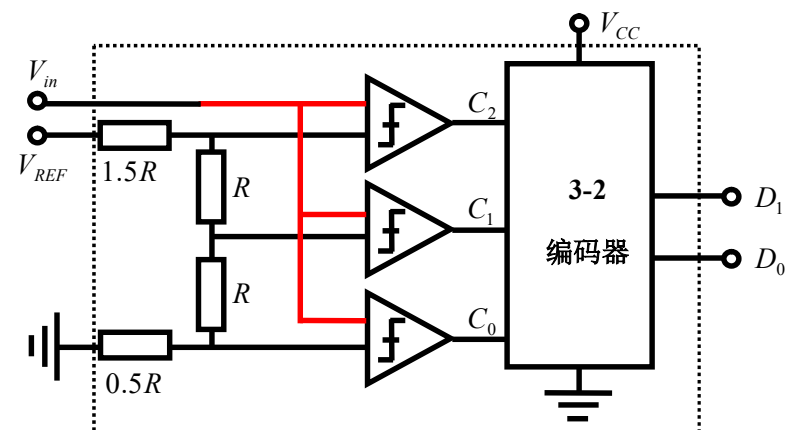
$$V_{REF} \frac{3}{8} < V_{in} < V_{REF} \frac{5}{8}$$



$$V_{in} > V_{REF} \frac{5}{8}$$

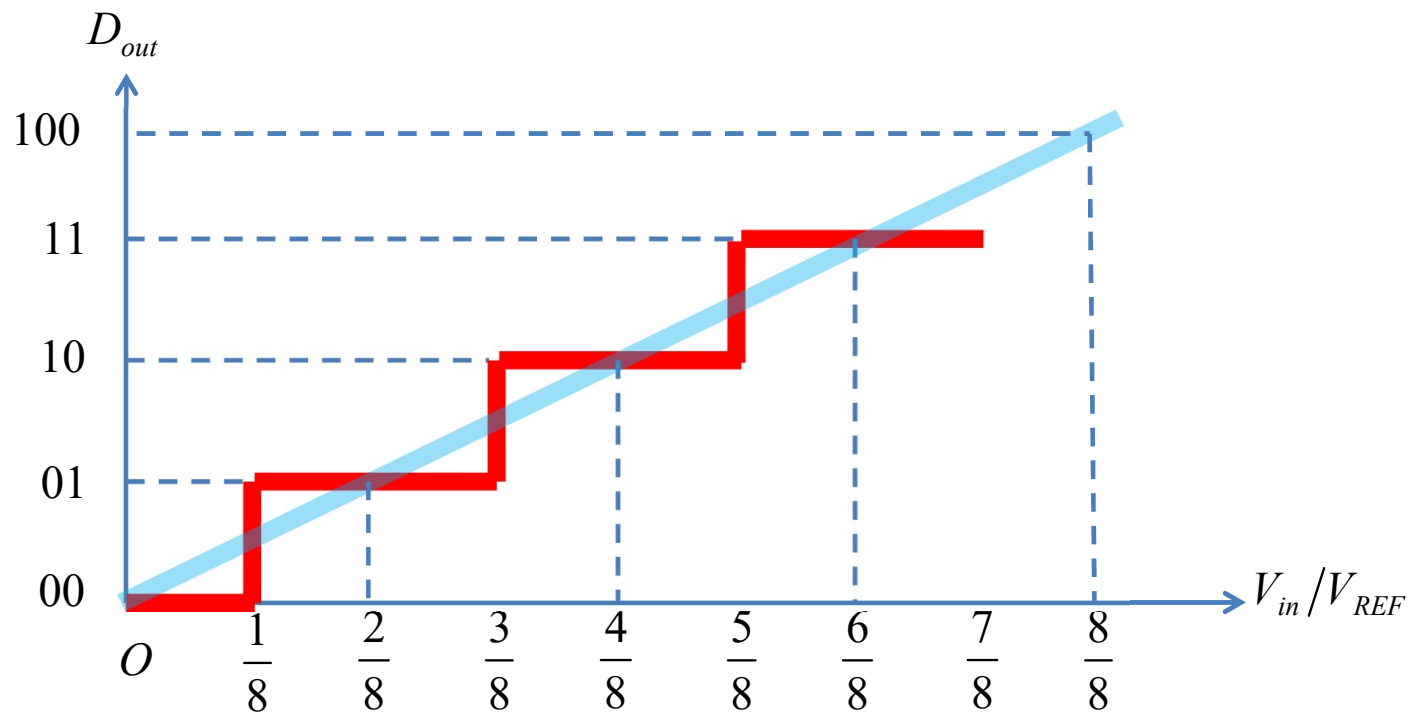


码表



| 模拟输入电压 | $C_2C_1C_0$ | 数字输出码 D_1D_0 |
|--|-------------|----------------|
| $V_{in} < \frac{1}{8}V_{REF}$ | 000 | 00 |
| $\frac{1}{8}V_{REF} < V_{in} < \frac{3}{8}V_{REF}$ | 001 | 01 |
| $\frac{3}{8}V_{REF} < V_{in} < \frac{5}{8}V_{REF}$ | 011 | 10 |
| $V_{in} > \frac{5}{8}V_{REF}$ | 111 | 11 |

转移特性曲线



2bit ADC转移特性曲线

作业5 CMRR

- 假设运放理想，证明：
- 回答：要想获得**80dB的CMRR**，对外部电阻精度提出什么要求？

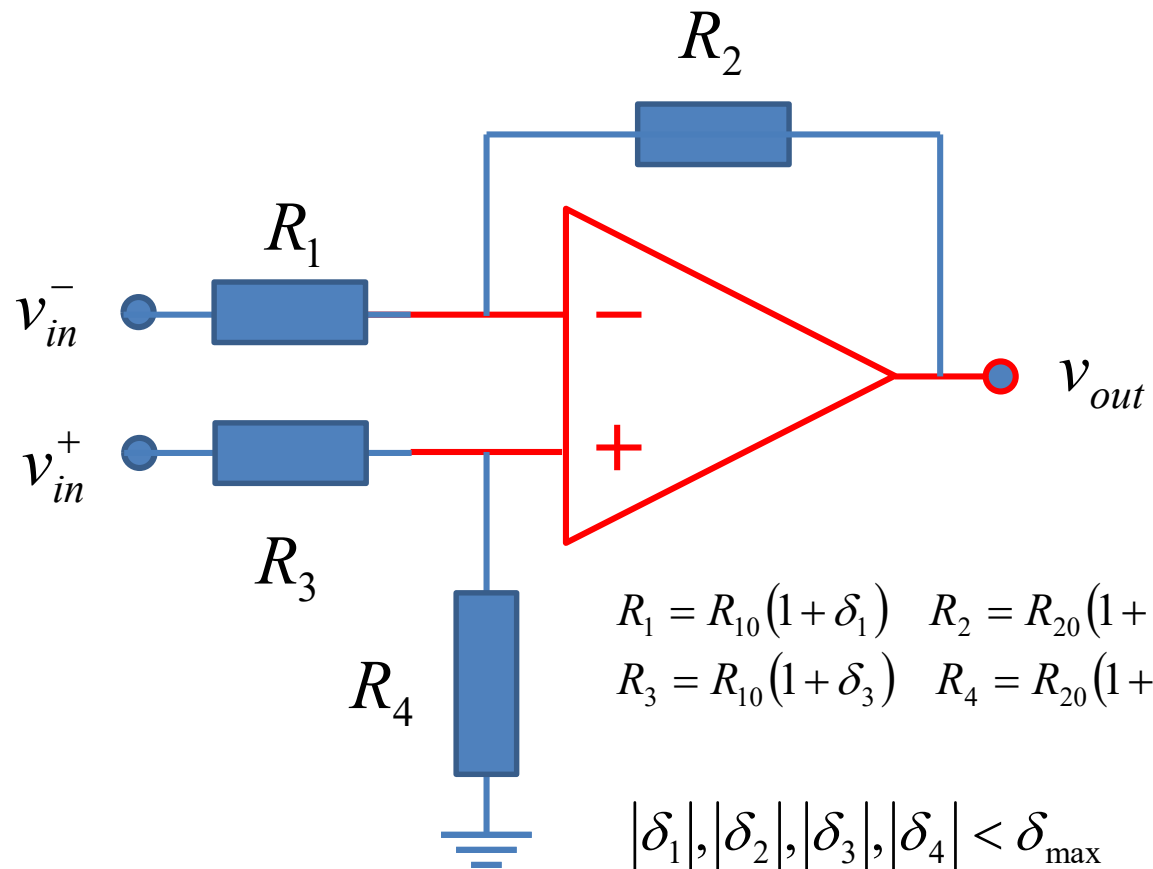
$$CMRR_{\min} = \frac{1}{4\delta_{\max}}$$

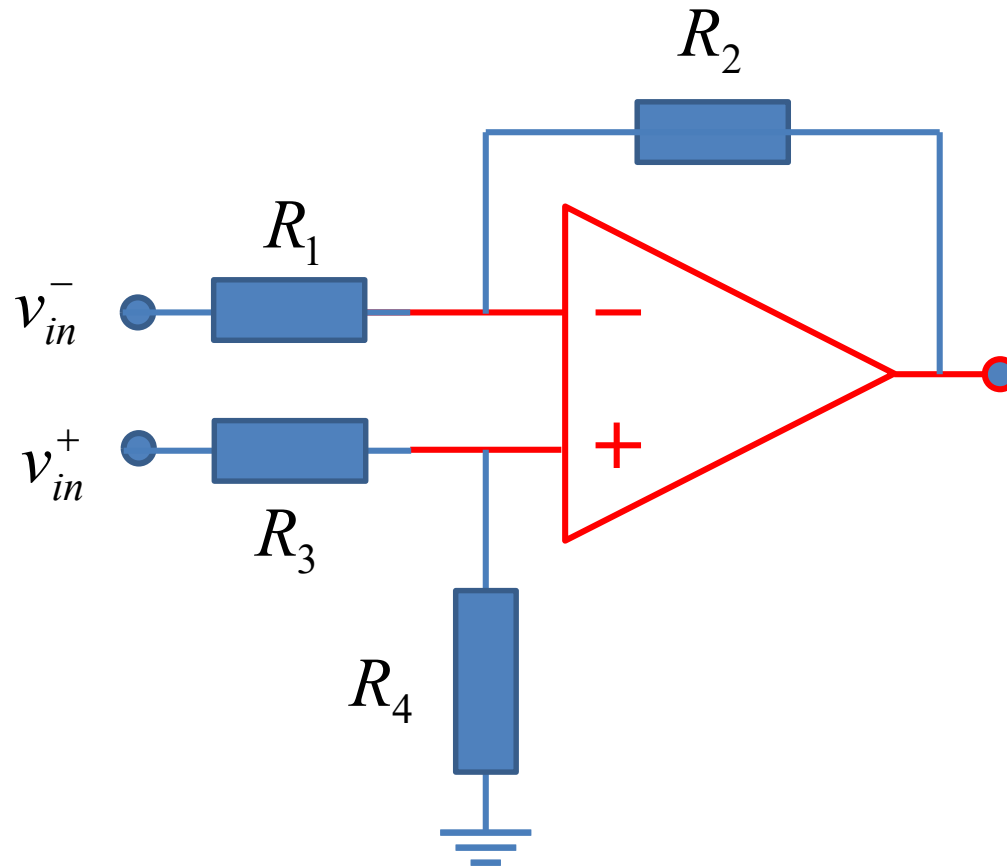
$$v_{in}^+ = v_c + 0.5v_d$$

$$v_{in}^- = v_c - 0.5v_d$$

$$v_{out} = A_{vd}v_d + A_{vc}v_c$$

$$CMRR = \left| \frac{A_{vd}}{A_{vc}} \right|$$





CMRR

$$v_{out} = A_v^- \cdot v_{in}^- + A_v^+ \cdot v_{in}^+$$

$$A_v^- = -\frac{R_2}{R_1}$$

$$A_v^+ = \left(\frac{R_2}{R_1} + 1 \right) \frac{R_4}{R_3 + R_4}$$

$$v_{in}^+ = v_c + 0.5v_d$$

$$v_{in}^- = v_c - 0.5v_d$$

$$R_1 = R_{10}(1 + \delta_1) \quad R_2 = R_{20}(1 + \delta_2)$$

$$R_3 = R_{10}(1 + \delta_3) \quad R_4 = R_{20}(1 + \delta_4)$$

$$CMRR = \left| \frac{A_{vd}}{A_{vc}} \right|$$

$$v_{out} = A_{vd} v_d + A_{vc} v_c$$

先求两个电压增益

$$\begin{aligned}v_{out} &= A_v^- \cdot v_{in}^- + A_v^+ \cdot v_{in}^+ \\&= -\frac{R_2}{R_1}(v_c - 0.5v_d) + \left(\frac{R_2}{R_1} + 1\right) \frac{R_4}{R_3 + R_4}(v_c + 0.5v_d) \\&= \left(\left(\frac{R_2}{R_1} + 1\right) \frac{R_4}{R_3 + R_4} - \frac{R_2}{R_1}\right)v_c + \left(\left(\frac{R_2}{R_1} + 1\right) \frac{R_4}{R_3 + R_4} + \frac{R_2}{R_1}\right)0.5v_d \\&= \left(\frac{R_2 + R_1}{R_1} \frac{R_4}{R_3 + R_4} - \frac{R_2}{R_1}\right)v_c + \left(\frac{R_2 + R_1}{R_1} \frac{R_4}{R_3 + R_4} + \frac{R_2}{R_1}\right)0.5v_d \\&= \left(\frac{R_1R_4 - R_2R_3}{R_1(R_3 + R_4)}\right)v_c + \left(\frac{2R_2R_4 + R_1R_4 + R_2R_3}{R_1(R_3 + R_4)}\right)0.5v_d\end{aligned}$$

$$CMRR = \left| \frac{A_{vd}}{A_{vc}} \right| = \left| 0.5 \frac{2R_2R_4 + R_1R_4 + R_2R_3}{R_1R_4 - R_2R_3} \right| = \dots$$

留大弃小

$$\begin{aligned}
 CMRR &= \left| \frac{A_{vd}}{A_{vc}} \right| = \left| 0.5 \frac{2R_2R_4 + R_1R_4 + R_2R_3}{R_1R_4 - R_2R_3} \right| \\
 &= \left| 0.5 \frac{2R_{20}(1+\delta_2)R_{20}(1+\delta_4) + R_{10}(1+\delta_1)R_{20}(1+\delta_4) + R_{20}(1+\delta_2)R_{10}(1+\delta_3)}{R_{10}(1+\delta_1)R_{20}(1+\delta_4) - R_{20}(1+\delta_2)R_{10}(1+\delta_3)} \right| \\
 &= 0.5 \left| \frac{2 \frac{R_{20}}{R_{10}} (1+\delta_2)(1+\delta_4) + (1+\delta_1)(1+\delta_4) + (1+\delta_2)(1+\delta_3)}{(1+\delta_1)(1+\delta_4) - (1+\delta_2)(1+\delta_3)} \right| \\
 &= 0.5 \left| \frac{2 \frac{R_{20}}{R_{10}} (1+\delta_2 + \delta_4 + \delta_2\delta_4) + (1+\delta_1 + \delta_4 + \delta_1\delta_4) + (1+\delta_2 + \delta_3 + \delta_2\delta_3)}{(1+\delta_1 + \delta_4 + \delta_1\delta_4) - (1+\delta_2 + \delta_3 + \delta_2\delta_3)} \right| \\
 &\approx 0.5 \left| \frac{2 \frac{R_{20}}{R_{10}} + 2}{\delta_1 + \delta_4 - \delta_2 - \delta_3} \right| = \left| \frac{\frac{R_{20}}{R_{10}} + 1}{\delta_1 + \delta_4 - \delta_2 - \delta_3} \right| \geq \left| \frac{1}{\delta_1 + \delta_4 - \delta_2 - \delta_3} \right| \geq \frac{1}{4\delta_{\max}} = CMRR_{\min}
 \end{aligned}$$

高精度意味着高成本

$$CMRR = \left| \frac{A_{vd}}{A_{vc}} \right| \approx \frac{R_{10} + R_{20}}{R_{10}} \frac{1}{|\delta_4 - \delta_2 + \delta_1 - \delta_3|} \geq \frac{1}{4\delta_{\max}} = CMRR_{\min}$$

$$CMRR \geq 80dB$$

$$CMRR_{\min} \geq 80dB$$

$$20 \log \frac{1}{4\delta_{\max}} \geq 80dB$$

$$\frac{1}{4\delta_{\max}} \geq 10^4$$

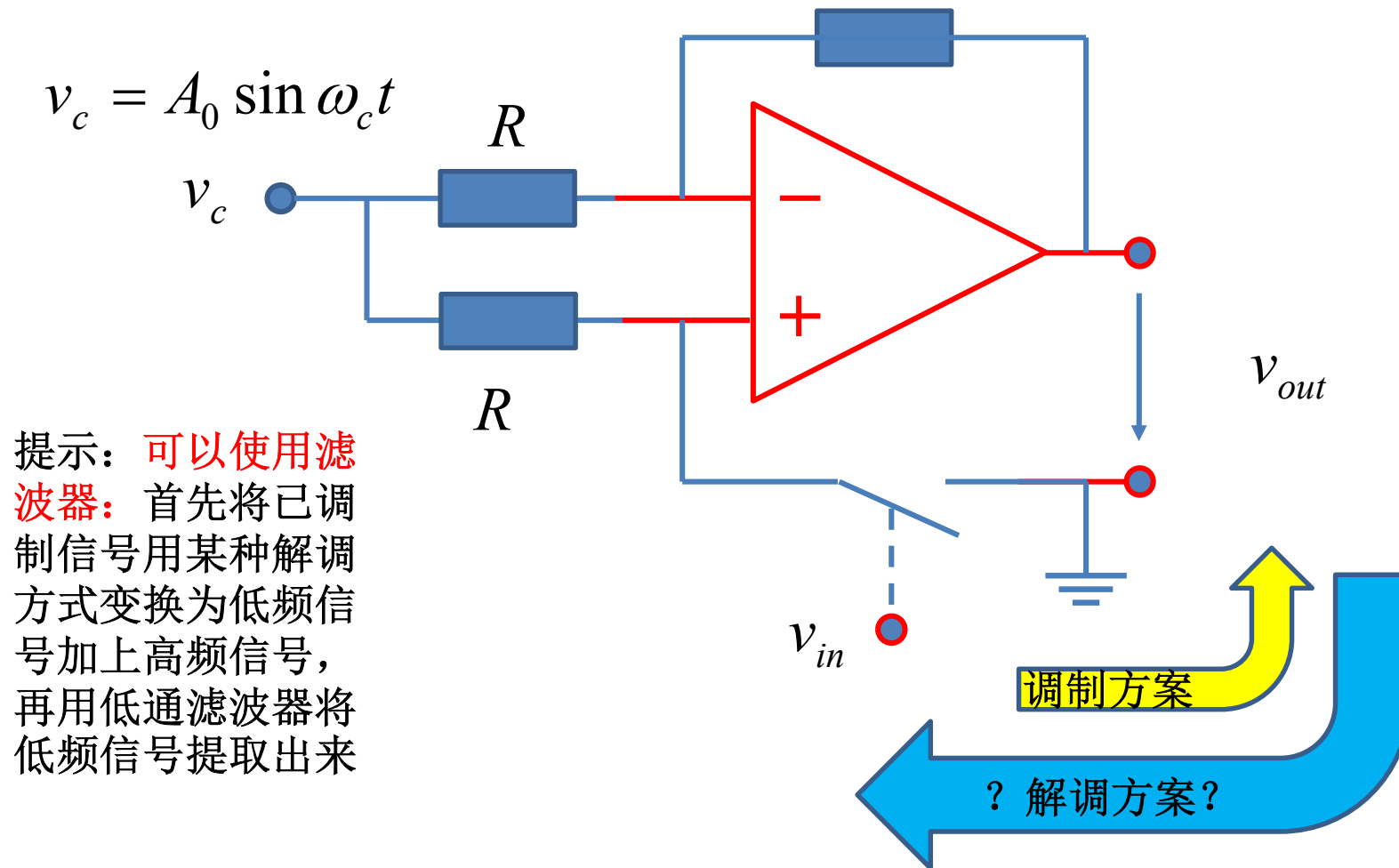
$$\delta_{\max} \leq \frac{1}{4 \times 10^4} = 2.5 \times 10^{-5} = 0.25\%\%$$

极高的精度要求，成本将会急剧提高

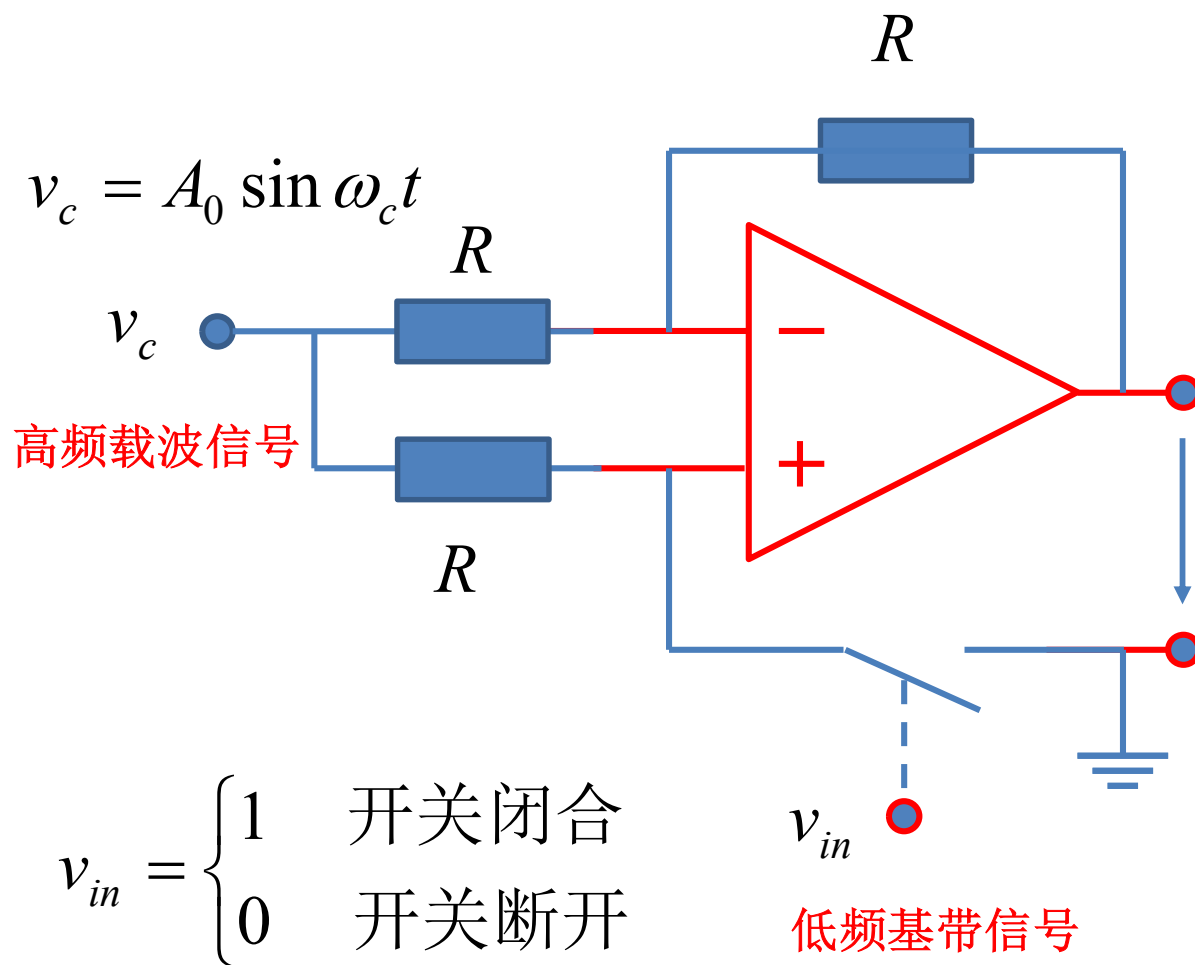
作业6 解调方案

- 给出你的解调方案，画出电路图或原理方框图。

$$v_c = A_0 \sin \omega_c t$$



简单调制电路



低频基带信号被调制到高频载波信号的幅度或相位上：信息装载到载波的幅度或相位上

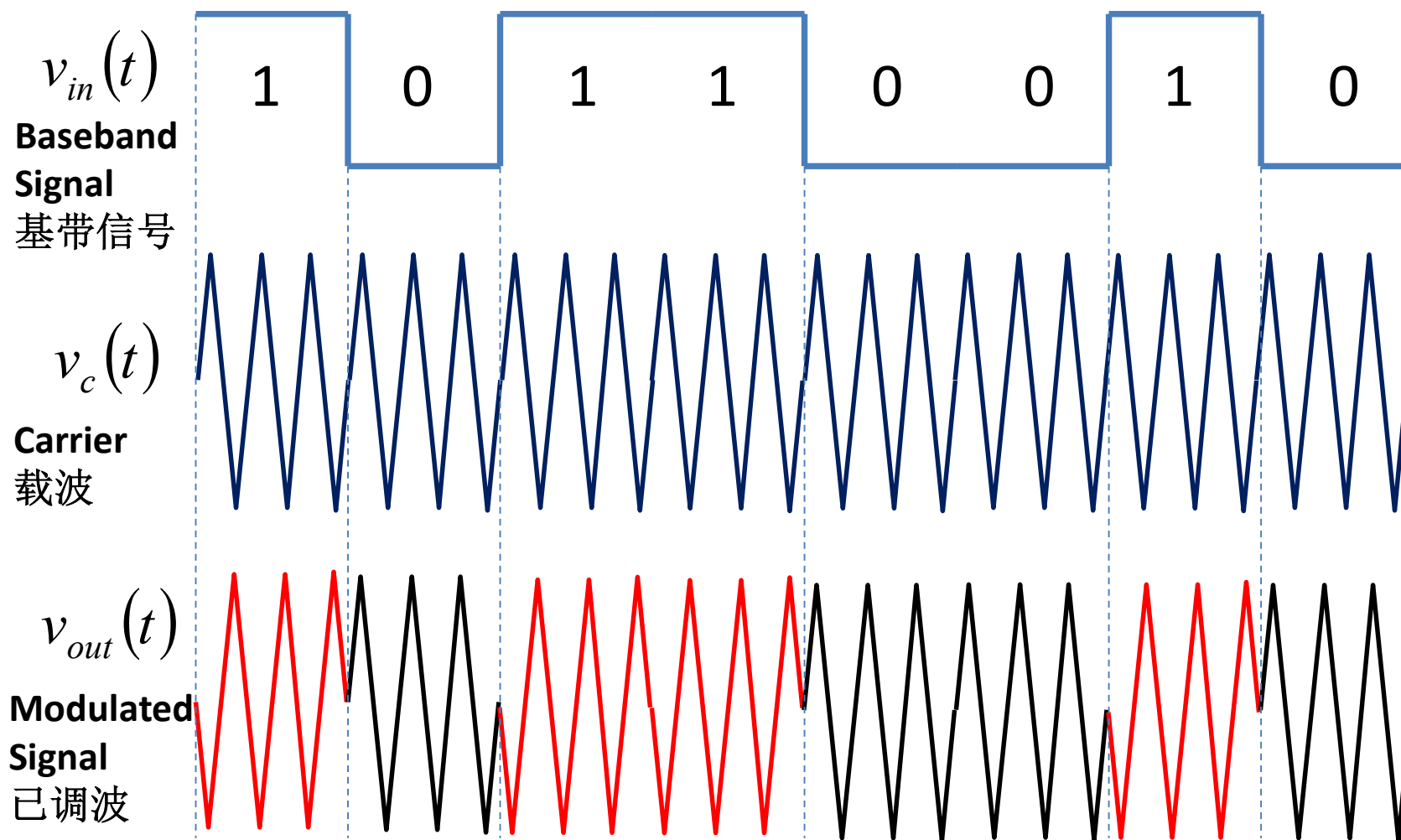
$$v_{out} = \begin{cases} -v_c & v_{in} = 1 \\ +v_c & v_{in} = 0 \end{cases}$$

$$= (1 - 2v_{in}) \cdot A_0 \sin \omega_c t$$

$$= A_0 \sin(\omega_c t + v_{in} \cdot \pi)$$

已调波波形

$$v_{out} = \begin{cases} -v_c & v_{in} = 1 \\ +v_c & v_{in} = 0 \end{cases} = (1 - 2v_{in}) \cdot A_0 \sin \omega_c t = A_0 \sin(\omega_c t + v_{in} \cdot \pi)$$



解调原理： 乘以载波信号

$$v_{out}(t) = (1 - 2v_{in}(t)) \cdot A_0 \sin(\omega_c t + \varphi_e) \quad \text{幅度调制}$$

$$v_{out}(t) \cdot v'_c(t) = (1 - 2v_{in}(t)) \cdot A_0 \sin \omega_c t \cdot A_1 \sin(\omega_c t + \varphi_e)$$

$$= (1 - 2v_{in}(t)) \cdot A_0 A_1 \sin \omega_c t \cdot \sin(\omega_c t + \varphi_e)$$

$$= (1 - 2v_{in}(t)) \cdot A_0 A_1 \frac{\cos \varphi_e - \cos(2\omega_c t + \varphi_e)}{2} \quad \text{幅度解调}$$

$$= \frac{A_0 A_1}{2} (1 - 2v_{in}(t)) (\cos \varphi_e - \cos(2\omega_c t + \varphi_e))$$

$$= \frac{A_0 A_1}{2} \cos \varphi_e (1 - 2v_{in}(t)) - \frac{A_0 A_1}{2} (1 - 2v_{in}(t)) \cos(2\omega_c t + \varphi_e)$$

$$v_d(t) = f_{Lowpassfilter}(v_{out}(t) \cdot v'_c(t)) \quad \text{低通滤波}$$

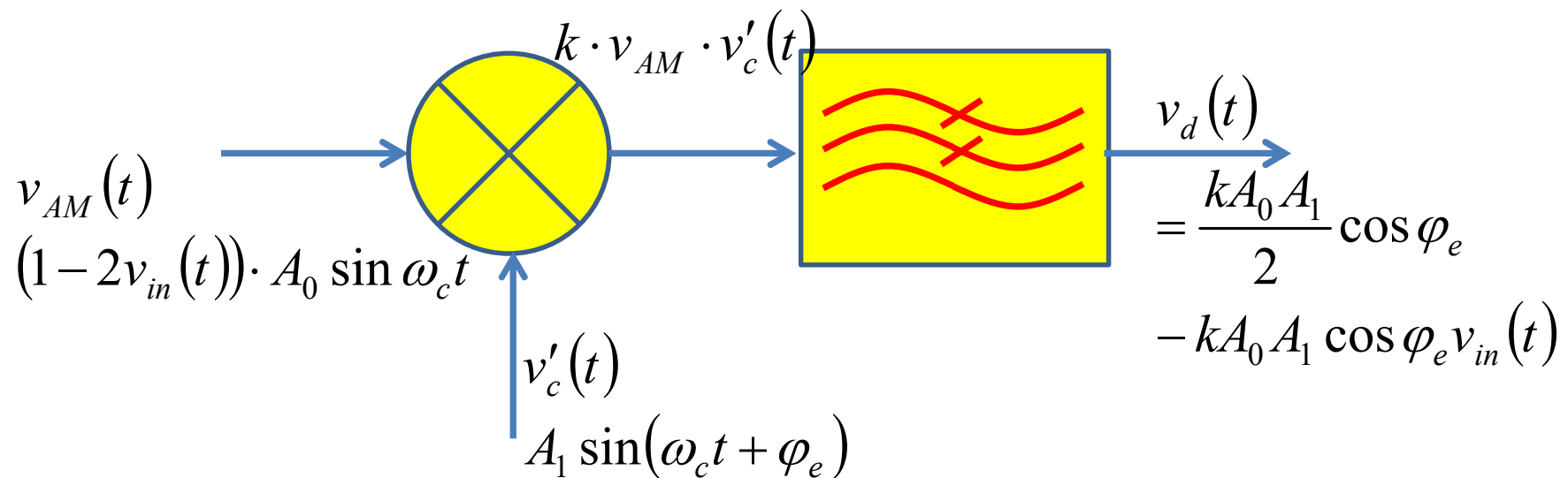
$$= f_{Lowpassfilter} \left(\frac{A_0 A_1}{2} \cos \varphi_e (1 - 2v_{in}(t)) - \frac{A_0 A_1}{2} (1 - 2v_{in}(t)) \cos(2\omega_c t + \varphi_e) \right)$$

$$= \frac{A_0 A_1}{2} \cos \varphi_e (1 - 2v_{in}(t - \tau_0)) = \frac{A_0 A_1}{2} \cos \varphi_e - A_0 A_1 \cos \varphi_e v_{in}(t - \tau_0)$$

低通滤波器引入的延时
空间传输也会引入延时

理想传输、理想
滤波无失真

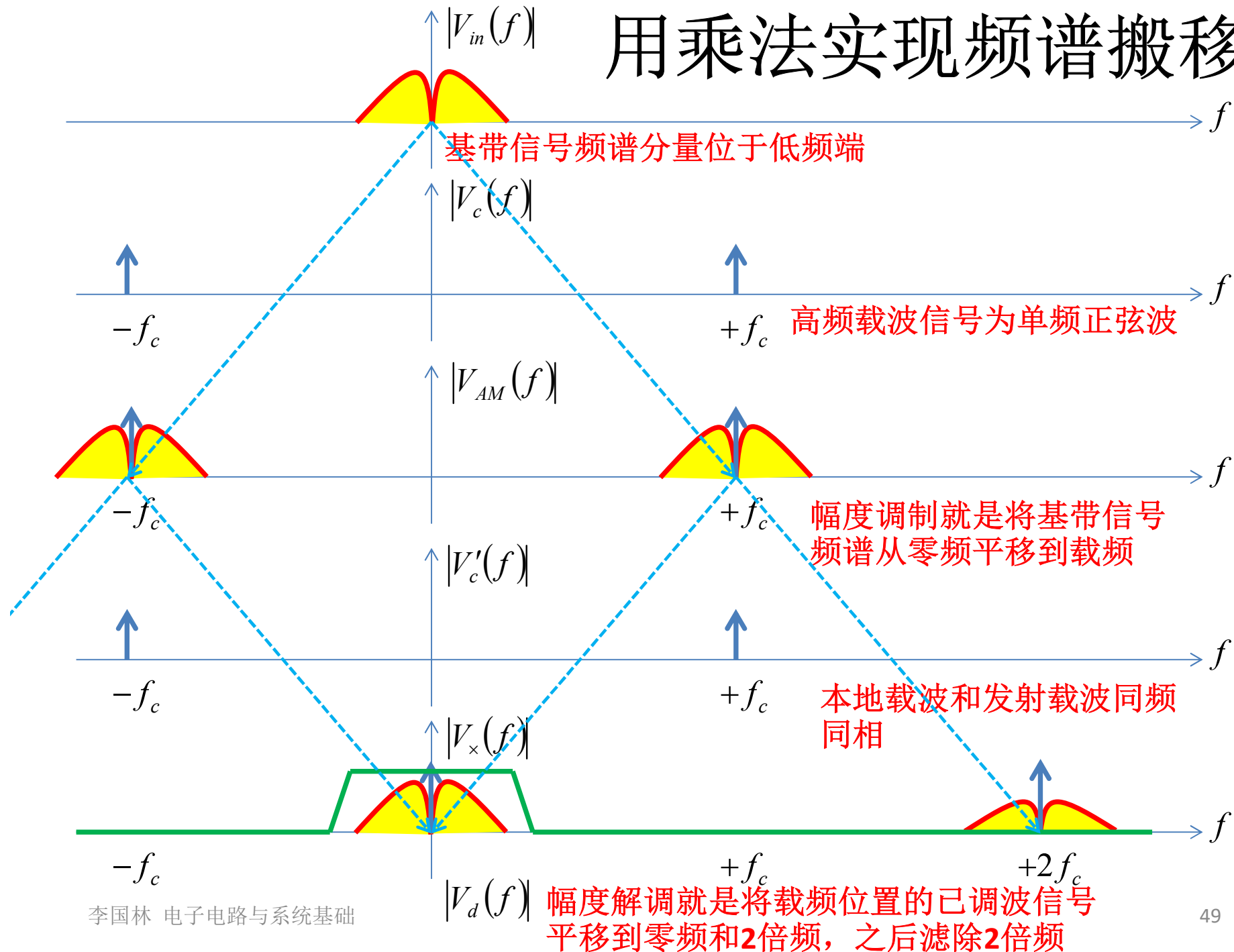
幅度解调器原理性方案



同频同相本地载波的产生是解调的关键技术

《通信电路》课程讨论锁相环技术，可实现同频同相本地载波的产生

用乘法实现频谱搬移



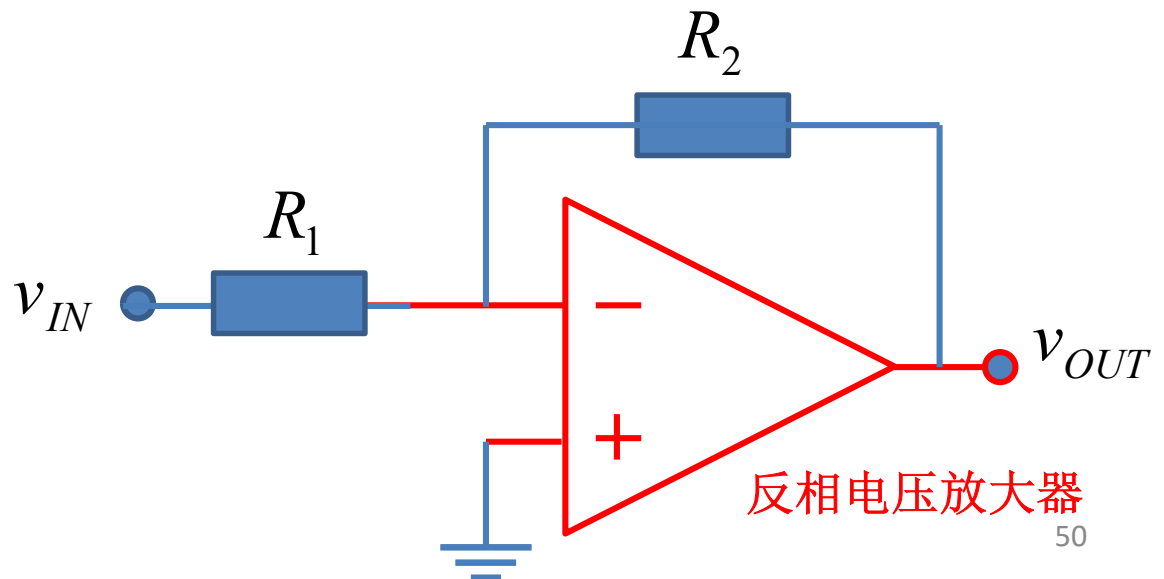
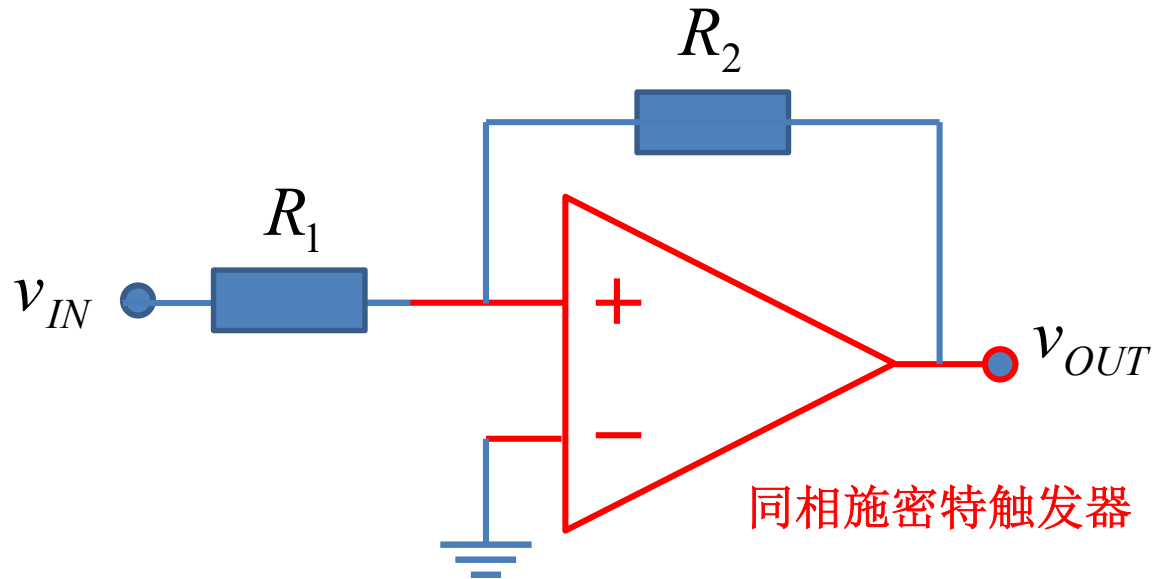
作业7 同相施密特触发器

- 分析并画出如下滞回比较器的输入输出转移特性曲线（滞回曲线分析）

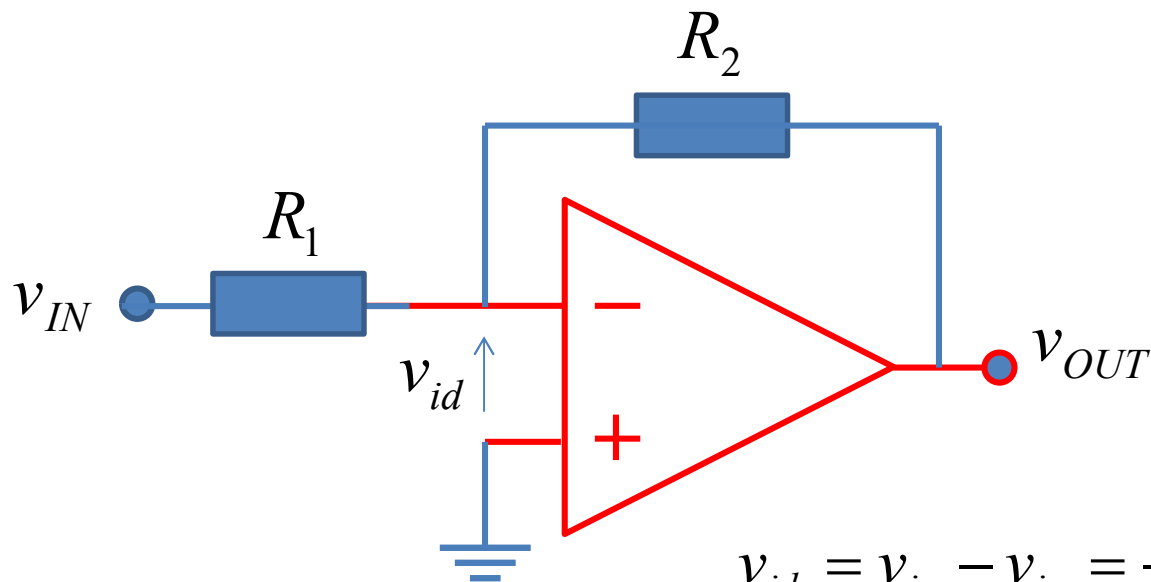
- 和课堂上讲述的反相施密特触发器的滞回曲线比较，两者差别在哪里？

- 用图解法分析其转移特性曲线和反相电压放大器的区别

- 课堂上讨论了反相施密特触发器与同相电压放大器的图解法



反相电压放大器外围电路分析



$$v_{id} = v_{ip} - v_{in} = -\frac{R_2}{R_1 + R_2} v_{IN} - \frac{R_1}{R_1 + R_2} v_{OUT}$$

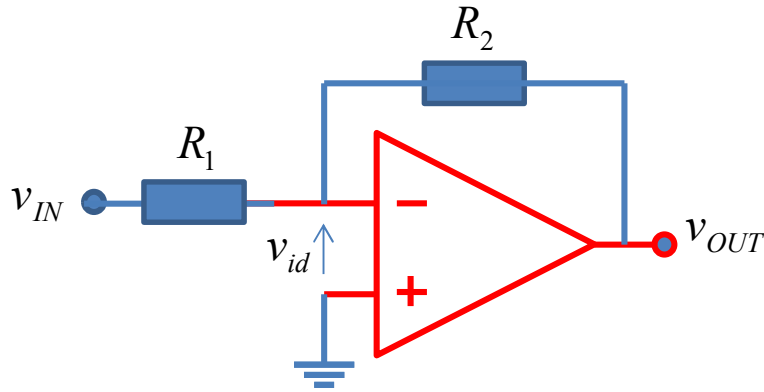
$$v_{ip} = 0$$

$$v_{in} = \frac{R_2}{R_1 + R_2} v_{IN} + \frac{R_1}{R_1 + R_2} v_{OUT}$$

$$v_{OUT} = -\frac{R_2}{R_1} v_{IN} - \frac{R_1 + R_2}{R_1} v_{id}$$

外加激励源形成一系列关系
对运放电路而言，这是负反馈关系

反相放大器输入输出转移特性曲线

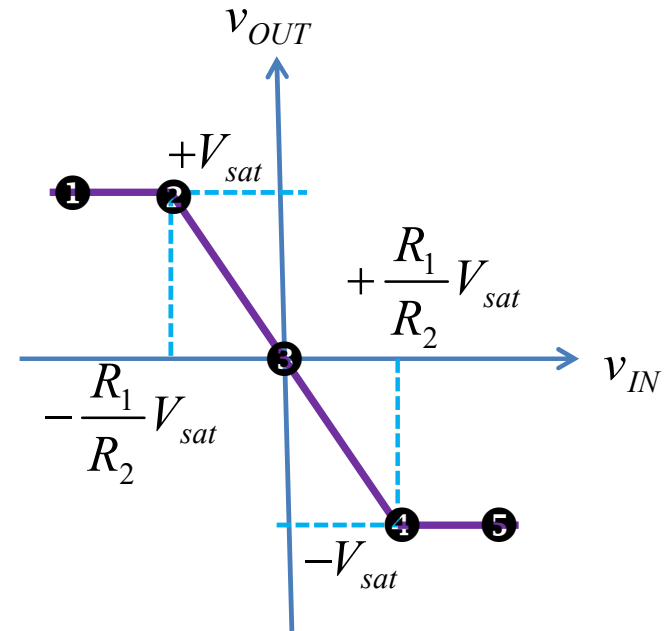
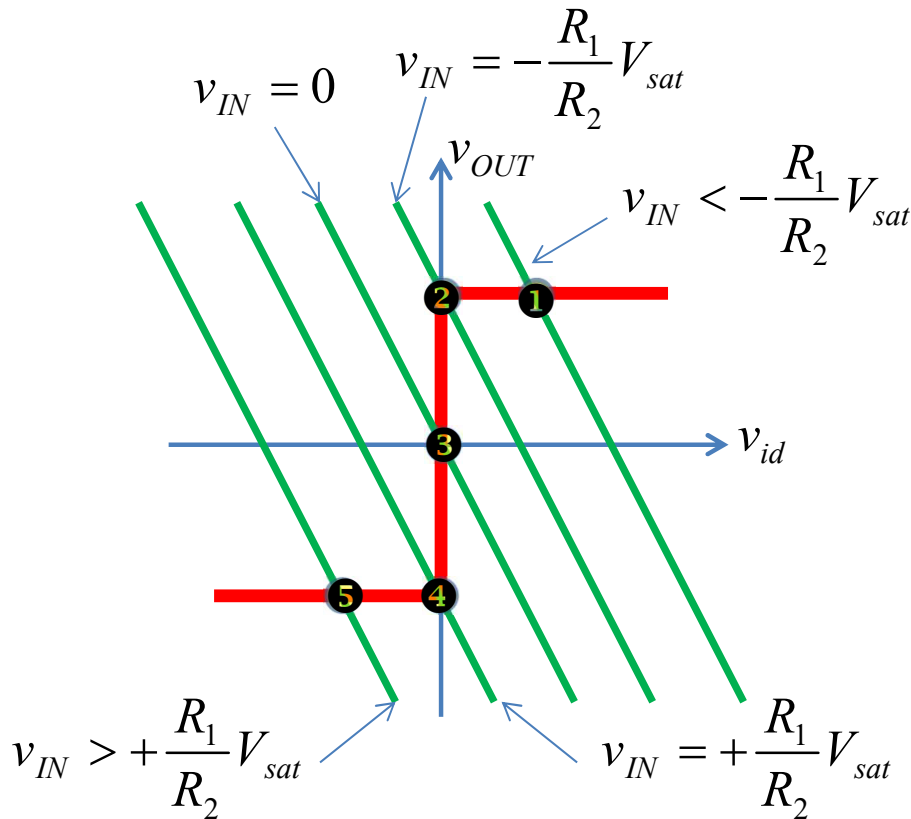


$$v_{OUT} = -\frac{R_2}{R_1} v_{IN} - \frac{R_1 + R_2}{R_1} v_{id}$$

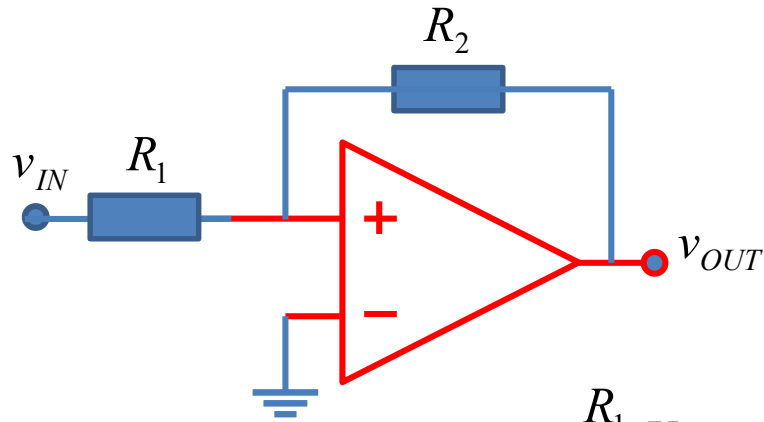
运放外围器件关系

$$v_{OUT} = f(v_{id})$$

运放自身关系



同相施密特触发器转移特性曲线



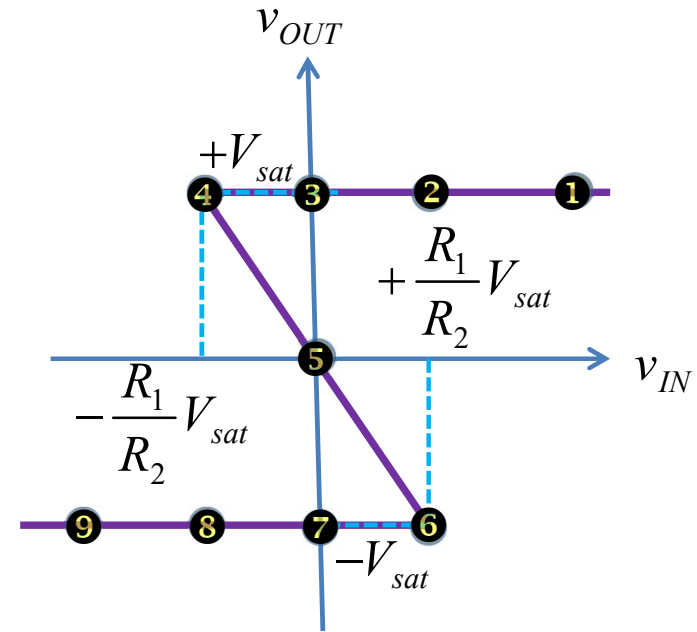
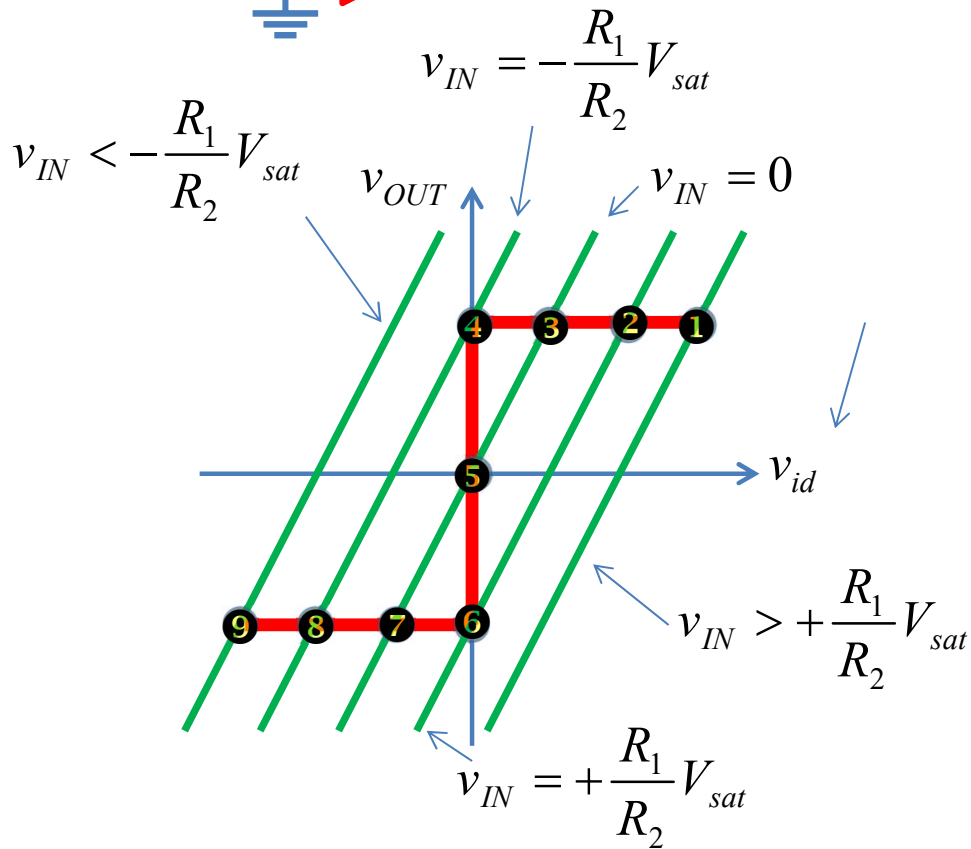
$$v_{OUT} = -\frac{R_2}{R_1} v_{IN} + \frac{R_1 + R_2}{R_1} v_{id}$$

运放外围器件关系

$$v_{OUT} = f(v_{id})$$

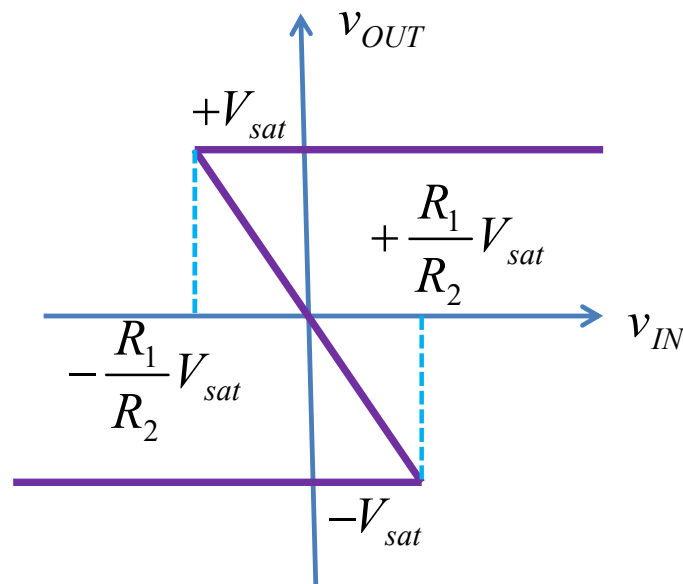
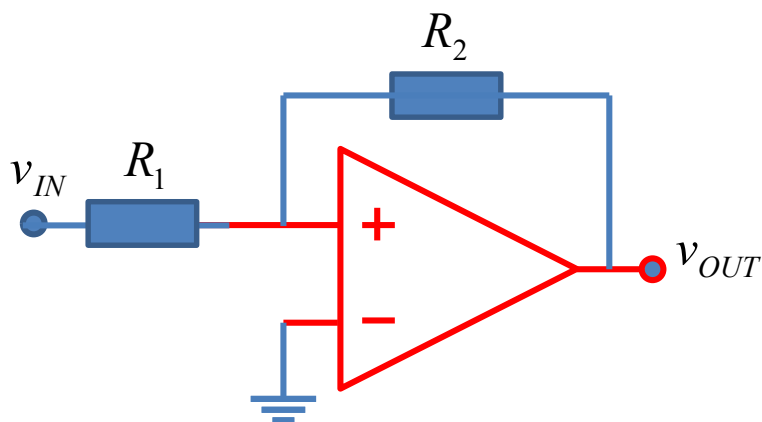
正反馈的表现

运放自身关系



同相滞回曲线

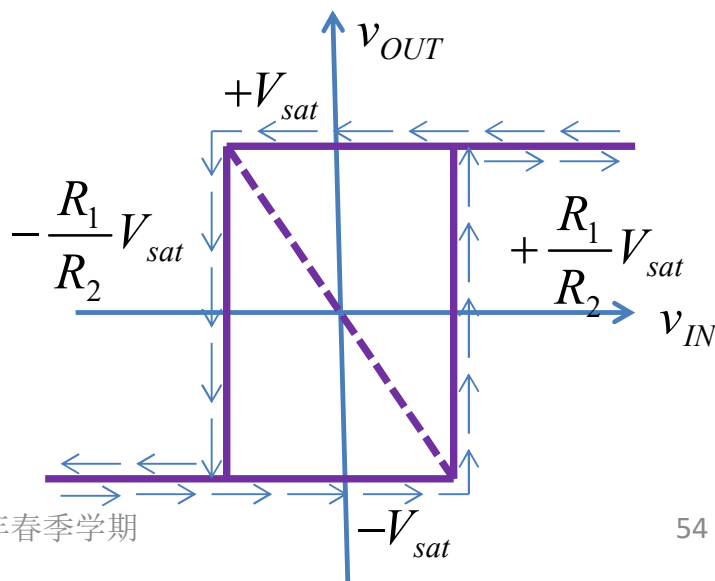
$$v_{ip} = \frac{R_2}{R_1 + R_2} v_{IN} + \frac{R_1}{R_1 + R_2} v_{OUT}$$



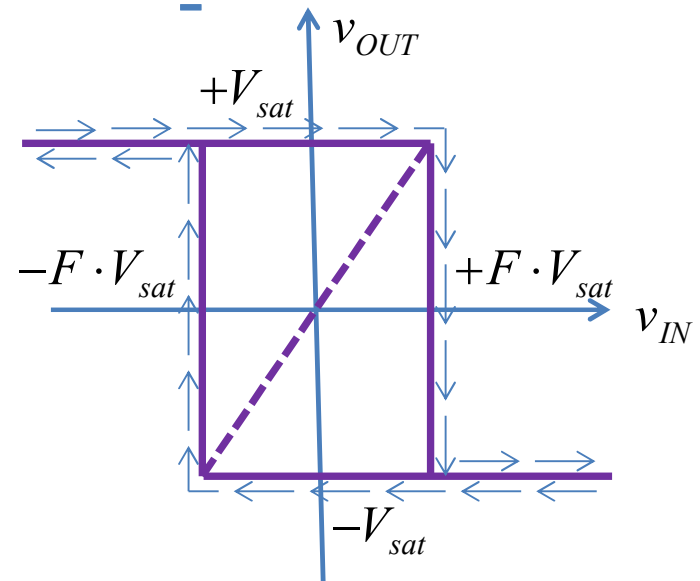
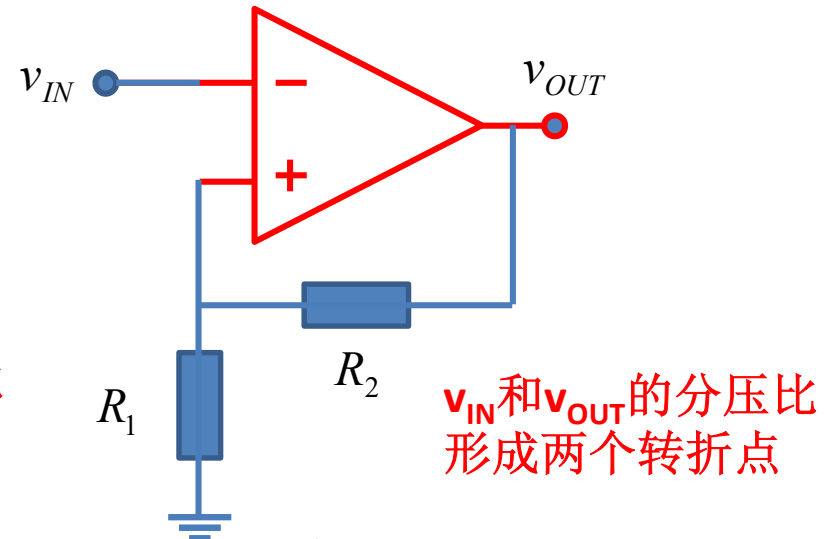
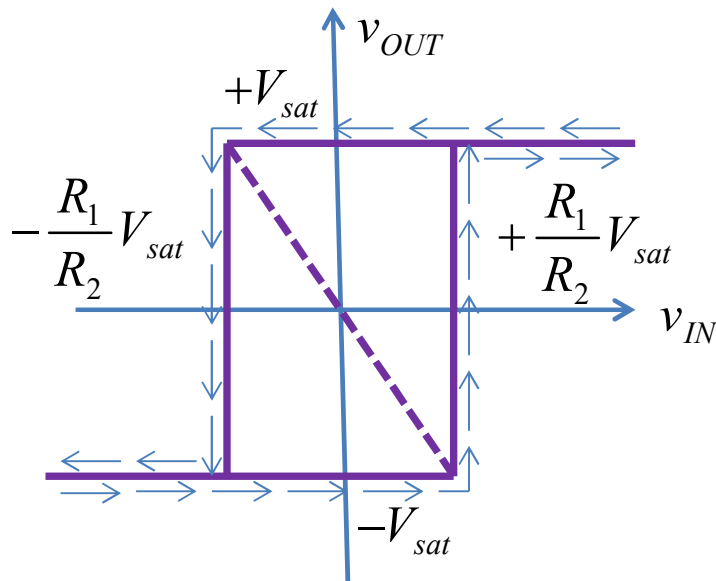
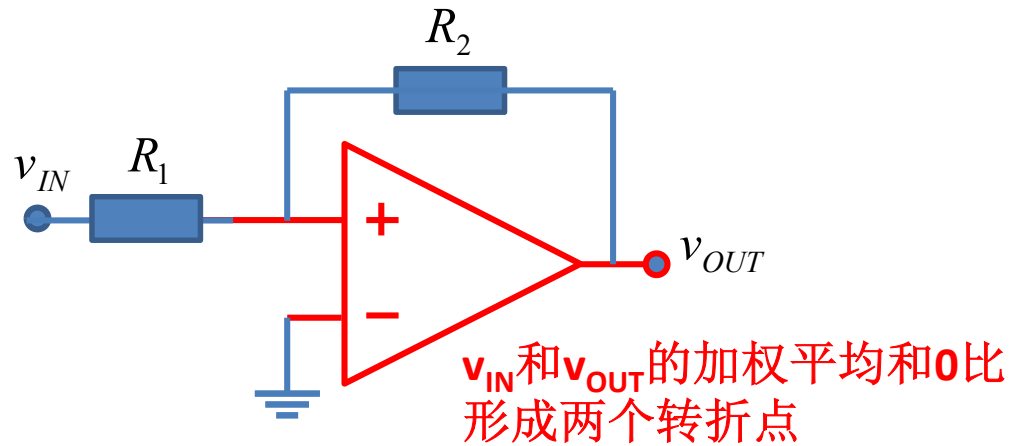
数学上的理论转移特性曲线
中间为不稳定区，实际工作点无法稳定平衡
实测为正相滞回转移特性曲线

正反馈导致多个工作点
一个不稳定工作点，待不住
两个稳定工作点，具有记忆能力
到底在哪个稳定工作点，由之前的经历决定

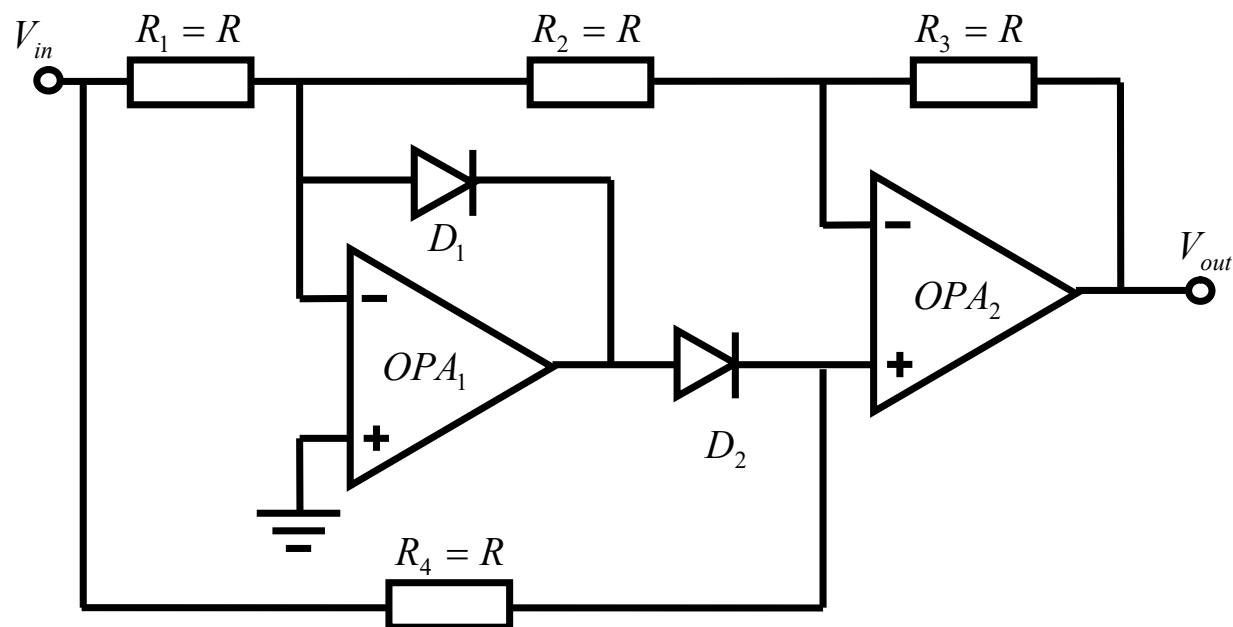
负阻具有多个工作点
施密特触发器可形成负阻



同相滞回曲线和反相滞回曲线

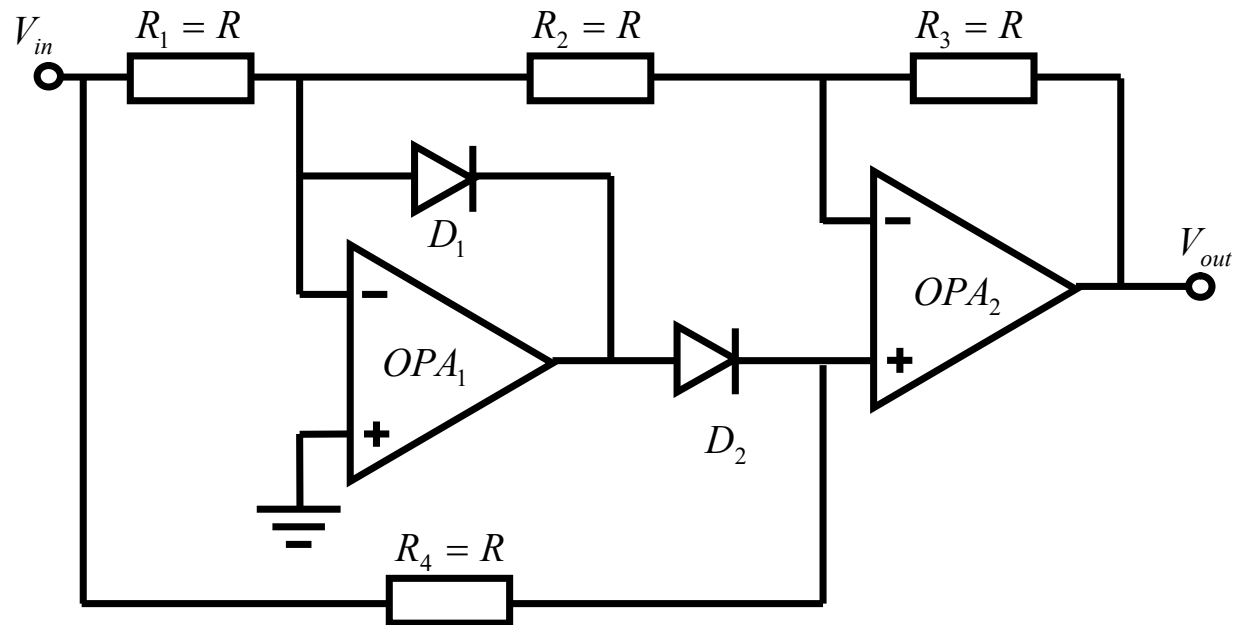


作业8 双运放非线性应用



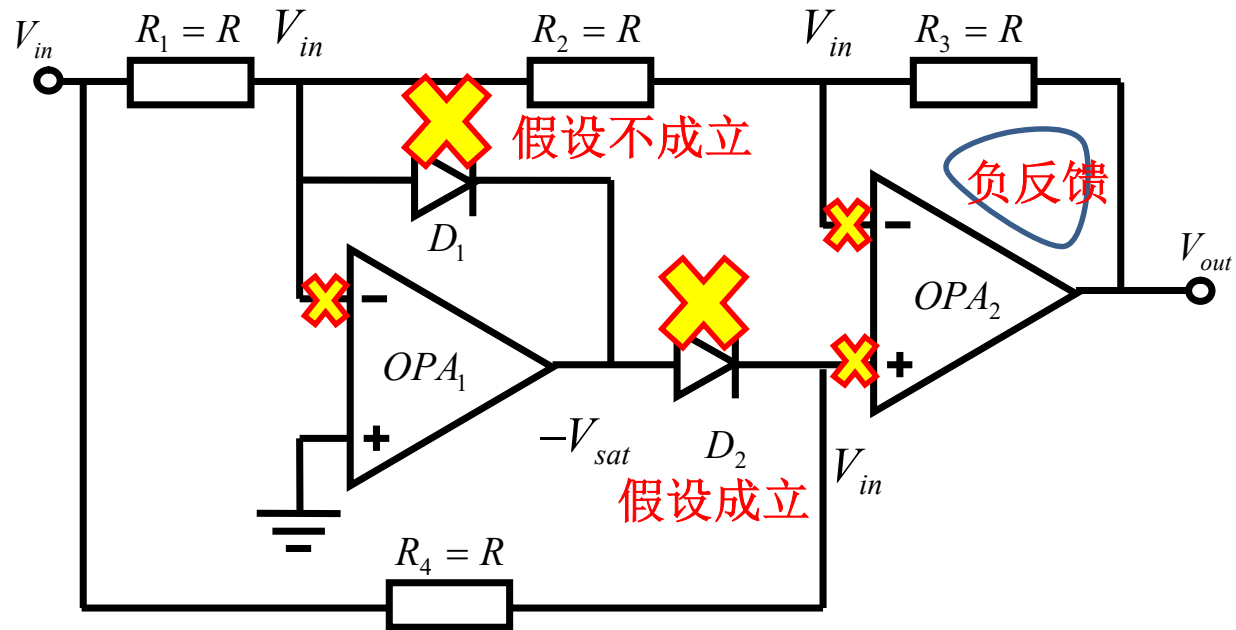
- 分析这个双运放二极管电路实现了什么电路功能？
 - 画出输入输出转移特性曲线
 - 如果输入为正弦波，输出为什么波形？

二极管抽象为两个状态：导通或截止

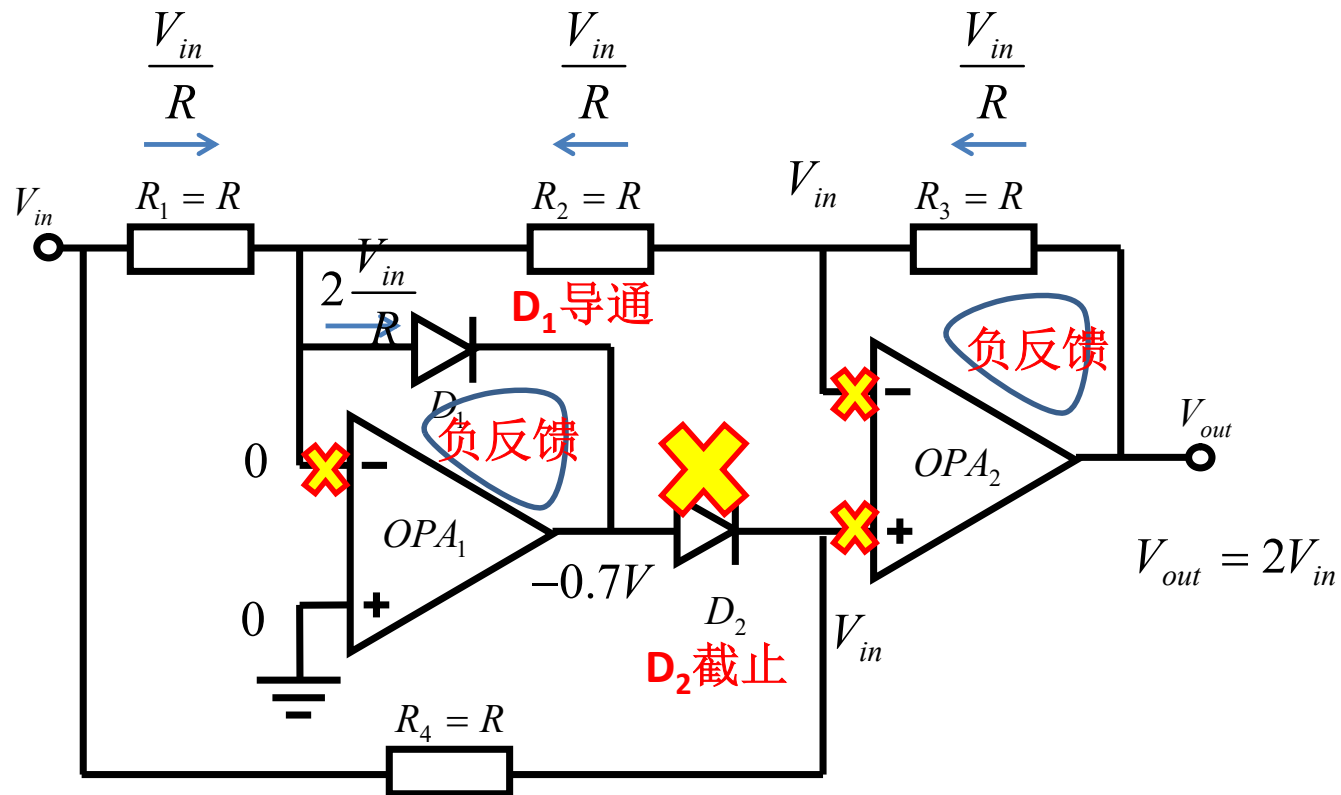


假设二极管工作在截止区，分析电路工作状态，如果二极管外围电路确实满足二极管截止条件 ($v_D < 0.7V, i_D = 0$)，则假设成立，如果二极管外围电路不满足二极管截止条件 ($v_D > 0.7V$)，假设则不成立，需要重新假定二极管工作在导通区 ($v_D = 0.7V, i_D > 0$)，分析结果符合则分析结束

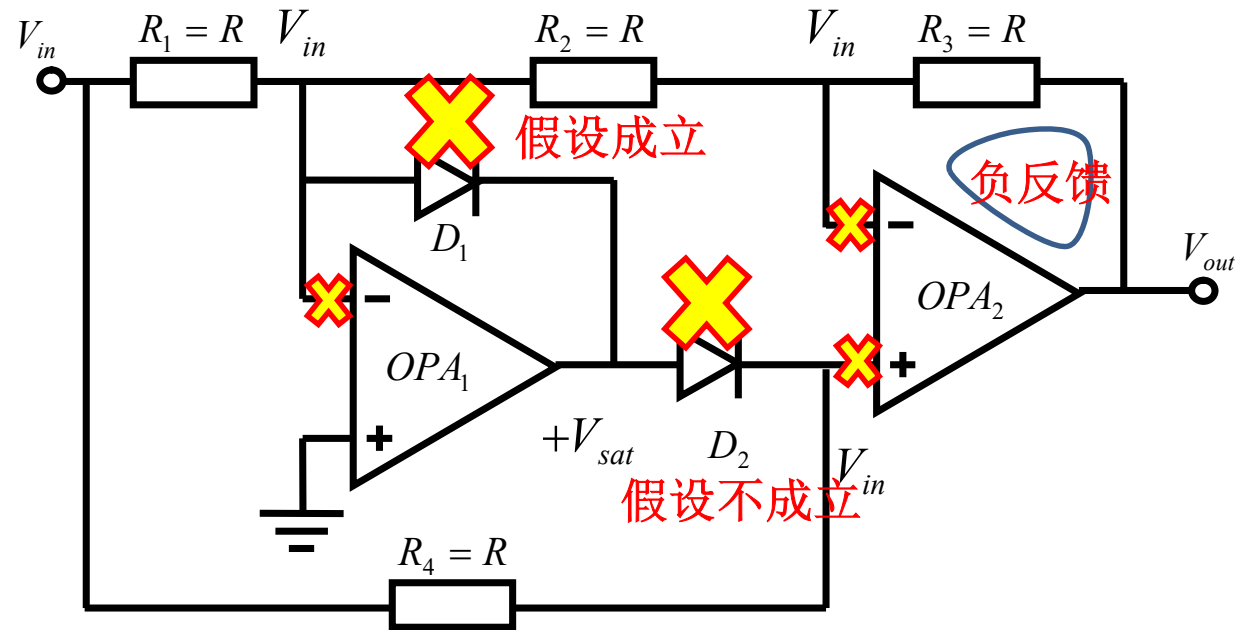
$V_{in} > 0$: 假设二极管截止



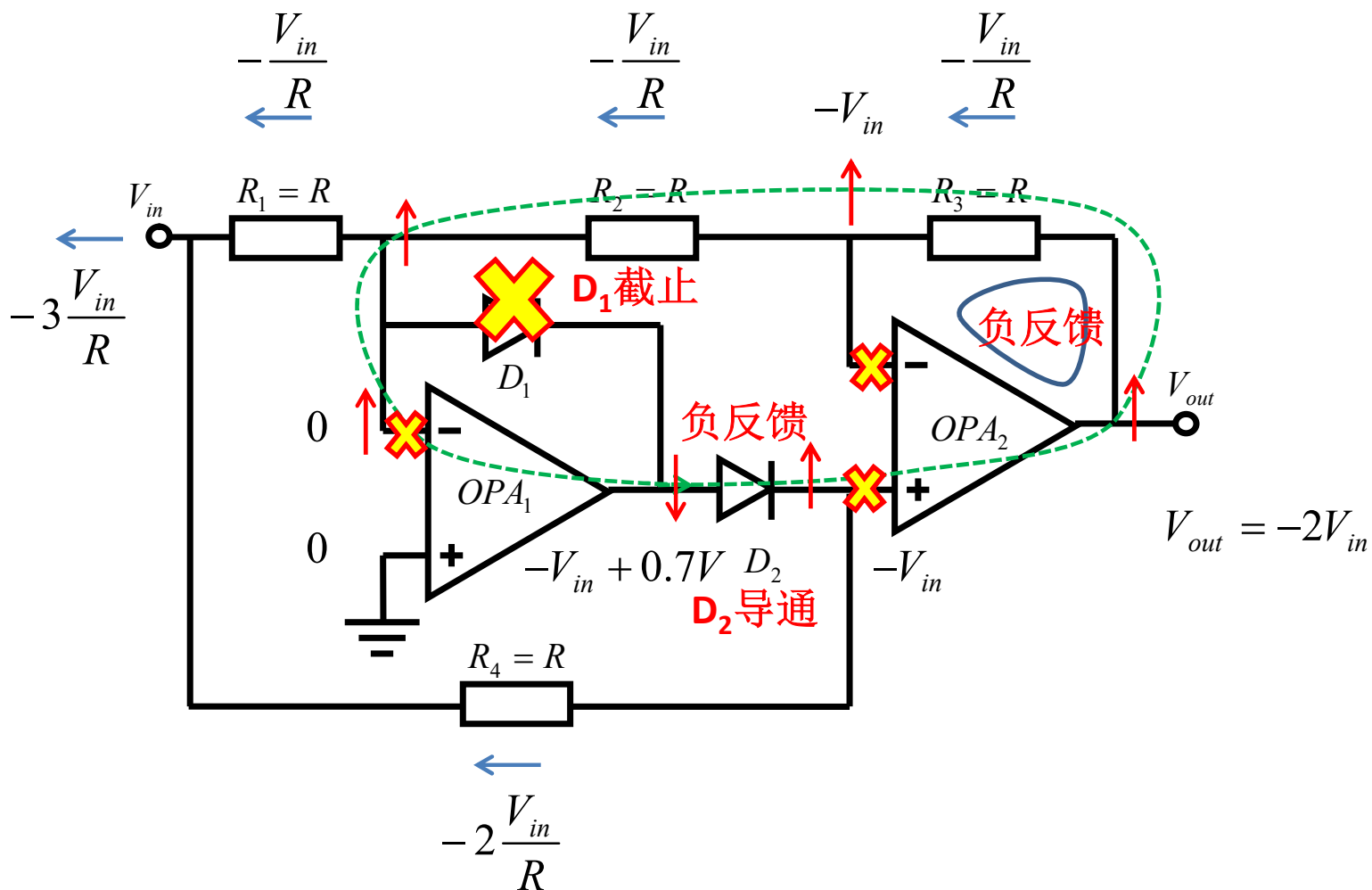
$V_{in} > 0$: D_1 导通, D_2 截止



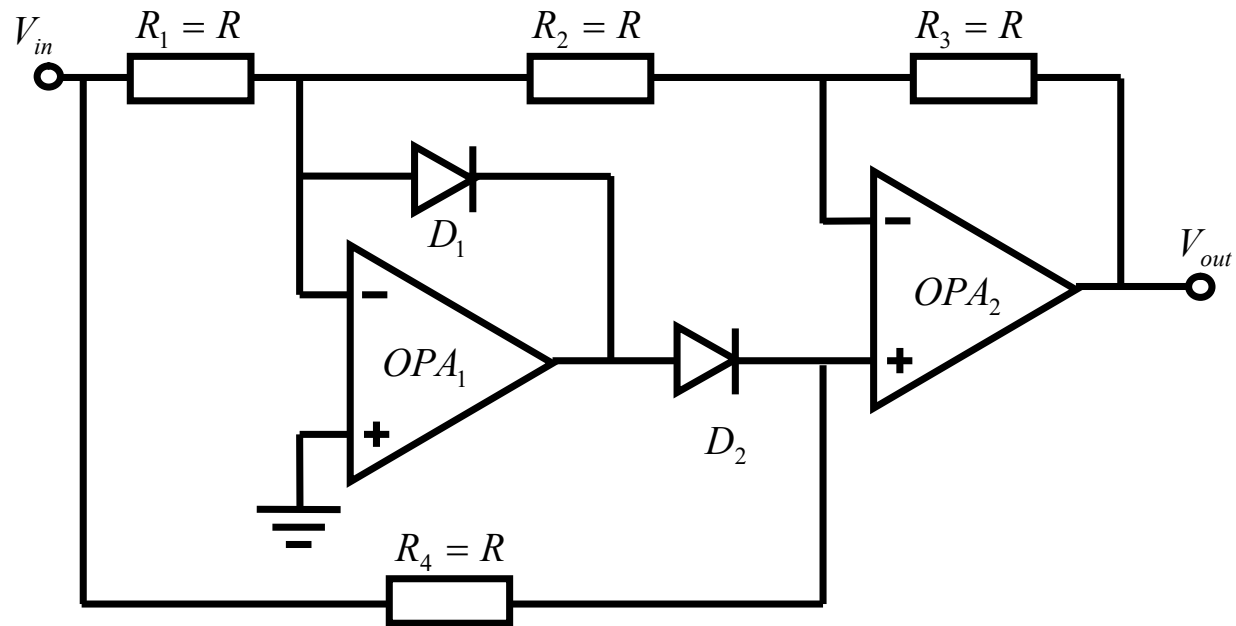
$V_{in} < 0$: 假设二极管截止



$V_{in} < 0$: D_1 截止, D_2 导通

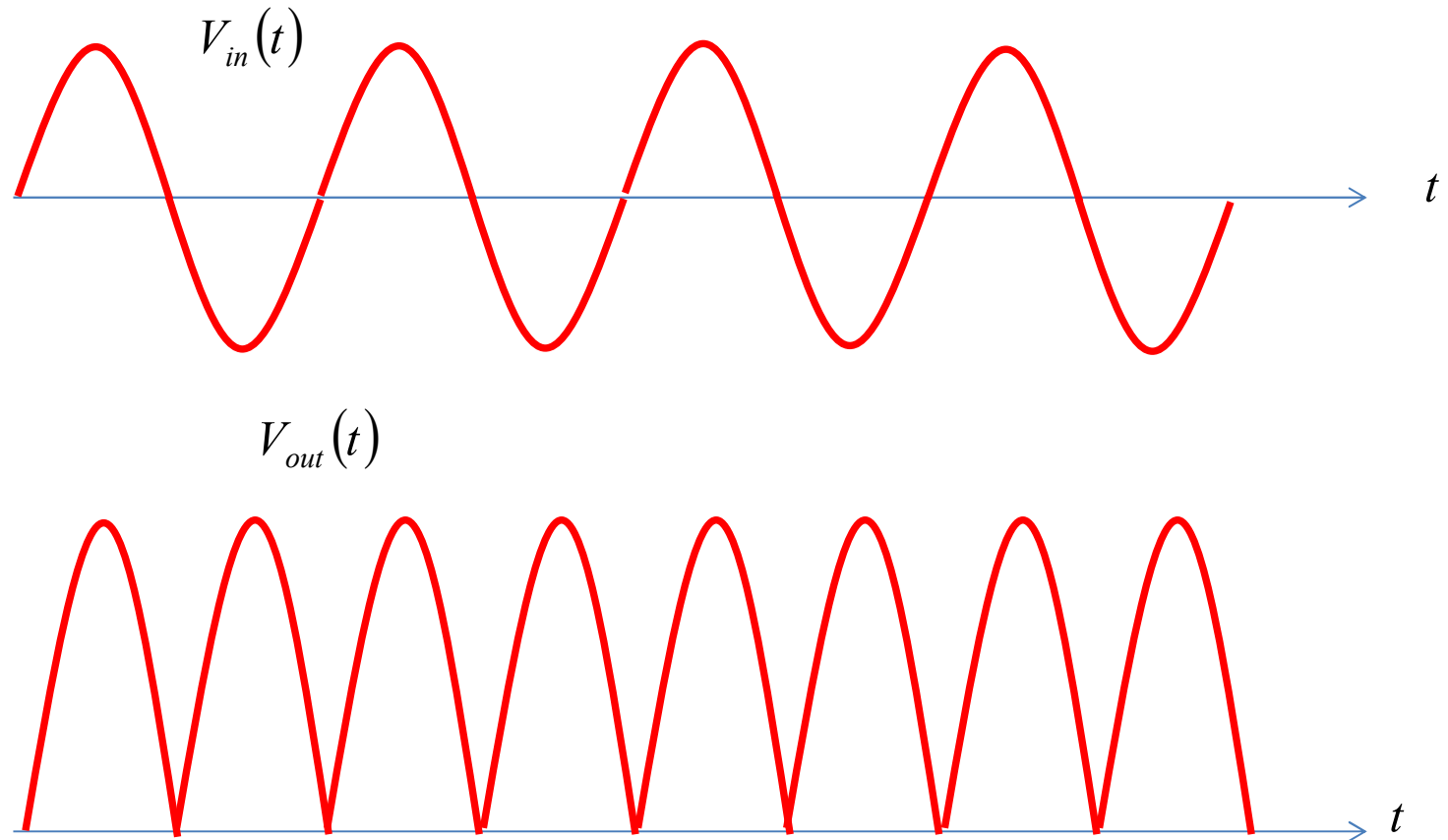


求绝对值电路

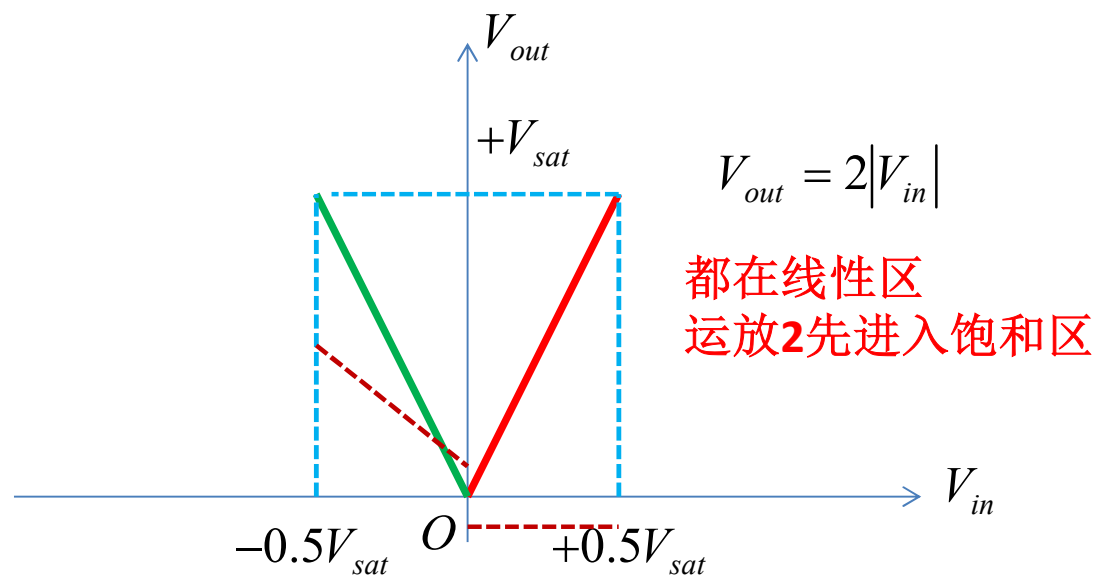
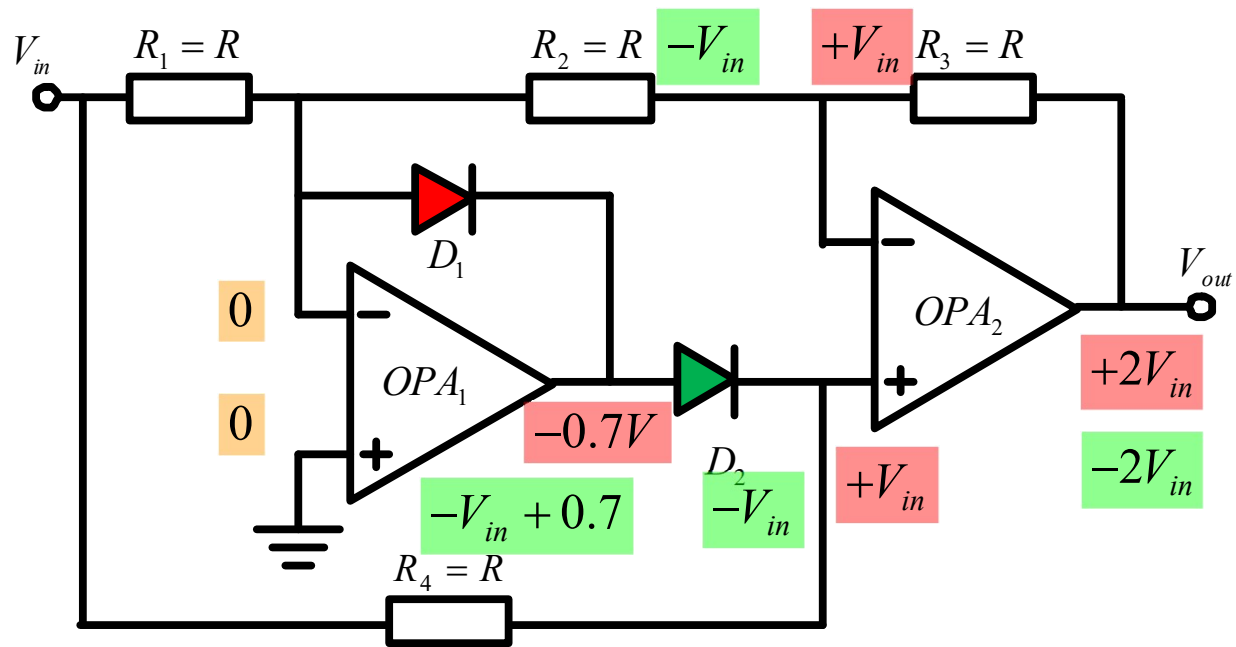


$$V_{out} = \begin{cases} +2V_{in} & V_{in} > 0 \\ -2V_{in} & V_{in} < 0 \end{cases} = 2|V_{in}|$$

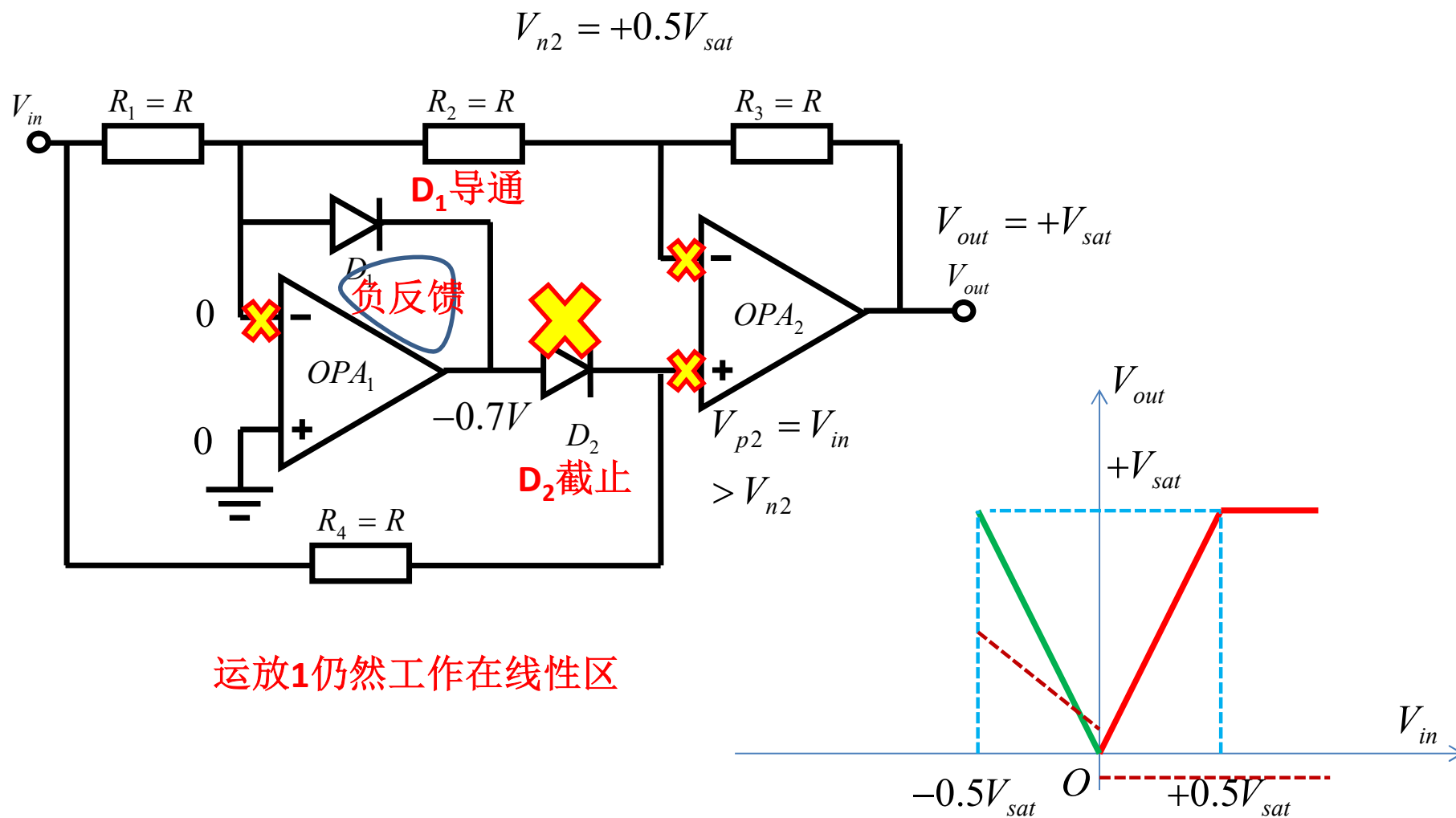
获得全波信号



转移特性曲线？



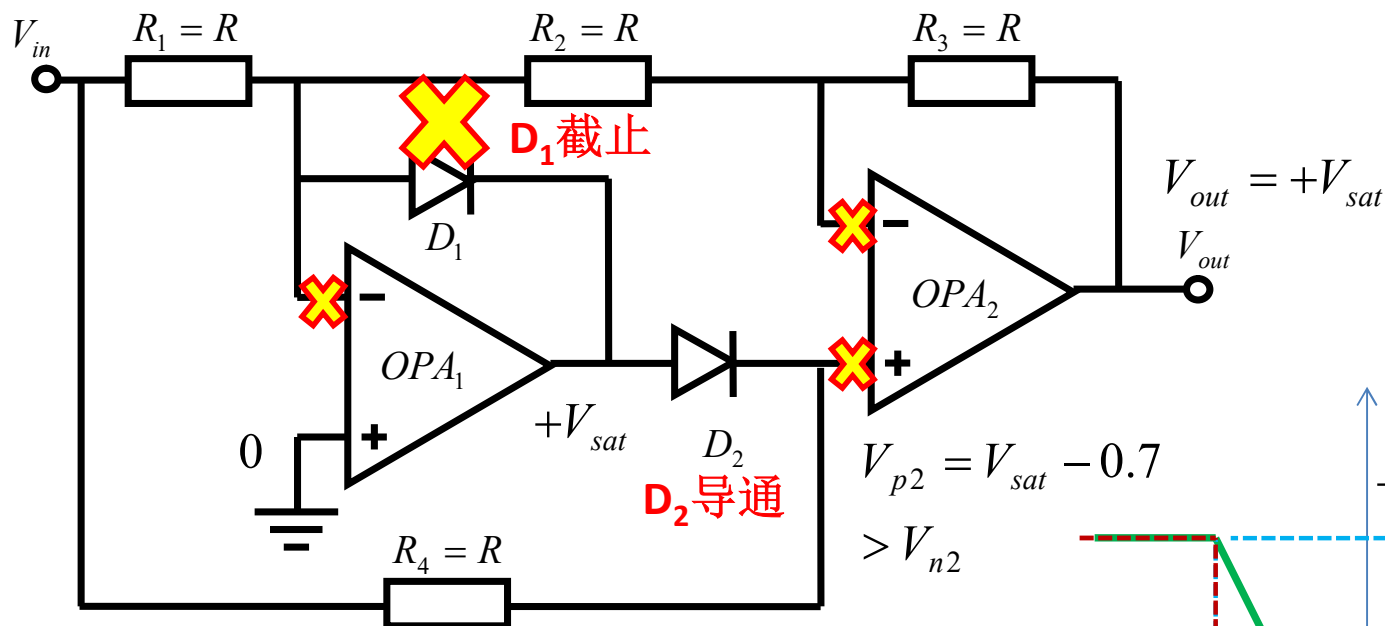
$V_{in} > 0.5V_{sat}$: 运放2进入正饱和区



$V_{in} < -0.5V_{sat}$: 运放2进入正饱和区

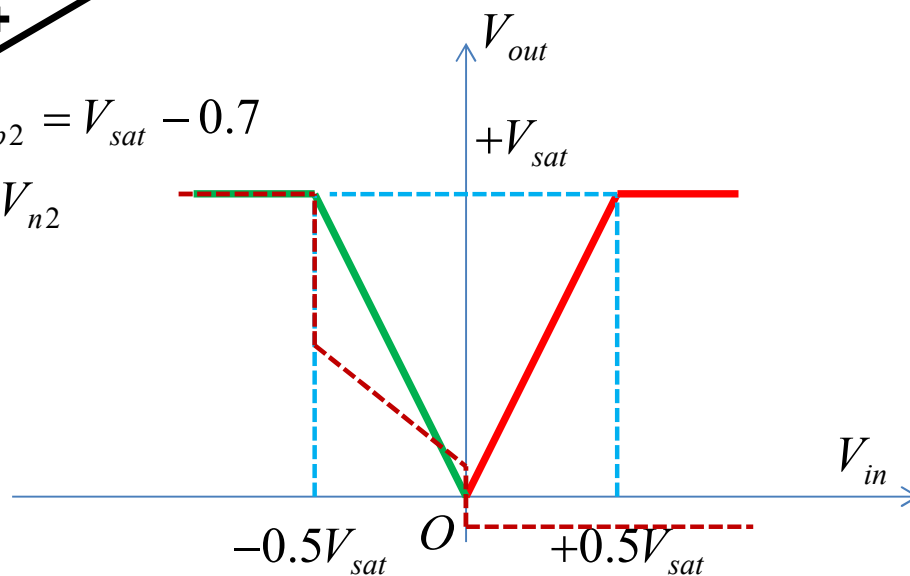
$$V_{n1} = \frac{2}{3}V_{in} + \frac{1}{3}V_{out} < 0$$

$$V_{n2} = \frac{1}{3}V_{in} + \frac{2}{3}V_{out} < -\frac{1}{6}V_{sat} + \frac{2}{3}V_{sat} = \frac{1}{2}V_{sat}$$



运放1工作正饱和区

$$V_{p2} = V_{sat} - 0.7 > V_{n2}$$



考前答疑与考试地点

- 考前安排到时通知
 - 时间
 - 考场分配
 - 答疑

考场要求

- 自带计算器
- 隔行隔列坐，严格考场纪律，不允许自带草稿纸，不允许多拿卷子
- 手机关机装到书包中，书包放前台
- 监考老师收卷、数卷无误后，方可离场

- 祝同学获得好成绩